

ARCHITECT CO PARTNERSHIP

**TECHNICAL PAPER IN SUPPORT OF THE
ENVIRONMENTAL ASSESSMENT**

WASTE RECYCLING FACILITY NEATH PORT TALBOT

TECHNICAL PAPER No 5

GROUND CONDITIONS AND CONTAMINATION

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1 NON-TECHNICAL SUMMARY

This is the non-technical summary for Technical Paper No 5 Ground Conditions and Contamination in support of the Environmental Assessment for the proposed recycling facility at Crymlyn Burrows in the County Borough of Neath Port Talbot.

Site investigations, in the form of trial pits and boreholes, have been carried out to enable samples of the existing soils which underlie the site, to be sent for laboratory testing and analysis. The results of the tests show that there are elevated levels of contaminants within the soils and is likely to be as a result of previous activities at the site, by adjacent users and historical backfill materials.

The effects on groundwater quality resulting from the proposed development are considered to be minimal and may be considered as insignificant. Measures have been designed and will be implemented in order to avoid or reduce disturbance of soils during construction work. It is considered that these mitigation measures should ensure that changes in groundwater quality do not occur.

Prior to construction, discussions will take place with environmental health officers of the Local Authority and Environment Agency. These discussions will allow for agreement with regards to acceptable levels of contamination which may be allowed to remain on the site and any measures which may be required to remove contamination from the site.

Consultation with the Local Authority and Environment Agency will also be undertaken to agree a process of ongoing water quality monitoring, prior to, during and after the construction phase of the project.

GIBB Environmental (GIBB) was commissioned on 18 September 1998 by Architects Co-Partnership (ACP) to provide technical support for an Environmental Assessment for a proposed reclamation facility at Crymlyn Burrows in the County Borough of Neath Port Talbot. The Environmental Assessment project is being led by ACP.

The Environmental Statement will be presented in three parts:

Part 1 - Project Description and Existing Environmental Conditions

Part 2 - Plan and Policies

Part 3 - Assessment of Environmental Impact

ACP is responsible for Part 1 and Part 2 of the Environmental Statement. ACP and GIBB are responsible for Part 3 of the Environmental Statement. The following Technical Reports are provided by GIBB in support of the Environmental Statement to be submitted with the Planning Application.

Technical Paper No. 1 - Ecological Impact Assessment

Technical Paper No. 2 - Noise and Vibration

Technical Paper No. 3 - Traffic and Highways

Technical Paper No. 4 - Water Resources

Technical Paper No. 5 - Ground Conditions and Contamination

Technical Paper No. 6 - Air Quality

This report is the Technical Paper No.5 Ground Conditions and Contamination.

The terms of reference for Technical Paper No.5 are to identify the existing ground conditions and contaminants and assess whether the proposed development will have any adverse effect on the ground conditions. This will include consultation with the local organisations, site investigations, a review of previous uses of the land and results from the laboratory testing, and consideration of the requirement for mitigation works.

The location of the proposed site is shown on Figure 1, and the location of the site investigations are shown in Figure 2. A description of the waste recycling process is given in Chapter 4 of this report.

3 SCOPING AND CONSULTATION EXERCISE

A scoping and consultation exercise was undertaken for the preparation of the technical paper in support of the environmental assessment process. The objective of the scoping and consultation exercise was to:

- (a) identify environmental baseline data available for the site;
- (b) gain an understanding of the proposed project in terms of the potential for environmental effects;
- (c) identify the key environmental issues to be addressed in the environmental statement; and
- (d) determine the extent and scope of any baseline surveys required.

The information sought for this exercise was obtained from various sources as set out below:

1. EnviroCheck Survey

An EnviroCheck report was obtained from the Landmark Information Group Ltd (LIGL), a database company that specialises in the provision of environmental information. This report provides historical ordnance survey maps, a site sensitivity map and data tables pertaining to the site, which identify and tabulate information such as landfill sites, British Geological Survey boreholes, Regionally Important Geological Sites (RIGS), Sites of Special Scientific Interest (SSSI), nature reserves, water/groundwater abstraction points, discharge consents, etc.

The full EnviroCheck report is included in Appendix B

2. Historical Records Review

The history of the land was researched to identify the previous land uses of the site and the surrounding environment. The object was to identify potentially contaminative historical land uses on or adjacent to the site. The search included a review of available historical maps, and other identified site-specific information.

4 PROJECT DESCRIPTION

The process carried out within the waste recycling facility comprises of waste separation, composting, refining and packaging and power generation. All operations are carried out within an enclosed building in order to contain the dust, odour and noise. The building will be insulated and all openings will be designed to minimise any impact on adjacent buildings.

Incoming refuse vehicles deposit the waste on the floor of the reception building, where buckets loaders stack and transfer the waste material onto conveyors feeding the process plant. Any large unwanted items are removed prior to treatment. The reception area will utilise rapid response doors to minimise dust and odour emissions.

Waste from the reception area is placed in a large hopper, where the plastic refuse sacks are split open, the contents screened and conveyed to the picking station. The picking stations remove the recyclable materials, placing them in separate containers for exportation from the plant. The remaining waste materials are further screened into materials which are combustible and waste material suitable for composting.

The material suitable for combusting is further screened before being densified into pellet form. The densified pellets are then stored prior to being fed into the combustor, which generates electricity to be used by the plant and exported to the National Grid.

The material suitable for composting is fed into the composting reactors, which convert the waste material into compost. The process involves the material being continuously turned to ensure the correct aeration and moisture levels are maintained, for approximately 63 days. The refined material is then bagged and stored ready for exportation.

5 REVIEW OF EXISTING INFORMATION

5.1 Site History

5.1.1 Sources of information

The historical information reviewed below has been compiled from Ordnance Survey maps as follows:

1880	1:2,500	Appendix C
1884	1:10,560	Appendix B
1899	1:2,500	Appendix B
1900	1:10,560	Appendix B
1917	1:2,500	Appendix B & Appendix C
1921	1:10,560	Appendix B
1938	1:10,560	Appendix B
1941	1:2,500	Appendix B & Appendix C
1964	1:10,560	Appendix B
1971	1:2,500	Appendix C
1979	1:10,000	Appendix B
1989	1:10,000	Appendix B

The maps in Appendix C were obtained from the archives of Swansea City Records Office. Appendix B maps were provided by LIGL in the EnviroCheck Report

5.1.2 Introduction

During the last two hundred years or so and up until the second world war, Swansea was one of the country's largest and busiest ports. Along the navigable length of the River Tawe, heavy industrial factories were constructed to produce steel, tin, zinc, copper, arsenic etc. as all the materials required for the production of these products were available. Ores were imported from other parts of Britain or abroad and coal imported from the South Wales coal fields which extended from the Swansea valley eastwards. Over a period of time the docks were expanded to cope with the larger ships bringing in the raw materials and exporting coal and other finished products to all parts of the world. The port was further enhanced by the increased use of rail freight, which continued expanding up until the establishment of the M4 motorway.

The site is in an area which reflects Swansea's more recent industrial past as the docks developed.

5.1.3 1880

The earliest maps available of the area date from 1880 (Ordnance Survey 1st Edition) and indicate that the site was undeveloped and in its natural state as sand burrows (Crymlyn Burrows). At this time the site was bounded to the north by a dual track rail line which remains today. Beyond this and slightly to the north west, a chemical production factory existed from pre 1880, owned by J.D. Pritchard & Company. Adjacent to the north of the factory was the Port Tennant Canal which remains today but in a disused state.

5.1.4 1880 - 1884

Between these years the area remains substantially unchanged. The site is shown as undeveloped rough pastures with no further developments in the surrounding area except markings to the north of the site, east of the Pritchard chemical factory (noted on the map as Burrows Works - Chemical), which may indicate a new boundary and the appearance of a pit.

It is possible that this shows the construction of the terraced houses known as Pritchard's Cottages.

5.1.5 1884 – 1899/1900

The site still remains undeveloped at this time. The Pritchard chemical works were still in use and the company had constructed a terrace of six houses to the east of the factory (Pritchards Cottages). A number of pits have appeared to the north and the east of the chemical factory, possibly generated by the construction works in the local area.

Carriage repair sheds were also constructed to the west of the site, one immediately adjacent to the site entrance as shown on the 1899 map. This structure remains and is currently used by Gower Chemicals Ltd.

5.1.6 1899 - 1917

- By 1917 the area saw massive and rapid development on the Crymlyn Burrows, possibly on a par with the nearby docks expansion. The site was now used as rail sidings, possibly as holding areas for ore and coal either for the local industry or export.

Pritchard's chemical works has been re-named Crymlyn Chemical Works.

Immediately to the south of the site a large tinplate works had opened. Marked on the maps as Kings Dock Tinplate Works and owned by Baldwins Ltd, the company also constructed a number of houses further south. These houses exist today, the street being known as Baldwin's Crescent. Surrounding the Tinplate works, to the south and east, the land shows distinct marks indicating that the area has been backfilled to accommodate rail sidings. This construction appears to be by end-tipping, probably using ash from the railways or slag waste from the tin plate works.

5.1.7 1917 - 1921

There are no substantial changes to the site and the surrounding area. Construction of a railway line had begun to the north of the site and the original railway lines. The original lines remain and are noted as serving the Vale of Neath. Within the site, two rail lines were extended to the east and are indicated as the Rhondda – Swansea line. Both of these lines would have carried coal mainly for export from the extensive South Wales coal fields.

The sand pit to the north of the chemical works has expanded, possibly due to on-going construction works in the local area.

5.1.8 1921 - 1938

Several structures had been constructed on the land adjacent to the site. The Baldwin's tinplate works is indicated to have expanded considerably and another large tinplate works had been constructed to the south. To the east, another large tinplate works had been constructed, this being owned by the Elba Tinplate Company Ltd, who also constructed housing to the south of the factory (Elba Crescent).

Pritchard's Cottages remain and are indicated as being inhabited, Crymlyn Chemical Works still appears to be operational.

5.1.9 1938 - 1941

The site itself remains largely unchanged at this time. During this period an extension of the rail sidings occurred. Rail tracks were constructed closer to the site to the north. A spur off the northern rail line had also been constructed, leading to further sidings at Jersey Marine, approximately 1 mile to the east.

5.1.10 1941 - 1964

Buildings and railway lines around the site remain unchanged during this time. Pritchard's Cottages remain marked on the map but appear derelict. The chemical factory has now been demolished, with most of this land to the north of the rail line having been reverted to sand burrows/woodland/bog. The area previously indicated as a pit has now been reclaimed and is featured on the plan as a contoured area.

5.1.11 1964 - 1971

By 1971, the rail sidings had been fully removed from the site with only the Vale of Neath line remaining. Rail sidings serving the Baldwin's tinplate works remain, however it is not known when the works ceased production.

By this time the A483 (Jersey Marine/Fabian Way) road had been constructed linking Swansea with the M4 motorway at Baglan, Port Talbot. During the mid 1960s the Ford motor company constructed their factory adjacent to the A483. It is possible that the Elba tinplate works building was transferred to Ford.

5.1.12 1971 - 1979

On the 1979 map, the site area is noted as the Freightliner Terminal. Baldwin's tinplate factory has been demolished and replaced by another works unit to the south of the site. An additional building has been constructed to the east, just south of the original tinplate works. An oil storage area has also expanded along the coastline, to the south of the site.

5.1.13 1979 - 1989

The site and surrounding areas remain substantially unchanged up to 1989, with the dismantling of the Vale of Neath railway being the only alteration to the area.

5.1.14 1989 - Present Day

The Freightliner terminal, still identified in the 1989 map is thought to have closed within the last 5 years. From this time it is thought the site has remained derelict. Ford Motor Co. still occupy the former tinplate works to the south. The Gower Chemicals works occupies the former railway sheds and warehouse to the east.

5.2 Previous Ground Investigations

Two previous ground investigations are known to have been carried out recently. These were by Golder Associates (1989) and Eastwood Materials Laboratory [EML] (1996). Both of these reports are included as Appendix E in this report.

No contamination testing was undertaken as part of the Golder's report but the fourteen trial pits and five cable percussion boreholes revealed made ground to a maximum thickness of 3.5m (generally 1 to 1.5 metres thick).

The EML report revealed the ground to have been impacted, principally with diesel fuel and lubricating oil. Total PAH was recorded at levels up to 170 mg/kg. Made ground was measured at thicknesses of between 0.6 and 2.4 metres.

5.3 Pollution Incidents

Several Pollution incidents are recorded in the EnviroCheck report, although one concerning an adjacent site user, Gower Chemicals, is not included. The incident, which is not recorded in the EnviroCheck report, involved a leak of Arcton 11®, a chemical synonymous with trichlorofluoromethane. This report is important as elevated levels of trichlorofluoromethane were found in the groundwater of BHE3, adjacent to the Gower Chemicals site.

6 EXISTING ENVIRONMENT

The existing environment is described below, based upon observations made at the site and the results of intrusive investigations.

6.1 Description of Site Conditions and Surrounding Area

The site is generally flat and is currently derelict. A large proportion of the centre of the site is covered in a concrete hardstanding. This relatively good quality concrete is doweled and sealed between joints.

To the north the Rhondda - Swansea railway line is currently in use and is known to carry coal. Further north a SSSI area of marsh (Crymlyn Bog) exists. Immediately to the east of the site is derelict land where rail sidings once stood.

The southern part of the site is bounded by a railway line used by Ford Motor Co. for their engineering works. This operation, manufacturing motor components, is housed in the old tin works.

Two major operations are housed immediately to the west of the site. Gower chemicals manufacturing various types of refrigerants and a metal works, machining pipes and other materials for Margham steelworks.

6.2 Fieldwork

The ground investigation fieldwork that has been carried out by Exploration Associates has included:

- Eleven environmental trial pits with disturbed sampling.
- Three shallow cable tool percussion environmental boreholes with in-situ testing, gas monitoring and disturbed sampling.
- Four cable tool percussion geotechnical boreholes with in-situ testing and disturbed and undisturbed sampling. A standpipe piezometer installation has been included one of the boreholes for ground water observations.

These were located as shown in Appendix A - Figure 2.

Samples of soil and groundwater were taken for chemical analysis and for future inspection. In situ testing in the form of Standard Penetration Tests (SPTs) was carried out to assist with the preliminary geotechnical appraisal of the site.

Soil samples for each trial pit and borehole were selected for chemical analysis, based on site observations.

PVC Type II permanent groundwater monitoring wells were installed into all three environmental boreholes drilled. The locations were chosen in order to assess the soil and groundwater quality on-site, to allow the direction of groundwater to be evaluated, and to assess the potential migration of contaminants on and off the site. The wells were purged after installation to ensure that the sample was taken from representative formation water. One groundwater sample was submitted for chemical analysis from each well location. The samples were delivered to the laboratories of Hyder Testing services for chemical analysis.

The samples were transported under chain-of-custody and UKAS accredited analytical methodologies were generally used.

Further ground investigations are proposed to be carried out by Exploration Associates, which will include two geotechnical boreholes utilising the ODEX drilling method. The purpose of these boreholes is to determine the depth of the dense gravel underlying this site

6.3 Geology and Ground Engineering

The following information is based on preliminary borehole logs, trial pit logs and the driller's daily sheets. Laboratory test results for geotechnical samples are unavailable.

The ground conditions that have been revealed by the excavations carried out to date reveal Made Ground overlying Recent Deposits and Alluvium.

6.3.1 Made Ground

Made Ground was encountered in all the trial pits and boreholes, comprising of a reinforced concrete slab, hardcore, dense to very dense gravels and occasional cobbles of ash, coal and slag. The thickness of the Made Ground varies between 0.5 and 1.6m.

6.3.2 Recent Deposits

The Recent Deposits was encountered in all the boreholes and trial pits underlying the Made Ground. These deposits comprise of loose to medium dense sand with occasional gravels, bands of peat and occasional bands of soft clay/silt. The thickness of the Recent Deposits varies between 3.7 and 6.5m. The thickness of the peat layer varies between 0.1 and 0.9m.

6.3.3 Alluvial Deposits

The Alluvial Deposits were encountered in all the geotechnical boreholes. However the full depth of these deposits was not determined during this phase of investigation, due to the very dense nature of the underlying gravels.

The alluvial deposits generally comprise very soft to soft sandy silty clay, very loose to medium dense sandy clayey silt, bands of peat, dense to very dense gravels and silty sand. Both clay and silt horizons were found to contain varying amounts of peat and plant remains. Boreholes G1, G3 and G4 were terminated into very dense gravels and cobbles. The thickness of the Alluvial Deposits penetrated varies between 13 and 19m.

6.4 Engineering Conditions

It is anticipated that the proposed development will have column loads varying between 600 and 1200 kN, and a ground floor loading of 50 kN/sqm. Assuming the columns are supported on 2m square foundations then the resulting loads on the founding medium will be 150 and 300 kPa.

The ground conditions, which include very soft alluvial deposits, are not adequate to provide sufficient bearing capacities. Structures founded on these deposits with peat layers will be subjected to considerable settlements and differential settlements.

The structures within this development are used to house and process domestic refuse, which contains leachates, and therefore need to be designed with very low differential settlements. In view of this requirement the existing ground conditions are not considered suitable. Therefore the structures should be supported on foundations incorporating piles taken into the very dense gravels.

6.5 Contaminated Land

6.5.1 Objectives

The objective of the assessment was to evaluate potentially contaminated shallow soils and groundwater within a targeted area of the site (Figure 2, Appendix A) for the presence of contaminants and to assess whether historical and current activities have adversely impacted the environmental condition of the site.

6.5.2 Contamination Criteria

In order to interpret the analytical results, it is common practice to compare them with the various guidelines published in the UK and Europe: the UK Interdepartmental Committee on the Redevelopment of Contaminated Land's (ICRCL) guidelines published as Guidance Note 59/83 (second edition 1987) and the guidelines published by the Dutch authorities as the Dutch Test Table. These guidelines are used to provide an indication of the levels of contamination present at the site, assess the potential risks to health posed by the levels for various end-uses and aid in the identification of potential environmental liabilities associated with a site.

The ICRCL values provide the most appropriate guidance in the UK and are primarily intended as a guide for site redevelopment. They were published in 1983 and revised in 1987 and use the concept of 'trigger concentrations' of contaminants in soil which are related to the intended end use of the site, these trigger concentrations differ depending upon the sensitivity of the end-use to contamination. There are two trigger concentrations given known as the threshold level and the action level. In general, if after a thorough investigation, soil samples from a site show values below threshold trigger concentrations it is reasonable to regard the site as uncontaminated. If, however, some results exceed the action level, some remedial action may be required if the chosen form of development is to proceed. It is recommended that sites with sample concentrations that fall between the threshold and action trigger levels be assessed on a site specific basis, where considerations such as level of risk and cost of remediation are taken into account in determining whether remedial action is necessary.

However, the ICRCL guidelines do not contain trigger concentrations for all contaminants in soil and in particular they do not contain action levels for metals. Furthermore they do not contain trigger concentrations for any contaminants in groundwater. They were developed in the late 1970s/early 1980s using humans as the most sensitive receptor to contamination, and are now considered to be somewhat dated by many practitioners. The Department of the Environment has initiated a research programme into contaminated land in order to increase the list of substances for which guidance is given, to revise the current ICRCL limit values, and to review their relation to ecological effects which in some cases can be a more sensitive receptor than humans. It is likely that this programme will result in a revised set of ICRCL guidelines in which a number of the threshold values are changed.

In the meantime, it is common practice to refer to the more comprehensive guidance levels used by the Dutch authorities and given in the Dutch Test Table. However, these levels are generally more stringent than the ICRCL values because they are not 'end-use' specific and therefore the levels reflect the values at which the most sensitive receptors (ie. groundwater or children) are considered at risk. In addition they have been developed for the Netherlands specific ground conditions where groundwater is highly vulnerable to pollution from

contamination. Nevertheless, the Dutch values are commonly used as a framework for indicating and evaluating potential contamination risks for those contaminants not specified by the ICRL guidelines in soil and for contaminants in groundwater.

The Dutch guidelines are based on a framework comprising a 'target' level and an 'intervention' level. This replaces previous Dutch limits which have comprised an A, B and C classification for uncontaminated, need for further investigation and need for environmental remediation respectively.

The 'Target' level is a reference value above which there is demonstrable pollution and below which there is no demonstrable pollution.

The 'Intervention' Level is the threshold value above which the pollutant should generally be treated, if sufficient volume of contamination exists.

The results of the chemical analysis are discussed in the following section.

6.5.3 Results of Chemical Analysis

a) Soils (Appendix F)

Polyaromatic Hydrocarbons (PAH)

All of the soil samples tested for PAHs were below the ICRL Threshold level for Landscaped areas and hard cover. One sample however, TP2 @ 0.6 - 0.7m was greater than the Dutch Intervention Level of 40 mg/kg at 61.91mg/kg.

Total Petroleum Hydrocarbons (TPH)

This analysis was undertaken to indicate the presence of petroleum hydrocarbons in the subsurface. This method allows the identification of the total concentration of petroleum hydrocarbons in the Carbon 7 to Carbon 32 (C7-C32) range.

Soil samples BHE2 and BHE3 were found to contain concentrations of petroleum hydrocarbons (53.6 mg/kg, and 61.1 mg/kg, respectively) which exceed the Dutch Target level concentration of 50 mg/kg. However, the concentrations did not exceed the Dutch Intervention level concentration of 5000 mg/kg. TPH concentrations tended to reduce with soil depth.

Soil taken from trial pits contained only trace amounts of petroleum hydrocarbons and were below the Dutch target level.

Volatile Organic Compounds (VOCs)

All soil samples submitted for analysis were found to be below the Dutch Intervention levels for all VOCs for which Intervention levels are available, although traces of certain VOCs were found in a number of samples, taking the concentrations of these particular VOCs above the Dutch Target value.

Soil samples BHE1, BHE2 and BHE3 contained traces of Dichloromethane at 7.1 mg/kg, 11.3 mg/kg and 4.98 mg/kg respectively. The higher concentrations were found to occur in samples collected from deeper levels in the borehole. Soil samples taken from the environmental boreholes and all of the trial pits contained traces of 1,1,1 trichloroethane and toluene at concentrations ranging from 0.0025 mg/kg to 32.8 mg/kg and 0.002 mg/kg to 23.1 mg/kg respectively. The highest concentration of 1,1,1, trichloroethane was found at BHE2, between 2.5 - 3.5 meters depth and toluene at TP1, at a depth of 1.9 - 2.3 meters.

Trichloroethene was present in all trial pit samples at concentrations of 0.0011 mg/kg to 0.168 mg/kg, with the largest concentration occurring at TP6 between depths of 1.2 - 1.4 meters. In comparison to the data from other boreholes, there is no connection of elevated

concentrations with depth.

Traces of trichloromethane and M/P xylene were also found in some trial pit samples at concentrations of between 0.002mg/kg to 0.088 mg/kg and 0.002 mg/kg to 0.035 mg/kg respectively. The highest of these concentrations are found in TP1 soil samples, which in addition to the compounds above, also contains tetrachloromethane and O-xylene at concentration of 0.0107 mg/kg and 0.0118 mg/kg respectively.

Soil sampled from TP9 at a depth of 2.6-2.7 meters also contain a number of derivatives of butyl/propylbenzene which are not found in any other soil sample. The concentrations of these compounds are also very high in comparison to the concentrations of other VOCs. For example sec-butylbenzene is found at elevated concentrations of 0.528 mg/kg

Metals

Samples taken from the top layers of the soil profile, from 0.1 to 1.2 meters show elevated concentrations of the metals that have been analysed. The highest concentrations found in the soil samples are detailed below.

Arsenic was detected at concentrations of 49mg/kg, 52mg/kg, 55mg/kg, 91mg/kg and 196mg/kg in the soil samples from BHE3, TP2(0.6 to 0.7m depth), TP4(0.4 to 0.6m depth), TP8(0.3 to 0.4m depth) and TP10(0.6 to 0.7m depth) respectively, exceeding the ICRL Threshold level concentration of 40 mg/kg, especially in the latter two boreholes where the concentrations are particularly high.

Boron was detected at concentrations 4.3 mg/kg and 6.6 mg/kg in the soil samples from TP1 and TP9 respectively, exceeding the ICRL Threshold level concentration of 3 mg/kg. It should be noted that the high concentration of boron in TP9 was found at a depth of between 2.6 and 2.7 meters.

Copper was detected at concentrations of 386mg/kg, 441mg/kg, 171mg/kg, 191mg/kg, 310mg/kg in the soil samples from BHE3, TP2, TP5, TP8, TP10, respectively, all of which exceed the ICRL Threshold level concentration of 130 mg/kg.

Nickel was detected at concentrations of 80mg/kg, 74mg/kg and 76mg/kg in the soil samples from BHE3, TP8 and TP10, respectively, all of which exceed the ICRL Threshold level concentration of 70 mg/kg.

Zinc was detected at concentrations of 5440mg/kg, 3550mg/kg, 330mg/kg and 407mg/kg in the soil samples from TP2, TP5, TP6 and TP8, respectively, all of which exceed the ICRL Threshold level concentration of 300 mg/kg.

b) Groundwater (Appendix F)

Total Petroleum Hydrocarbons (TPH)

Petroleum Hydrocarbons were not detected in any of the groundwater samples taken from the environmental boreholes, therefore concentrations of TPHs in groundwater were within the Dutch target value of 50 µg/l.

Volatile Organic Compounds (VOCs)

Water samples collected from all boreholes were found to contain only traces of VOCs at concentrations that do not exceed the Dutch Intervention values. However, the VOCs that were detected during analysis are classed as being above the Dutch Target levels. These particular VOCs are detailed below.

BHE1 was found to contain trichlorofluoromethane at a high concentration of 62.0µg/l, although there is no target level defined for this compound in the Dutch recommendations. Similarly 1,1,1 trichloroethane and tetrachloroethene are found at concentrations of 3.2 µg/l

and 1.2 µg/l respectively, with no target level defined. 1,1 dichloroethane is also found in the groundwater of BHE1 at 1.7 µg/l which is below the Dutch Intervention level of 400 µg/l

BHE2 contains a number of VOCs which include 1,3,5/1,2,4 trimethylbenzene, N-butylbenzene, benzene, M/P xylene, O-xylene and p-isopropyltoluene at concentrations of 33.9 µg/l, 17.6 µg/l, 6.6 µg/l, 1.1 µg/l, 7.7 µg/l, 2.5 µg/l and 6.4 µg/l. The only compounds which have been designated an intervention level are benzene (at 30 µg/l) and Xylene (at 70 µg/l) and so these compounds are below the Intervention Levels.

In groundwater sampled from BHE3 the only VOC to be present is trichloromethane existing at a concentration of 3.4 µg/l which does not exceed the Dutch Intervention level of 400 µg/l.

Metals

Arsenic is present in BHE2 and BHE3 samples at concentrations of 51 µg/l and 28 µg/l which are above the Dutch target value of 10 µg/l but are just below the Intervention value of 60 µg/l. The groundwater sample taken from BHE1 shows a concentration of 9 µg/l which is just below the target value.

Chromium is only detected in BHE3. The water sample from this borehole shows an elevated concentration of this metal of 70 µg/l which exceeds the intervention value of 30 µg/l.

Copper is detected in all three boreholes (BHE 1, 2, and 3) at concentrations between 20 µg/l and 40 µg/l which are below the intervention value of 75 µg/l, but above the target value of 15 µg/l.

Lead is present in BHE2 and BHE3 to concentrations of 60 µg/l and 180 µg/l respectively. The Dutch Intervention level for arsenic in water is 60 µg/l, and therefore exceeds the intervention level in groundwater from BHE3 and is equal to the intervention level in BHE2

Mercury is present in BHE2 and BHE3 at concentrations of 0.14 µg/l and 0.04 µg/l respectively. The concentration of mercury in BHE3 is just below the target value of 0.05 µg/l, whereas BHE2 exhibits concentrations greater than the target level but below the Intervention level of 0.3 µg/l.

Nickel is present in boreholes BHE1, BHE2 and BHE3 at concentrations of 30 µg/l, 60 µg/l and 100 µg/l respectively. The concentration of Nickel in BHE3 is above the Intervention level of 75 µg/l and BHE1 and 2 are above the target value of 15 µg/l.

Concentrations of zinc in all three groundwater samples are below the intervention value of 800 µg/l at concentrations of 80 µg/l, 260 µg/l and 610 µg/l respectively, but exceed the target value of 65 µg/l

Boron was present in BHE1, BHE2, and BHE3 at concentrations of 130 µg/l, 190 µg/l and 180 µg/l. However, no assessment levels of boron in groundwater has been defined in the Dutch criteria.

Neither Selenium, chromium or cadmium were detected in any of the borehole groundwater samples.

5.2.3 Quality Assurance/Quality Control (QA/QC) (Table Appendix F)

The duplicate groundwater sample, taken from BHE2 but labelled E4, showed good correlation to the primary sample, with regard to all analysed parameters. Elevated concentrations were not detected in the laboratory blank sample which indicates that cross contamination via the sampling equipment or storage and transport of samples is unlikely to have occurred.

6.6 Gas

Gas monitoring was carried out at the site during drilling and on 16 October 1998, as detailed in Appendix H. The results of gas monitoring have been interpreted with respect to the guidance given in Waste Management Paper No.27 1991: Landfill Gas, and The Building Regulations Approval Document 1991 Part C2 "Dangerous and Offensive Substances". These documents give a trigger value of 1% by volume for methane and 1.5% by volume for carbon dioxide in buildings.

If methane or carbon dioxide levels in the soil atmosphere beneath the site are found to exceed these trigger values, then a risk assessment and possibly remedial / preventive action is appropriate.

6.6.1 Methane

Methane was recorded at elevated concentrations of 82% and 24% by volume in BHE1 and BHE3, respectively, on 16 October 1998.

6.6.2 Carbon Dioxide

Carbon dioxide was recorded at elevated concentrations of 2.6% and 1.7% by volume in BHE1 and BHE3, respectively, on 16 October 1998.

7 CONSTRUCTION EFFECTS AND MITIGATION MEASURES

7.1 Construction Effects

The main construction works will take approximately 18 months to complete, and will require the use of heavy machinery. It is assumed there will sub-structure will be supported on piled foundations which will necessitate the removal of sections of the existing concrete apron.

Piling may provide a potential route for contamination to the deeper aquifer in the dense gravels at approximately 20 metres depth. Dewatering activities from excavations may also spread contamination and pollute controlled waters.

The effect of elevated methane and carbon dioxide must also be taken into account in both the design and in any construction operations which may include confined spaces. Methane is a potential explosive gas whilst carbon dioxide is an asphyxiate.

7.2 Mitigation Measures

The risks to workers, the general public and the environment from construction works on a site where elevated levels of contamination have been found will need to be assessed. Risk assessments must be undertaken both by the contractor for the works and by those involved in the planning and design of the works.

The Site Contractor would be required to undertake measures to prevent the spread of contamination. Typical construction activities such as excavation, trenching, and general site groundworks which disturb the ground, should be minimised both in design and execution, and be carefully managed to limit disturbance and infiltration of the surface water. Where the ash fill material is excavated it will need to be tested prior to either disposal or re-use. Further consideration should be given to this when site layout is finalised and working methods and construction phasing have been identified.

During the planning and design work, discussions will need to take place with officers of the Local Authority with respect to acceptable levels of contamination. Ongoing consultation with the Local Authority will be undertaken to ensure acceptable work procedures at the site and where contaminated materials are to be transported off-site.

The construction will be designed in such a way as to prevent the ingress of gas from beneath the floor slab, or into the buildings. The existing slab will be vented to prevent the build up of gases.

8 OPERATIONAL EFFECTS AND MITIGATION MEASURES

8.1 Operational Effects

Operations at the site will be planned so as not to create further contamination. All fuel and chemical storage will be within reinforced concrete bunded areas, all ground floor slabs are to be designed and constructed to minimise cracking and the number of floor joints – reducing the possible leachate migration. All surface water is to be stored and recycled through the composting process, negating the need for soakaways.

8.2 Mitigation Measures

Measures will be incorporated into the project during operation to prevent further contamination of the soil and groundwater. No intrusive work shall be undertaken unless a defined strategy, agreed with the Local Authority has been formulated.

The facility will be designed and operated in such a way that leachates generated during the storage and treatment of the waste will be collected and recycled into the composting process.

9 DEMOLITION/DECOMMISSIONING EFFECTS AND MITIGATION MEASURES

It is understood that this facility will be in continuous operation for a minimum period of 12 years, after which the combustor will have to be replaced due to wear and tear. Replacement work could take up to 3 to 4 months, after which the combustor will be in continuous operation for a further 12 years.

Demolition should, when required, be undertaken in a safe and clean manner, preventing the spread of dust and potentially harmful materials.

10 MONITORING REQUIREMENTS

10.1 Construction Monitoring Requirements

It is recommended that gas and ground water monitoring is undertaken prior to construction to provide a reasonable set of baseline data with which to compare future readings.

Ground water monitoring should be undertaken at location(s) to be agreed with the Local Authority, during critical phases when there may be a possibility of impacting the groundwater. This will allow any further impact on the quality of the groundwater to be identified, if it occurs. It will provide a database of information to show that the mitigation measures undertaken during the construction works have been successful. If possible the existing monitoring wells (BHE1 to BHE3 in Figure 2, Appendix B) should be utilised for this purpose.

Due to the high concentrations of gas measured, monitoring, which will include flow measurements, should be carried out to enable the risks posed by the subsurface gases to be more clearly understood and incorporated into the design prior to construction.

10.2 Operational Monitoring Requirements

Monitoring may be required by the Local Authority during the operational life of the plant. Ongoing monitoring of gas concentrations is recommended for both the exteriors and interiors of the building for a period following completion of the construction works.

11 CONCLUSIONS AND RECOMMENDATIONS

Based on the results of this investigation, there is evidence that both the made ground and the groundwater beneath the site have been impacted. At this stage, it is not known if the site is currently causing contamination of the groundwater. Due to the proximity of other possibly contaminating facilities in the area it is considered likely that the findings of this assessment reflect the true groundwater quality in the area.

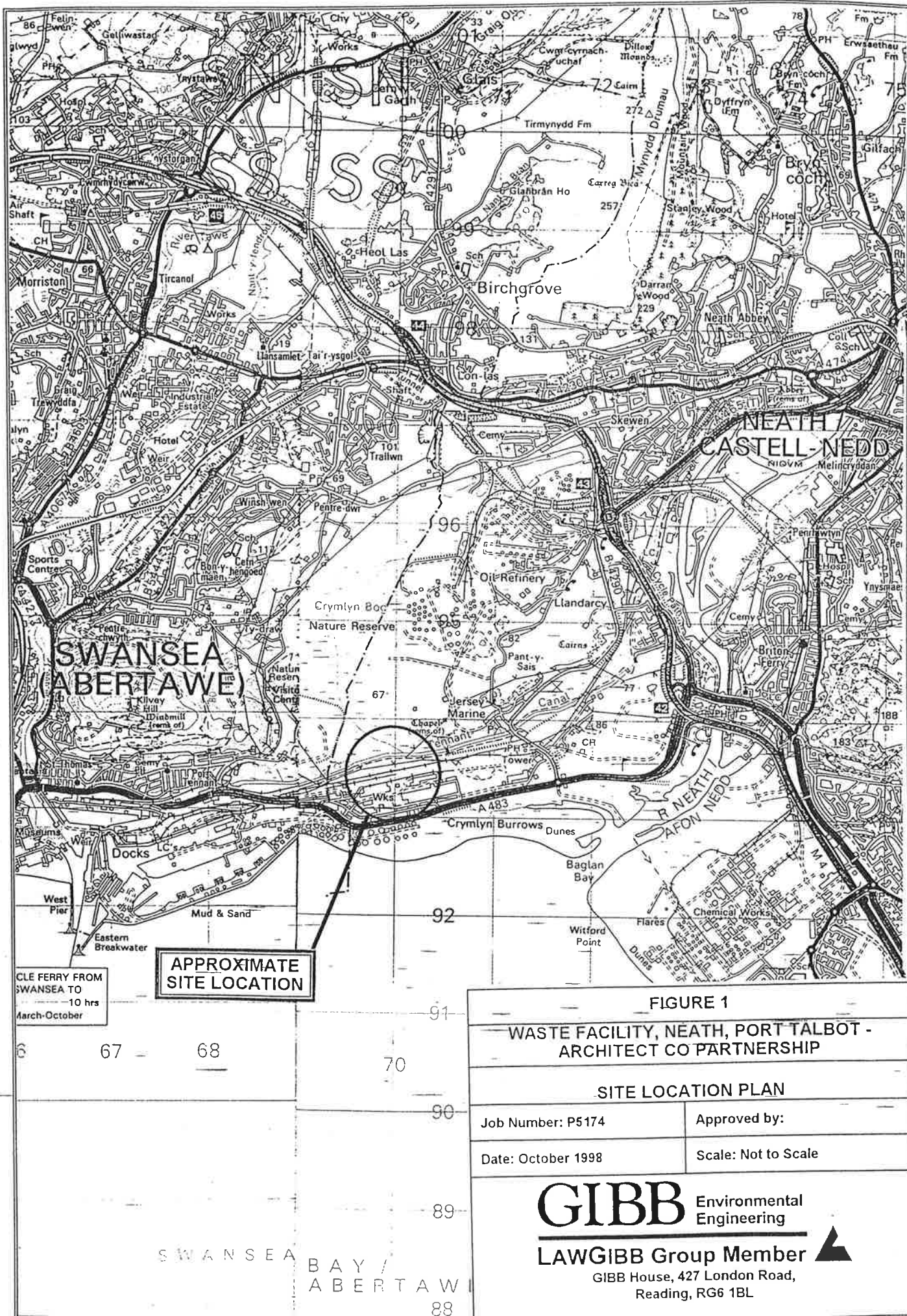
It is recommended that gas and water monitoring is undertaken prior to, and during construction, to provide a reasonable set of baseline data with which to compare future readings. There should then be an ongoing monitoring regime to firmly establish and fully understand the conditions at the site.

This monitoring should consist of water contamination sampling and testing, gas monitoring and gas flow measurement.

It is not considered necessary to undertake any remedial work at the site as the contaminated materials are considered to be isolated by the existing concrete slab, which is to be retained. The development of the site will increase the area of hardstanding on the site, which will further isolate any contaminated materials and limit further infiltration of contaminants into the groundwater.

It is recommended that any excavation of materials is undertaken after assessment of the risk to site operatives and the potential for leachate generation. All works are to be undertaken in a manner which will limit or prohibit these risks.

APPENDIX A – FIGURES



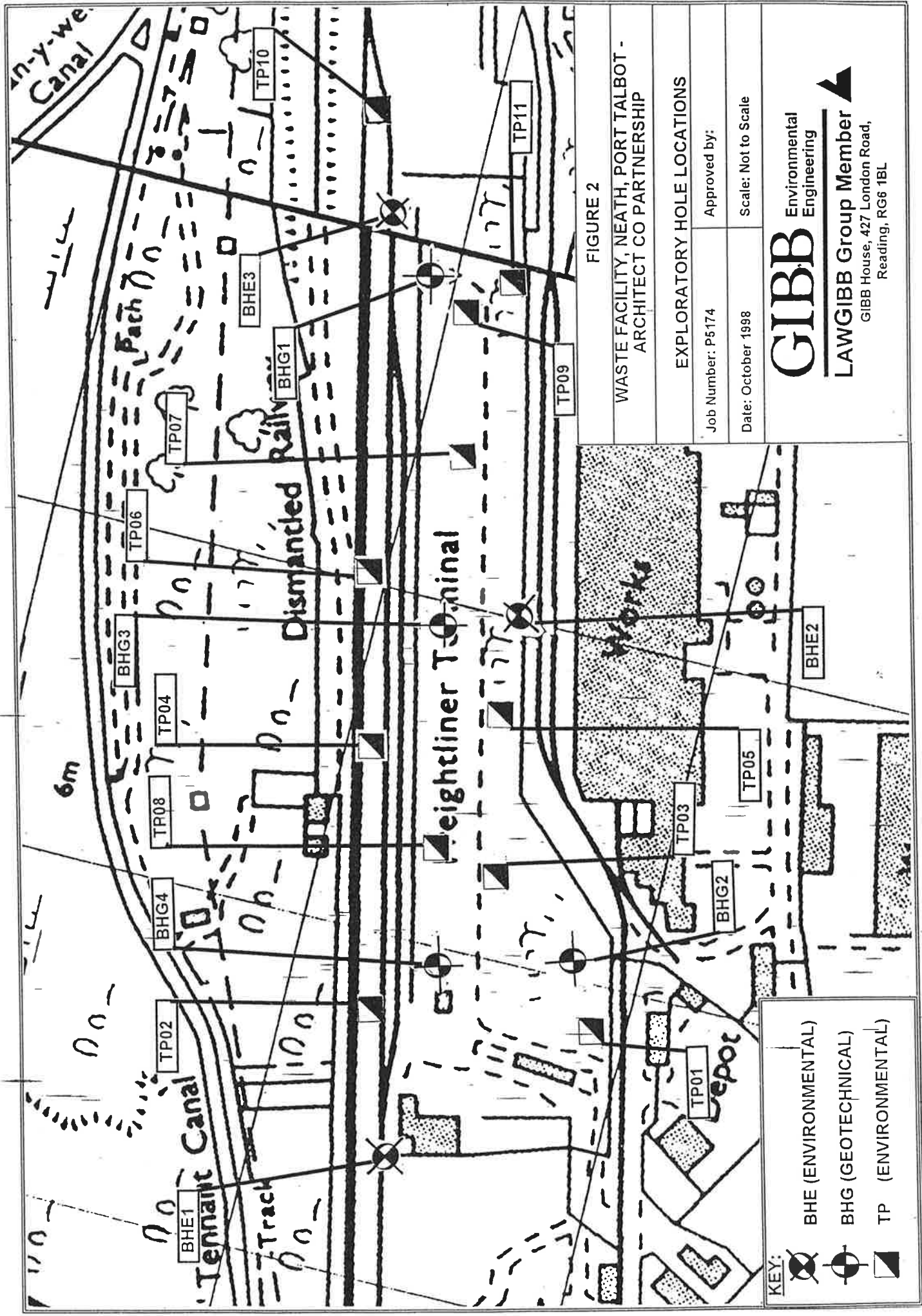


FIGURE 2

WASTE FACILITY, NEATH, PORT TALBOT - ARCHITECT CO PARTNERSHIP	
EXPLORATORY HOLE LOCATIONS	
Job Number: P5174	Approved by:
Date: October 1998	Scale: Not to Scale

GIBB Environmental Engineering

LAWGIBB Group Member

GIBB House, 427 London Road,
Reading, RG6 1BL

APPENDIX B
ENVIROCHECK-REPORT

**EnviroCheck Report on:**

Freightliner Terminal Site
SWANSEA

National Grid Reference :

269800, 193300 —

Prepared For :

Gibb Ltd
Development House
Road End Road
Oldbury
Warley
B69 4HW

Your Reference :

Neil Parry, NVP/J410/P5174/355/



Summary

Environmental Setting

Industrial Setting

Useful Contacts

BGS Borehole Order Form

Introduction

The Environment Act 1995 has made site sensitivity a key issue, as the legislation pays as much attention to the pathways by which contamination could spread, and to the vulnerable targets of contamination, as it does to the potential sources of contamination. For this reason, Landmark's Site Sensitivity Data Sheet places great emphasis on statutory data provided by the Environment Agency and the Scottish Environment Protection Agency; it also incorporates data from English Nature (and the Scottish and Welsh equivalents), the Environment Agency (and the Scottish equivalent) and Local Authorities; and highlights hydrogeological features required by environmental and geotechnical consultants. It does not include any information concerning past uses of land. The data sheet is produced by querying the legend database to 1km from a single point provided by the client.

Landmark has geocoded and plotted the data to 1m accuracy where possible. Where this isn't the case, data is geocoded to +/- 100m accuracy. In the attached datasheet the National Grid References (NGRs) are rounded to the nearest 100m in accordance with Landmark's agreements with a number of Data Suppliers.

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Data Type	50m	250m	500m	1000m
Water				
Water Abstractions				
Discharge Consents			✓ 1	✓ 1
Red List Discharge Consents				
Prosecutions relating to Controlled Waters				
Pollution Incidents to Controlled Waters			✓ 3	✓ 2
Nearest Surface Water Feature			✓	
Waste				
Landfill Sites				✓ 1
BGS Recorded Landfill Sites				
Waste Treatment or Disposal Sites				
Waste Transfer Sites			✓ 1	
IPC Registered Waste Sites				
Statutory / Authorisation				
Integrated Pollution Controls				
Air Pollution Controls				
Registered Radioactive Substances				
Prosecutions relating to Authorised Processes				
Enforcement and Prohibition Notices				
Planning Hazardous Substance Consents				
Planning Hazardous Substance Enforcements				
Other				
Planning Applications (of possible contaminative uses)				✓ 1
BGS Recorded Mineral Sites				
BGS Boreholes		✓ 1	✓ 1	✓ 10
Sites of Special Scientific Interest			✓ 1	✓ 2
Potentially Contaminative Industrial Use				✓ 2

Water Abstractions identified, whose centres are more than 1000 metres (but less than 2000 metres) from the centre of the site: 1



Map ID	Details	Estimated Distance from Site	Source	NGR
	Water Abstraction			
	Operator B.P Oil Refinery Ltd	1300	EA	269900
	Licence No 22/59/5/0007			194600
	Location Location Description Not Available			
	Abstraction General Industrial			
	Source River			
	Daily Rate 0 cubic metres			
	Yearly Rate 205 cubic metres			
	Details Freemans Bund			
	Most Sensitive Groundwater Resource			
	Minor Aquifer with possible Drift Deposits		EA/SEPA	
1	Discharge Consent			
	Operator Dwr Cymru Cyfyngedig	710	EA	269900
	Property Type Sewerage Network - Sewers			192600
	Location Em O'Flow B Crymlyn Bur , Crymlyn Burrows S Scheme			
	Catchment Area N/A			
	Discharge Reference BE0010502			
	Issued 8th October 1969			
	Discharge Type Sewage Effluent Discharge-Crude Effluent			
	Discharge Coastal			
	Environment			
2	Discharge Consent			
	Operator Dwr Cymru Cyfyngedig	500	EA	269500
	Property Type Sewerage Network - Sewers			192900
	Location Emergency O'Flow A , Crymlyn Burrows Sewerage S			
	Catchment Area N/A			
	Discharge Reference BE0010501			
	Issued 8th October 1969			
	Discharge Type Sewage Effluent Discharge-Crude Effluent			
	Discharge Coastal			
	Environment			
8	Site of Special Scientific Interest			
	Details Site of Special Scientific Interest	820		270500
				193700
	Site of Special Scientific Interest			
	Details Site of Special Scientific Interest	270		269700
				193600
	Site of Special Scientific Interest			
	Details Site of Special Scientific Interest	580		270300
				193000
	BGS Borehole			
12	BGS Reference SS69SE 2	120	BGS	269800
	Drilled Length 42.67 metres			193200
	Bore Name CRYMLYN BURROWS (NEATH U.D.C.) BOREHOLE			
13	BGS Borehole			
	BGS Reference SS69SE 17	510	BGS	269400
	Drilled Length 21 metres			193000
	Bore Name KINGS DOCK JUNC. E. SIDE APPROACH RD, SWANSEA. 2			
14	BGS Borehole			
	BGS Reference SS69SE 23	980	BGS	268900
	Drilled Length 0 metres			193700
	Bore Name TIR JOHN POWER STATION. BH.2			
15	BGS Borehole			
	BGS Reference SS69SE 28	910	BGS	269000
	Drilled Length 0 metres			193700
	Bore Name TIR JOHN POWER STATION. BH.7			
16	BGS Borehole			
	BGS Reference SS69SE 16	490	BGS	269400
	Drilled Length 22.22 metres			193000
	Bore Name KINGS DOCK JUNC. E. SIDE APPROACH RD, SWANSEA. 1			



Map ID	Details	Estimated Distance from Site	Source	NGR
17	BGS Borehole BGS Reference SS69SE 22 Drilled Length 0 metres Bore Name TIR JOHN POWER STATION. BH.1	990	BGS	268900 193600
18	BGS Borehole BGS Reference SS69SE 24 Drilled Length 0 metres Bore Name TIR JOHN POWER STATION. BH.3	1000	BGS	269000 193900
19	BGS Borehole BGS Reference SS69SE 29 Drilled Length 0 metres Bore Name TIR JOHN POWER STATION. BH.8	950	BGS	269000 193800
20	BGS Borehole BGS Reference SS69SE 139 Drilled Length 0 metres Bore Name SWANSEA BAY BW1 SCHEME BH 165	1000	BGS	268900 192900
21	BGS Borehole BGS Reference SS69SE 140 Drilled Length 0 metres Bore Name SWANSEA BAY BW1 SCHEME BH 175	910	BGS	269000 192900
22	BGS Borehole BGS Reference SS69SE 141 Drilled Length 0 metres Bore Name SWANSEA BAY BW1 SCHEME BH 185	840	BGS	269100 192900
23	BGS Borehole BGS Reference SS69SE 142 Drilled Length 0 metres Bore Name SWANSEA BAY BW1 SCHEME BH 195	750	BGS	269100 192900
24	Landfill Site Licence Holder Swansea D c_City Of Licence Reference L1/21 A & B Site Tir John Tip, Crymlyn Bog, Swansea, W Glam Operator The Guildhall, Swansea, W Glam SA1 4PE Authority Environment Agency - Welsh Region South West Area Site Category Landfill Site Licence Status Site is operational as far as is known Waste types on Site: Authorised waste Household Waste Max.Waste From Fees/Charges Prohibited waste Toxic/Poisonous Wastes	860	EA	269000 193600



Map ID	Details	Estimated Distance from Site	Source	NGR
3	Pollution Incident to Controlled Waters Name: Unknown Operator Property Type: Road (Lost Load) Location: Jet Garage, Fabian Way, Swansea Authority: Environment Agency Welsh Region Pollutant: Miscellaneous - Fire water / Foam Note: Mechanical Failure Incident Date: 26th June 1995 Incident Reference: 24572 Catchment Area: N/A Received Water: N/A Cause: Spillage Severity: Category 3 - Minor Incident	500	EA	270200 193000
4	Pollution Incident to Controlled Waters Name: Unknown Operator Property Type: Unknown Location: Fabian Way, Swansea Opp, Fords Factory Authority: Environment Agency Welsh Region Pollutant: Crude Sewage Note: Not Given Incident Date: 17th February 1995 Incident Reference: 22687 Catchment Area: N/A Received Water: N/A Cause: Unknown Severity: Category 3 - Minor Incident	580	EA	270300 193000
5	Pollution Incident to Controlled Waters Name: Unknown Operator Property Type: Unknown Location: Location Description Not Available Authority: Environment Agency Welsh Region Pollutant: Light Oil Note: Not Given Incident Date: 9th February 1995 Incident Reference: 23086 Catchment Area: N/A Received Water: N/A Cause: Unknown Severity: Category 3 - Minor Incident	290	EA	270000 193500
6	Pollution Incident to Controlled Waters Name: Unknown Operator Property Type: Unknown Location: Tank Farm Authority: Environment Agency Welsh Region Pollutant: Unknown Note: Not Given Incident Date: 25th June 1996 Incident Reference: 28924 Catchment Area: N/A Received Water: N/A Cause: Unknown Severity: Category 3 - Minor Incident	940	EA	269000 192800
7	Pollution Incident to Controlled Waters Name: Unknown Operator Property Type: N/A Location: Opposite Blazers Caravans, Ewloe, Crymlyn Burrows, Swansea Authority: Environment Agency Welsh Region Pollutant: Crude Sewage Note: Mechanical/Electrical Plant Failure Incident Date: 10th October 1996 Incident Reference: 30444 Catchment Area: N/A Received Water: N/A Cause: Burst Severity: Category 1 - Major Incident	320	EA	269500 193200



Map ID	Details	Estimated Distance from Site	Source	NGR
11	Waste Transfer Site Licence Holder: Gower Chemicals Ltd Licence Reference: NBWD 6 Site: Crymlyn Burrows, Swansea, W Glam SA1 8PT Operator: Authority: Environment Agency - Welsh Region South West Area Site Category: Transfer Licence Status: Site is operational as far as is known Waste types on Site: Authorised waste: Ferric Chloride Max.Stor Prohibited waste: Elemental Sodium/Potassium Metal In Fine Powder Form Percussive/Explosive/Similar Waste Special Wastes N.O.S. Sub'S Control. Radioactive Subs Act'60 Waste Cont. Flam.Solvent (Exc.Petrol) Waste N.O.S.	450	EA	269400 193100
25	Planning Application (of possible contaminative use) Name: Filling Station Redevelopment Location: Llandarcy Filling Station, Jersey Marine, Swansea, West Glamorgan SA1 8QB Authority: Neath Port Talbot County Borough Council Description: Petrol Filling Stations Application Ref.: 95/0146/03 Dated 24th March 1995 Status: Detailed Plans Approved Site Area: n/a	580	LPR	270300 193000
26	Potentially Contaminative Industrial Use Name: Llandarcy Filling Station Jet Location: Fabian Way, Swansea, West Glamorgan SA1 8QB Classification: Fuel: retail sale of automotive fuel	590	Catalist Petroleum Station Database	270300 193000
27	Potentially Contaminative Industrial Use Name: Jeremy's Oil Distributors Ltd Location: Elba Crescent, Crymlyn Burrows, Swansea, West Glamorgan SA1 8QQ Classification: Wholesale non-agricultural intermediate products, inc. waste/scrap	510	Thomsons Trade Directory	270300 193100

**British Geological Survey Information Services Group**

Keyworth
Nottingham
Nottinghamshire
NG12 5GG

Telephone 0115 936 3100
Fax 0115 936 3200

Environment Agency - Welsh Region South West Area

Llys Afrom
Hawthorn Rise
Haverfordwest
Dyfed
SA61 2BQ

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Fax 01437 760881

Environment Agency Welsh Region

Rivers House
St Mellons Business Park
St Mellons
Cardiff
Mid Glamorgan
CF3 0LT

Telephone 01222 770088
Fax 01222 798555

Institute of Hydrology

Maclean Building
Crowmarsh Gifford
WALLINGFORD
Oxfordshire
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Fax 01491 692424

Neath Port Talbot County Borough Council

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Fax 01693 763444

Ordnance Survey

Romsey Road
SOUTHAMPTON
Hampshire
SO16 4GU

Telephone 01703 792000
Fax 01703 792404

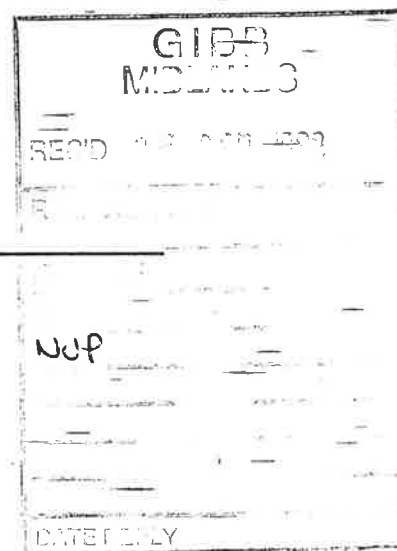
Report Reference: 12525-1**Site Address:** Freightliner Terminal Site, SWANSEA,**Company Name:****Grid Reference:** 269800 193300***EA (Water) Prosecutions***

The following company(s) have been prosecuted as shown below, however, from the information supplied, Landmark is unable to provide a National Grid Reference for the record(s).

Name	A J G I and Rosemary Matth
Address	Pennard Stream, SWANSEA, SA1
Authority	Environment Agency, Welsh Region
Details	EA Data. Other C.
Hearing Date	29-Mar-90
Verdict	Guilty
Fine	£450.00
Costs	£260.00

Name	Alberto Culver Co (UK) Limited
Address	River Tawe, SWANSEA, SA1
Authority	Environment Agency, Welsh Region
Details	EA Data. Industrial.
Hearing Date	16-Dec-94
Verdict	Guilty
Fine	£3,000.00
Costs	£391.98

Name	Alcoa Manufacturing (G.B.) Limited
Address	Trib of Gors Fawr Brook, SWANSEA, SA1
Authority	Environment Agency, Welsh Region
Details	EA Data. Oil.
Hearing Date	01-Jul-94
Verdict	Guilty
Fine	£2,000.00
Costs	£1,803.35



Name	BP Oil Llandarcy Refinery
Address	Queens Dock, SWANSEA, SA1
Authority	Environment Agency, Welsh Region
Details	EA Data. Industrial oil.
Hearing Date	30-Jun-93
Verdict	Guilty
Fine	£2,000.00
Costs	£600.00

Name	British Electrical Repairs Limited
Address	River Tawe, SWANSEA, SA1
Authority	Environment Agency, Welsh Region
Details	EA Data. Industrial.
Hearing Date	16-Dec-94
Verdict	Guilty
Fine	£3,000.00
Costs	£345.50

Name	Dwr Cymru Cyf
Address	Unnamed tributary of Parkmill Stream, SWANSEA, SA1
Authority	Environment Agency, Welsh Region
Details	EA Data. Sewage.
Hearing Date	06-Sep-91
Verdict	Guilty
Fine	£600.00
Costs	£540.00

Name	Ethnic Cuisine Limited
Address	Nant-y-Ffin, Viking Way, Winch Wen Industrial Estate, Winch Wen, SWANSEA, West Glamorgan, SA1 7DA
Authority	Environment Agency, Welsh Region
Details	Environment Times Vol.4 Issue 3, For polluting the Nant-y-Ffin and the Nant Fenfrod Lake with vegetable oil after a spillage from the company's effluent treatment plant.
Hearing Date	05-Feb-98
Verdict	Guilty
Fine	£7,500.00
Costs	£500.00

Name	Swansea City Council
Address	Glan-Y-Wern Canal and Crymlyn Bog SSSI, SWANSEA, SA1
Authority	Environment Agency, Welsh Region
Details	EA Data. Other.
Hearing Date	31-Oct-90
Verdict	Guilty
Fine	£2,000.00
Costs	£750.00

Name	W E Dowds
Address	Trib of Gors Fawr Brook, SWANSEA, SA1
Authority	Environment Agency, Welsh Region
Details	EA Data. Oil.
Hearing Date	01-Jul-94
Verdict	Guilty
Fine	£2,000.00
Costs	£1,803.35

Name	Welsh Water
Address	Ystalyfera, SWANSEA, SA
Authority	Environment Agency, Welsh Region
Details	ENDS Report; 282; p.56. Guilty of 8 charges of supplying water unfit for human consumption to addresses in Swansea Area. Some 18,000 people affected in Ystalyfera area. Customers complained of burning sensation in throat, diarrhoea, stomach cramps.
Hearing Date	15-Jul-98
Verdict	Guilty
Fine	£24,000.00
Costs	£7,960.00

Current Trade Directory Search

The following company(s) have been identified as possible contaminative premises as shown below, however, from the information supplied, Landmark is unable to provide a National Grid Reference for the record(s).

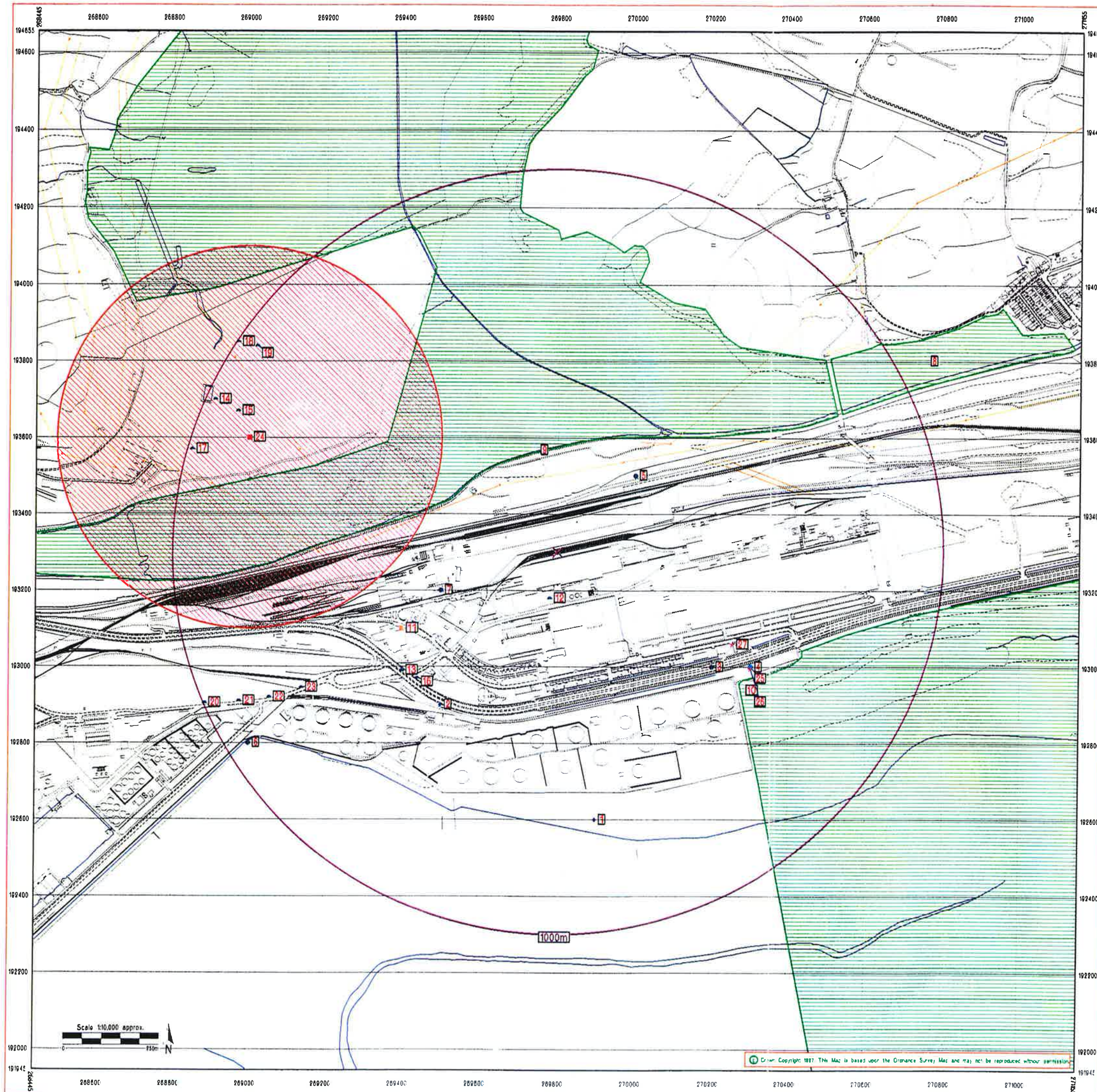
Name	Princess Service Station
Address	York Street, SWANSEA, West Glamorgan, SA1 3LZ
Classification	Fuel: retail sale of automotive fuel
Data Source	Petroleum Station Database
Source Date	30-Sep-97

Name Shooters Of Swansea
Address Regional Sports Centre, Upper Banc, SA1 7DS
Classification Weapons & ammunition [manufacture and storage]
Data Source Trade Directory
Source Date 26-May-95

Name SOUTH WALES SAND & GRAVEL
Address Prince of Wales Dock, Langdon Road, Swansea, West Glamorgan, SA1 8RQ
Classification Quarrying of sand & clay, operation of sand & gravel pits
Data Source Trade Directory
Source Date 01-Mar-97

Name THE FORGE
Address Alexandra Road, Swansea, West Glamorgan, SA1 5EE
Classification Metals: precious & non-ferrous metal manufacture
Data Source Trade Directory
Source Date 01-Mar-97

Name Ward Bros Mining Ltd
Address Nanthir Colliery, SA1 1PC
Classification Mining of coal & lignite
Data Source Trade Directory
Source Date 26-May-95



EnviroCheck

Environmental Site Sensitivity Data

CLIENT DETAILS

Order No. ES12525-1

Customer Ref: Neil Parry, NVP/J410/P5174/355/
Gibb Ltd
Development: House Road End Road
Oldbury
Warley B69 4HW

SITE DETAILS

Grid Reference 269800 193300

Freightliner Terminal Site

SWANSEA

KEY TO THE LEGEND DATABASE

SITE SETTING

- × Specified Site
- Buffer
- 8 Reference Number
- Several of Type at Location
- ⚡ Pylon or Mast

ENVIRONMENTAL SETTING

- Landfill
- BGS Recorded Landfill Site
- BGS Recorded Mineral Site
- BGS Borehole
- River Network and Water Feature
- Water Abstraction
- Discharge Consent
- Site of Special Scientific Interest

INDUSTRIAL SETTING

- Integrated Pollution Control
- Air Pollution Control
- Red List Discharge Consent
- Enforcement or Prohibition Notice
- Prosecution Relating to Authorised Process
- Registered Radioactive Substance
- Planning Application (of Possible Contaminative Use)
- Waste Treatment or Disposal Site
- Waste Transfer Site
- Integrated Pollution Control Registered Waste Site
- Planning Hazardous Substance Consent
- Planning Hazardous Substance Enforcement
- Potentially Contaminative Use
- Prosecution Relating to Controlled Waters
- Pollution Incident Relating to Controlled Waters

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British
Geological
Survey

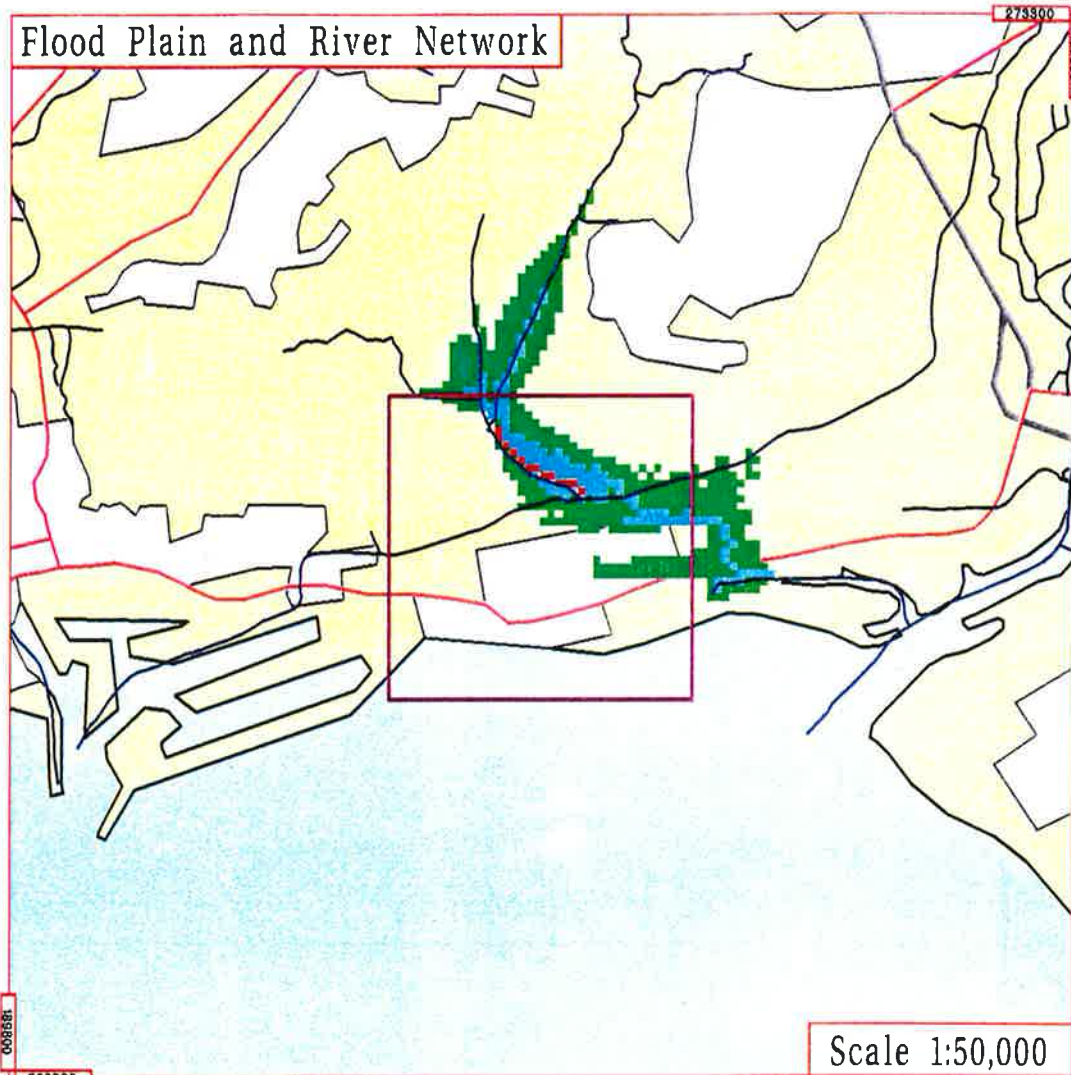
Value Added Reseller



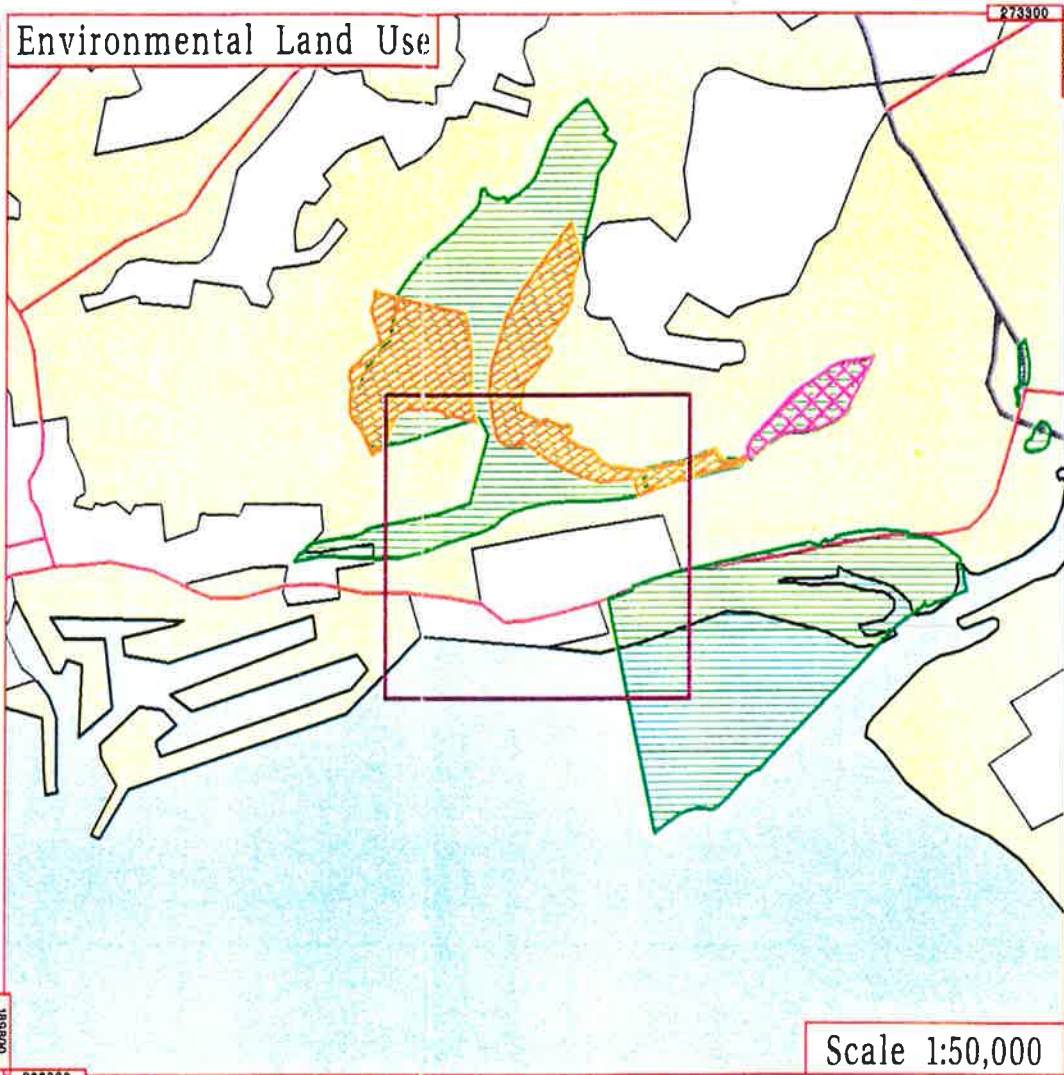
Value Added Reseller

Produced by Landmark Information Group Limited. Tel: 01392 441729 Fax: 01392 441709

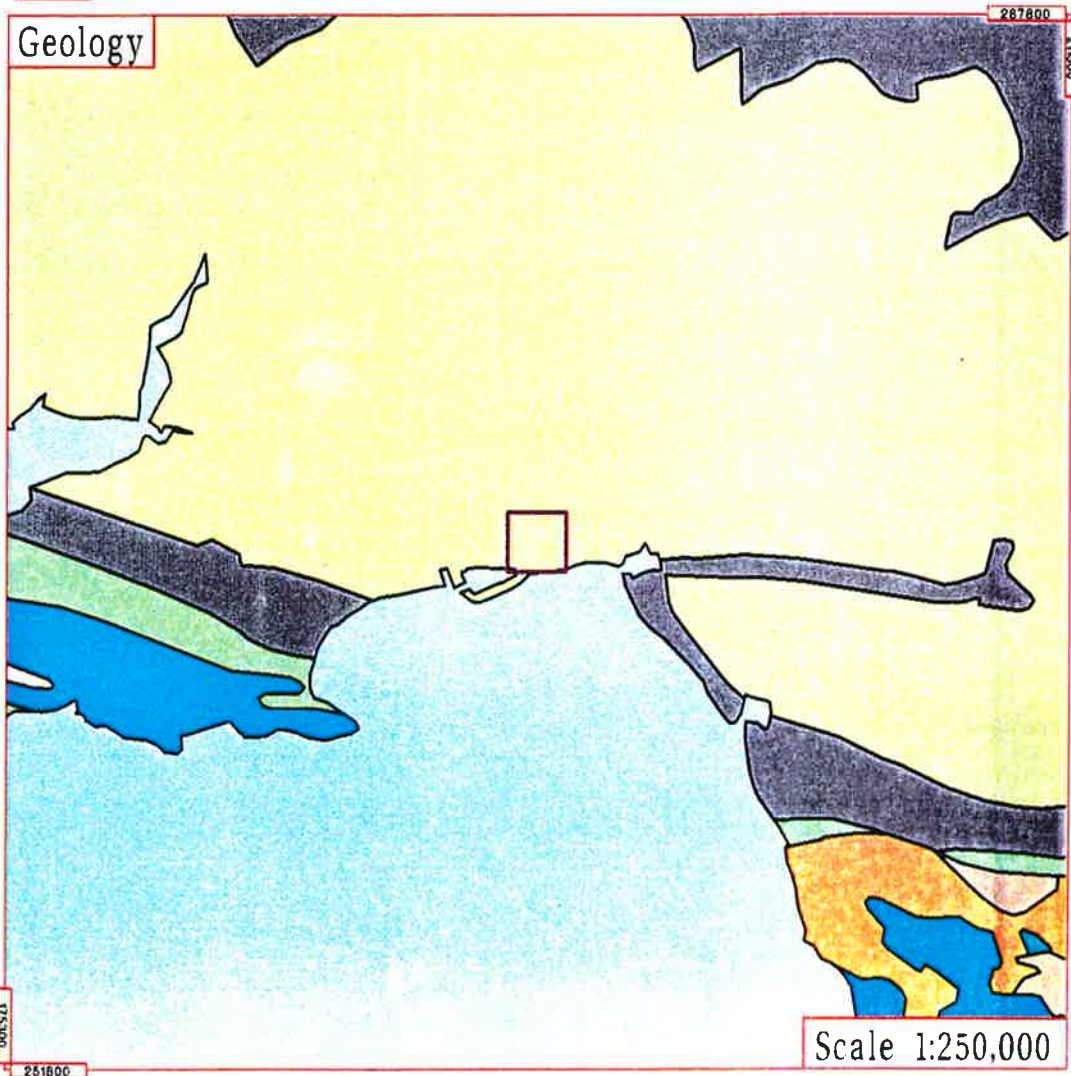
Flood Plain and River Network



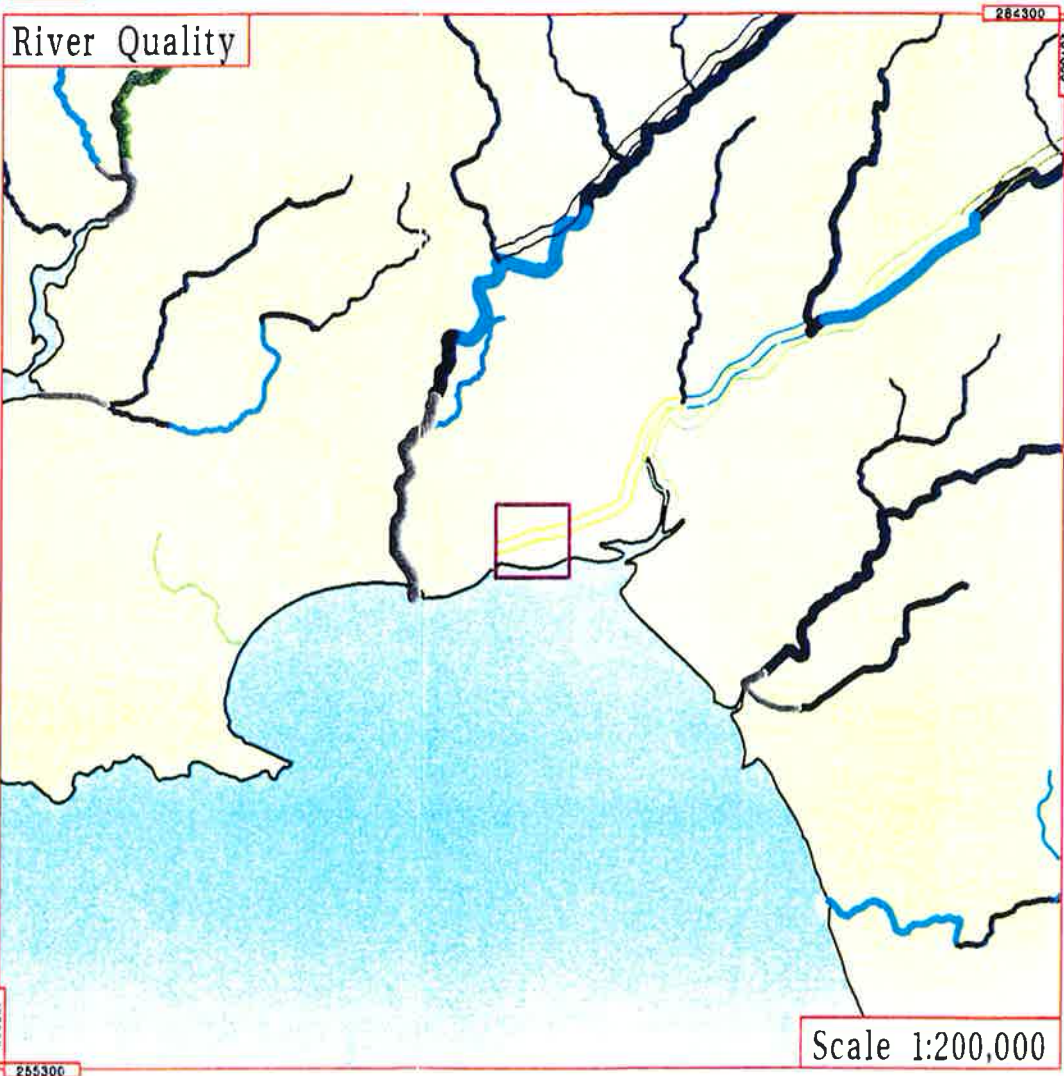
Environmental Land Use



Geology



River Quality



EnviroCheck

Environmental Site Sensitivity Data

CLIENT DETAILS

Order No. ES12525-1

Customer Ref: Neil Parry, NVP/J410/P5174/355/
Gibb Ltd
Development House Road End Road
Oldbury
Warrley B69 4HW

SITE DETAILS

Grid Reference 269800 193300

Freightliner Terminal Site

SWANSEA

General Legend

Urban Areas Motorways 'A' Roads Extent of Search

Guide to the Flood Plain and River Network Map

0 - 1 m estimated 100 yr flood depth 1 - 2 m estimated 100 yr flood depth over 2 m estimated 100 yr flood depth River Network and Water Feature

The flooded areas have been generated using a generalised technique and should not, by themselves, be used to infer that specific areas are or are not at risk of inundation. Flood risk at any specific location may be influenced by local factors - not least flood defences - that have not been taken into account.

Guide to the Environmental Landuse Map

Area of Outstanding Natural Beauty Nitrate Sensitive Area Nitrate Vulnerability Zone National Nature Reserve Local Nature Reserve Marine Nature Reserve Site of Special Scientific Interest Environmentally Sensitive Area Forest Park National Park

Guide to the Geology Map

Lower Lias Tournaisian and Viséan (Carboniferous Limestone Series) Triassic mudstones (including Keuper Marl, Dolomitic and Rhaetic) CAMBRIAN Lower Old Red Sandstone, including Downland Nemurian (Millstone Grit Series) Lower Westphalian (mainly Productive Coal Measures) Upper Old Red Sandstone and Upper Devonian Upper Westphalian (including Pennant Measures)

Guide to the River Quality Map

River Quality A River Quality B River Quality C River Quality D Canal Quality A Canal Quality B Canal Quality C Canal Quality E Canal Quality D Canal Quality C Unclassified Tidal River Unclassified River Sea



Produced by Landmark Information Group Limited. Tel: 01392 441729 Fax: 01392 441709

APPENDIX C

HISTORICAL MAPS

EnviroCheck Report on:

Freightliner Terminal Site
SWANSEA

National Grid Reference :

269800, 193300

Prepared For :

Gibb Ltd
Development House
Rood End Road
Oldbury
Worley
B69 4HW

Your Reference :

Neil Parry, NVP/J410/P5174/355/

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**Ordnance Survey County Series Published 1884**

County	Mapsheet	Scale	Year
Glamorganshire	024_00	1:10,560	1884

Ordnance Survey County Series Published 1900

County	Mapsheet	Scale	Year
Glamorganshire	024_NW	1:10,560	1900
Glamorganshire	024_NE	1:10,560	1900
Glamorganshire	024_SE	1:10,560	1900
Glamorganshire	024_SW	1:10,560	1900

Ordnance Survey County Series Published 1921

County	Mapsheet	Scale	Year
Glamorganshire	024_NW	1:10,560	1921
Glamorganshire	024_NE	1:10,560	1921
Glamorganshire	024_SW	1:10,560	1921
Glamorganshire	024_SE	1:10,560	1921

Ordnance Survey County Series Published 1938 to 1951

County	Mapsheet	Scale	Year
Glamorganshire	024_NW	1:10,560	1938
Glamorganshire	024_NE	1:10,560	1938
Glamorganshire	024_SW	1:10,560	1938
Glamorganshire	024_SE	1:10,560	1951

Ordnance Survey Plan Published 1964

National Grid Series	Mapsheet	Scale	Year
Sheet	SS69SE	1:10,560	1964
Sheet	SS79SW	1:10,560	1964



Ordnance Survey Plan Published 1979 to 1980

National Grid Series	Mapsheet	Scale	Year
Sheet	SS69SE	1:10,000	1979
Sheet	SS79SW	1:10,000	1980

Ordnance Survey Plan Published 1980 to 1989

National Grid Series	Mapsheet	Scale	Year
Sheet	SS79SW	1:10,000	1980
Sheet	SS69SE	1:10,000	1989



EnviroCheck Report on:

Freightliner Terminal Site
SWANSEA

National Grid Reference :

269800, 193300

Prepared For :

Gibb Ltd.
Development House
Rood End Road
Oldbury
Warley
B69 4HW

Your Reference :

Neil Parry, NVP/J410/P5174/355/

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Ordnance Survey County Series Published 1899

County	Mapsheet	Scale	Year
Glamorganshire	024_06	1:2,500	1899
Glamorganshire	024_07	1:2,500	1899

Ordnance Survey County Series Published 1917 to 1919

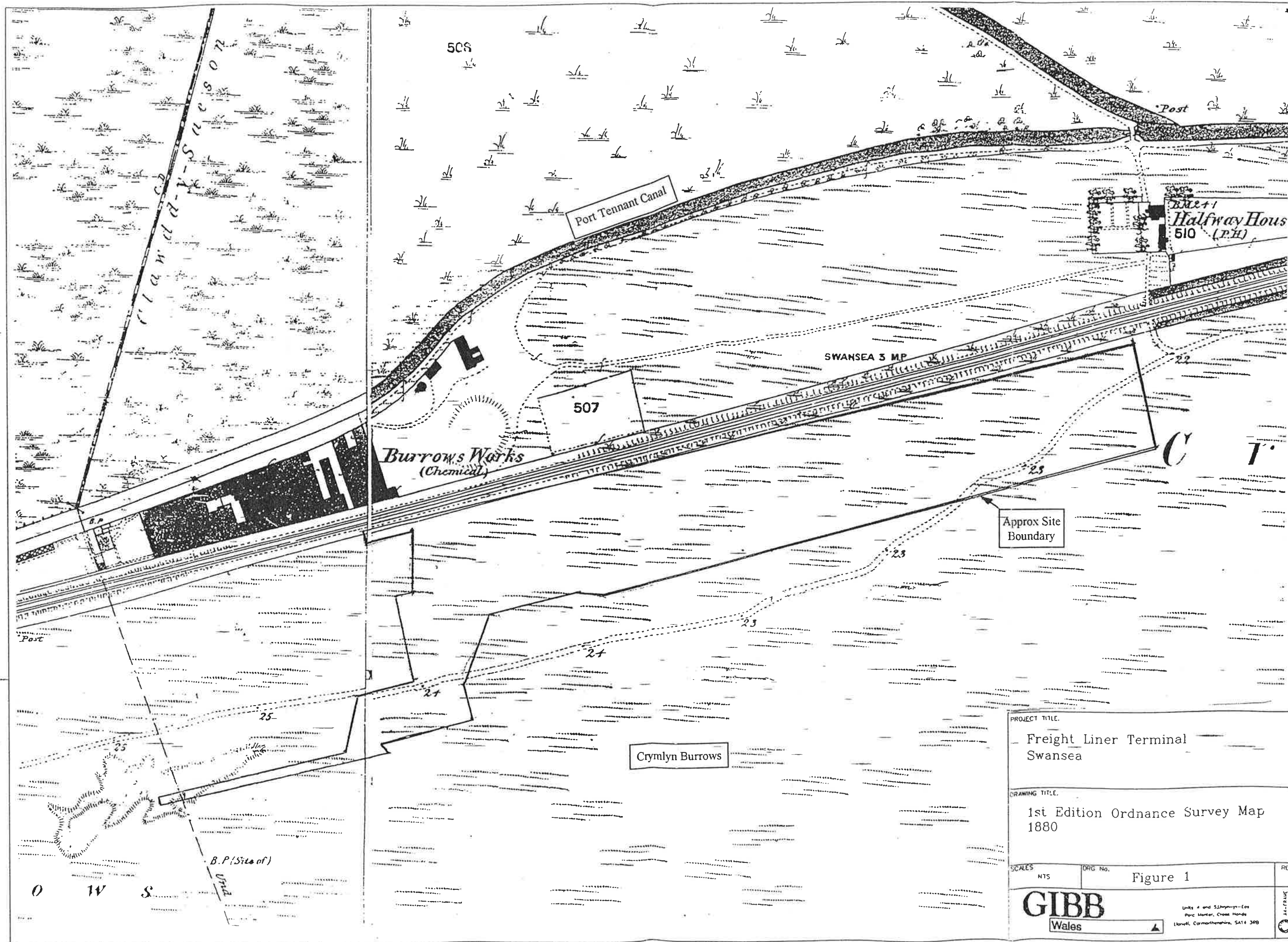
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Glamorganshire	024_06	1:2,500	1919

Ordnance Survey County Series Published 1941

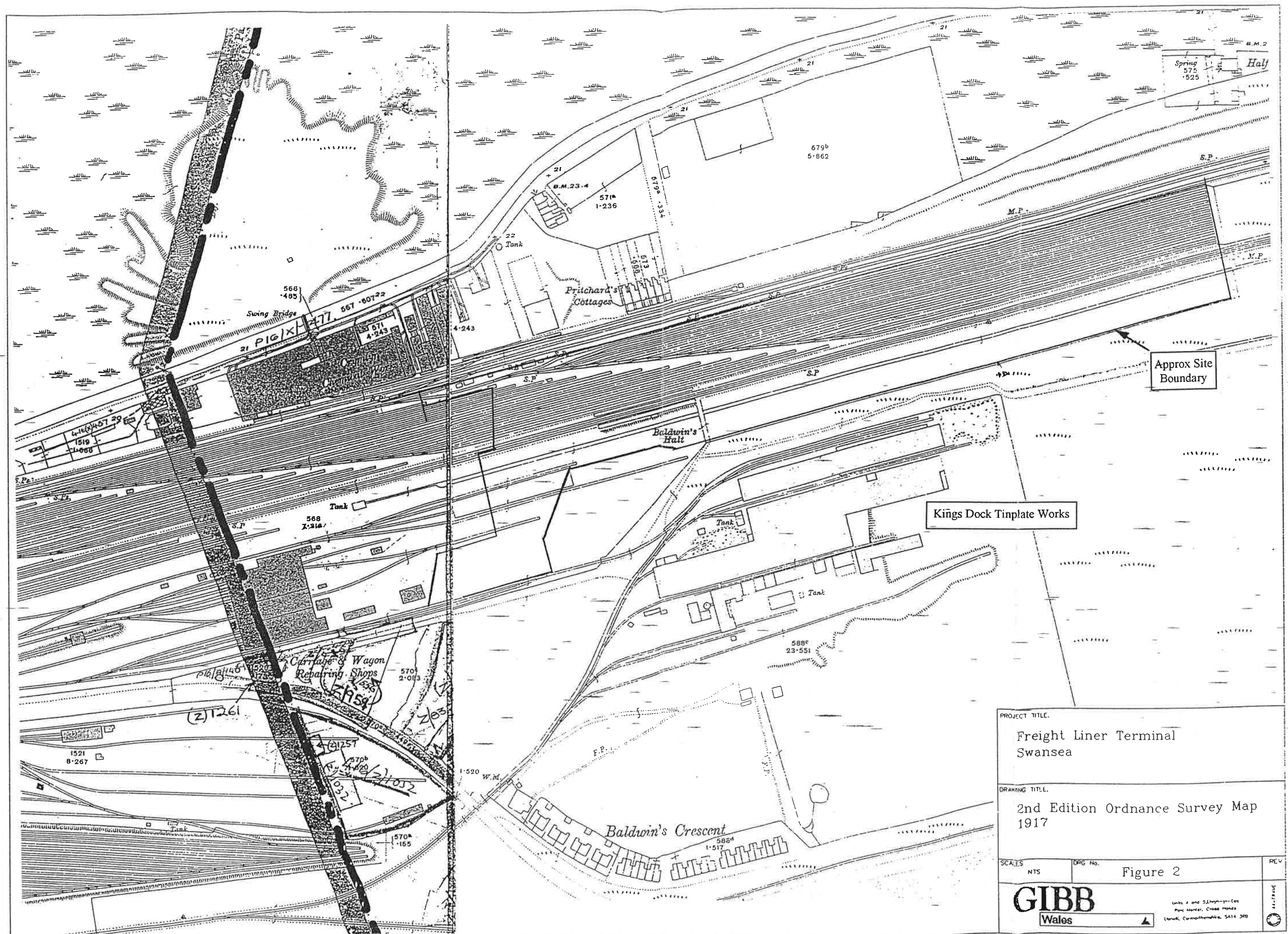
County	Mapsheet	Scale	Year
Glamorganshire	024_07	1:2,500	1941

APPENDIX C

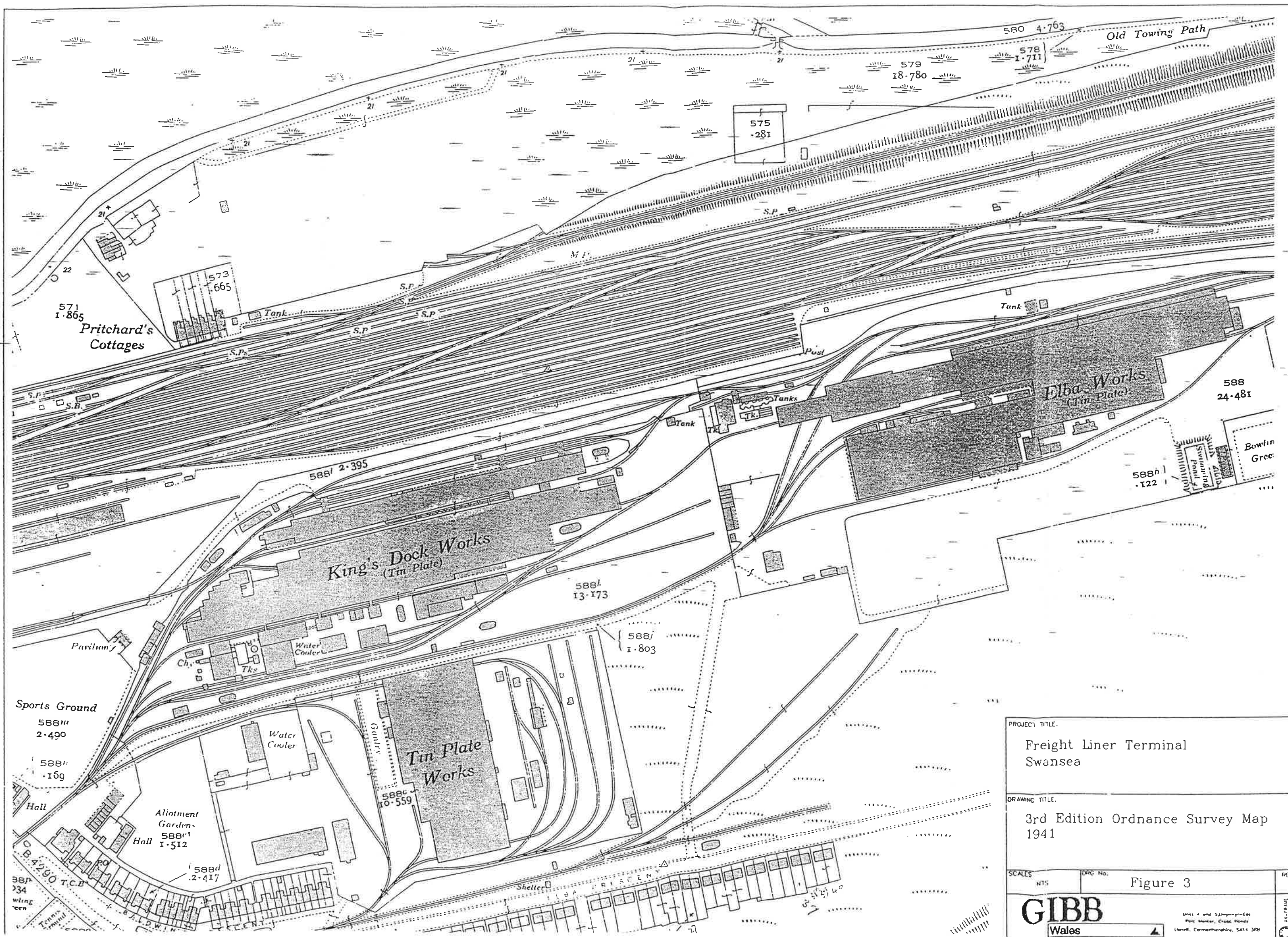
HISTORICAL MAPS



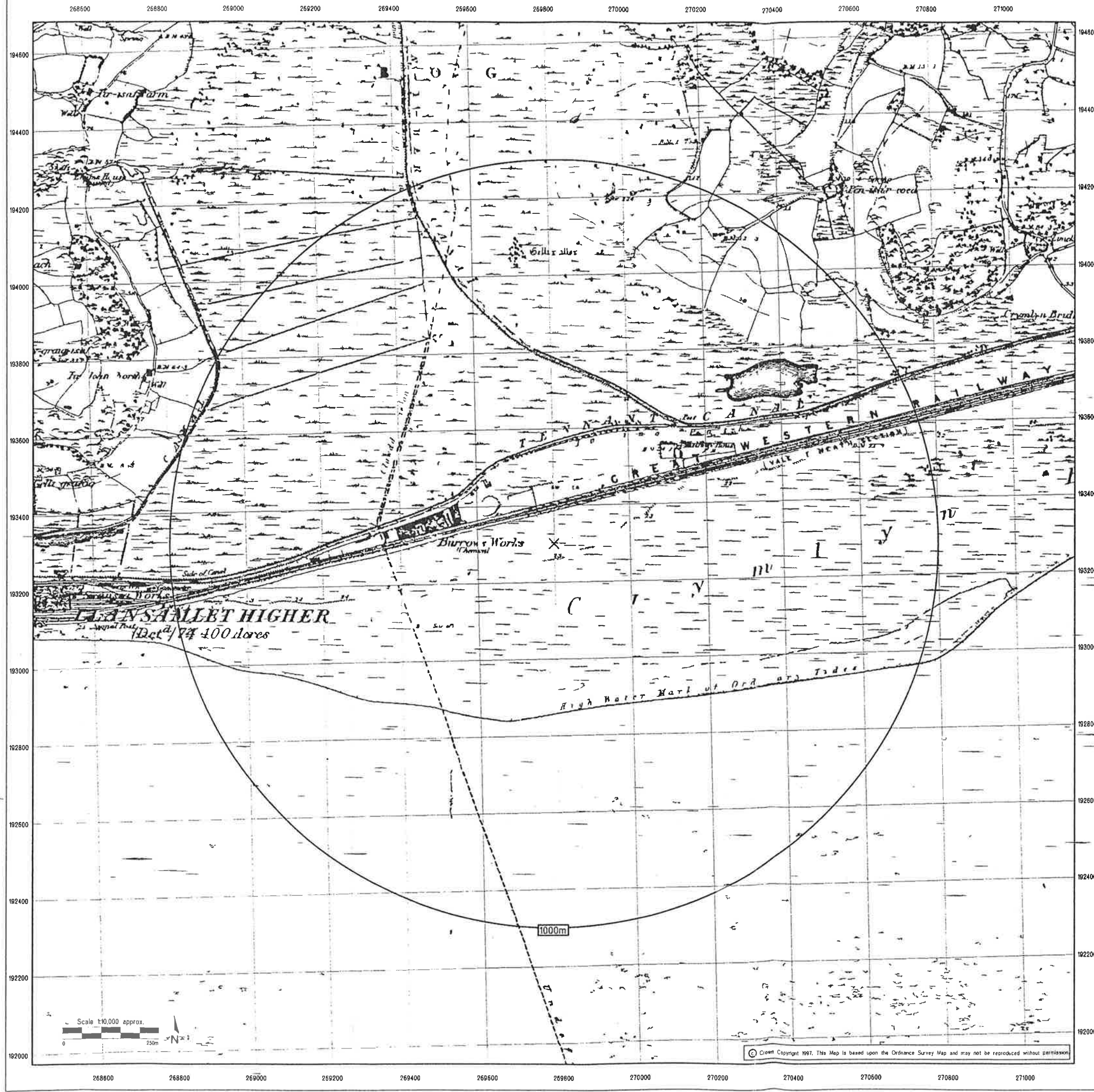
PROJECT TITLE	
Freight Liner Terminal Swansea	
DRAWING TITLE	
1st Edition Ordnance Survey Map 1880	
SCALES	REV
NTS	REV
Figure 1	
GIBB Wales	
Units 4 and 5, Stryker Road Park View, Cross Hands Llanelli, Carmarthenshire, SA14 3PB	



PROJECT TITLE.		
Freight Liner Terminal Swansea		
DRAWING TITLE.		
2nd Edition Ordnance Survey Map 1917		
SCALE	DRG No.	REV
NTS	Figure 2	
GIBB Wales		Units 4 and 5, Llyn-y-Cos Pont ap Iwan, Cross Roads Llanelli, Carmarthenshire, SA14 3JY



PROJECT TITLE.			
Freight Liner Terminal Swansea			
DRAWING TITLE.			
3rd Edition Ordnance Survey Map 1941			
SCALES		FIG. No.	REV
NTS		Figure 3	
GIBB			
Wales			
Units 4 and 5, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49, 50, 51, 52, 53, 54, 55, 56, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100			



EnviroCheck

Environmental Site Sensitivity Data

CLIENT DETAILS Order No. EH12525-1
Customer Ref: Neil Parry, NVP/J410/P5174/355/
Gibb Ltd
Development House Road End Road
Oldbury
Warley B69 4HW

SITE DETAILS Grid Reference 269800 193300
Freightliner Terminal Site
SWANSEA

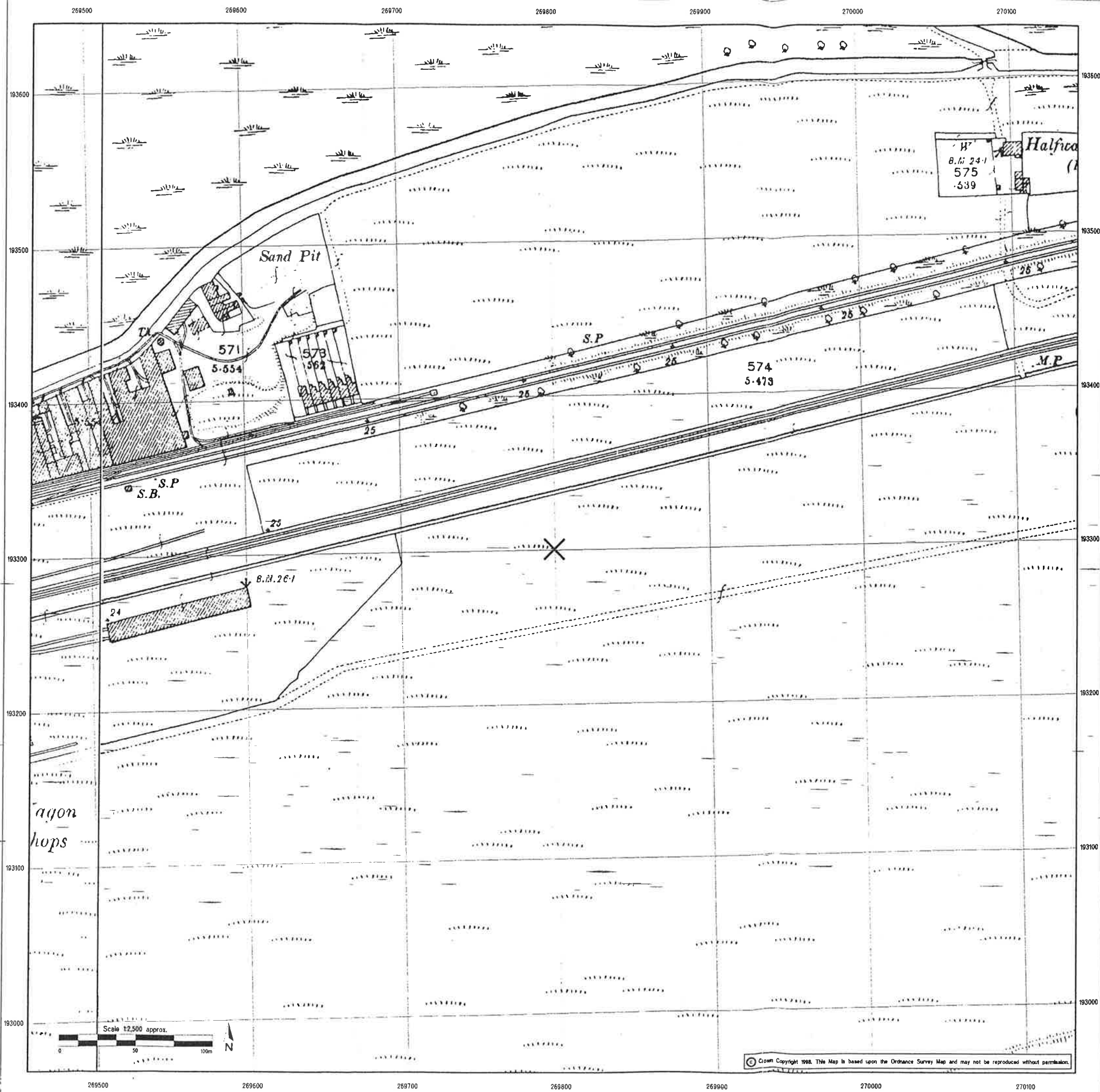
Historical Map Legend

Quarry	Shingle	Railway over Road	Road over Railway
Gravel Pit	Sand Pit	Level Crossing	Railway over River
Other Pits		Road over River or Canal	Road over Stream
Mixed Wood	Rough Pasture	Road over Stream	
Marsh		Sunken Road	Raised Road
Arrow denotes flow of water		Sketched Contour	Instrumental Contour

GLAMORGANSHIRE county
The historical maps shown were reproduced from maps predominantly laid at the scale adopted for England, Wales and Scotland is the 1840's. In 1854 the 1:2,500 scale was adopted for mapping urban areas; these maps were used to update the 1:10,000 maps. The published date given on the right therefore is often some years later than the surveyed date. Before 1938, all OS maps were based on the Cassini Projection, with independent surveys of a single county or group of counties, giving rise to significant inaccuracies in outlying areas. In the late 1940's, a Provisional Edition was produced, which updated the 1:10,000 mapping from a number of sources. The maps appear unfinished - with all military camps and other strategic sites removed. These maps were initially overprinted with the National Grid. In 1970, the first 1:10,000 maps were produced using the Transverse Mercator Projection. The revision process continued until recently, with new editions appearing every 10 years or so for urban areas.

1884

Date(s) of Publication



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Gibb Ltd
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Oldbury
Warley B69 4HW

SITE DETAILS Grid Reference 269800 193300
Freightliner Terminal Site

SWANSEA

Historical Map Legend

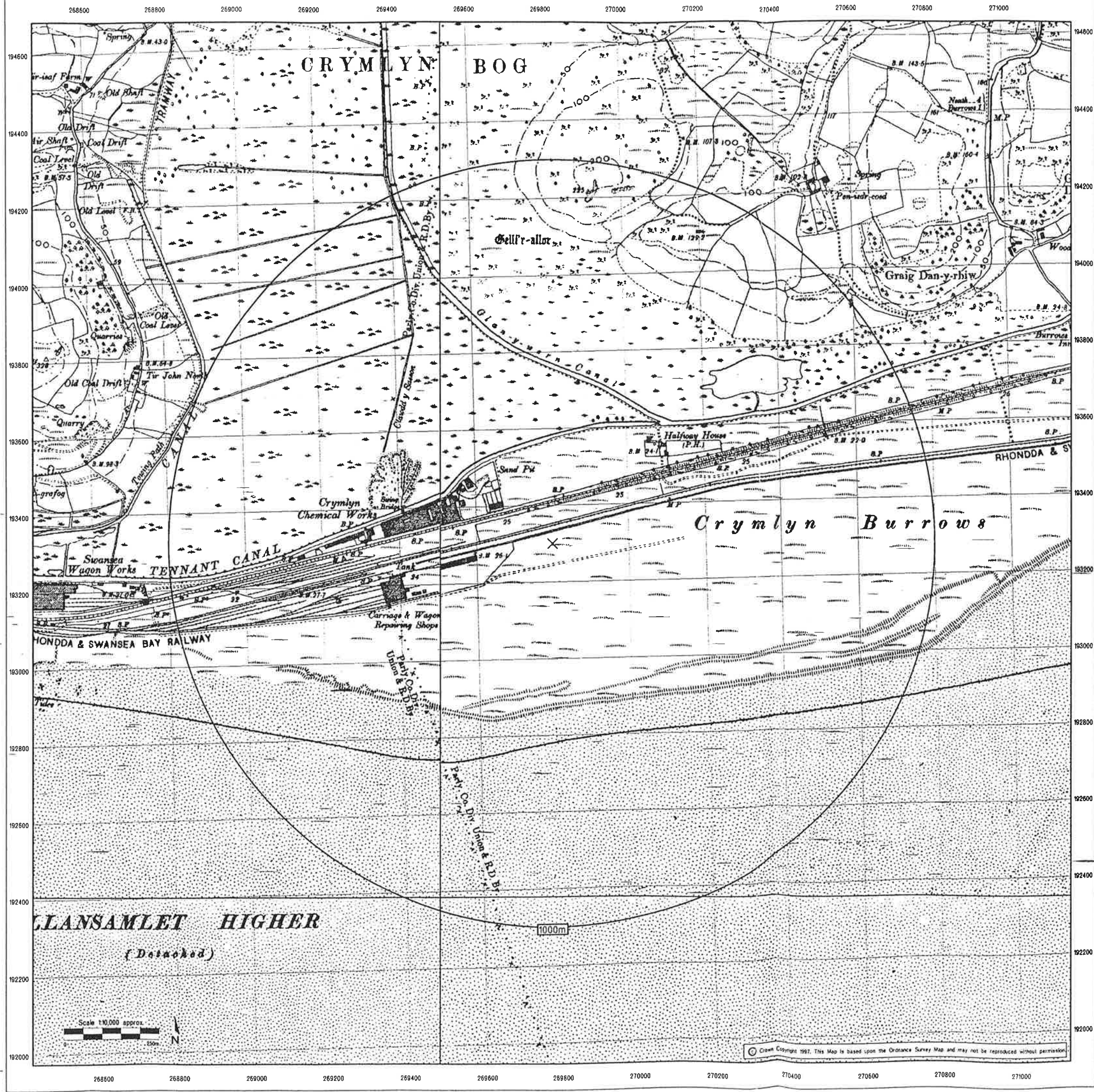
Quarry	Shingle	Railway over Road	Road over Railway
Gravel Pit	Sand Pit	Level Crossing	Railway over River
Other Pits	Road over River or Canal	Road over Stream	Sunken Road
Mixed Wood	Rough Pasture	Road over Stream	Raised Road
Marsh	Sketched Contour	Instrumental Contour	

Arrow denotes flow of water

Glamorganshire

The historical maps shown were reproduced from maps predominantly held at the scale adopted for England, Wales and Scotland in the 1840's. In 1854 the 1:25,000 scale was adopted for mapping urban areas and by 1896 it covered the whole of what were considered to be the cultivated parts of Great Britain. The published date given on the right is often some years later than the surveyed date. Before 1938, all OS maps were based on the Cassini Projection, with independent surveys of a single county or group of counties, giving rise to significant inaccuracies in outlying areas.

1899



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Environmental Site Sensitivity Data

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Gibb Ltd
Development: House Road End Road
Oldbury
Warley B69 4HW

SITE DETAILS Grid Reference 269800 193300
Freightliner Terminal Site

SWANSEA

Historical Map Legend

++++> Arrow denotes flow of water

GLAMORGANSHIRE county
The historical maps shown were reproduced from maps predominantly held at the scale adopted for England, Wales and Scotland in the 1840's. In 1854 the 1:25,000 scale was adopted for mapping urban areas; these maps were used to update the 1:10,000 maps. The published date given on the right therefore is often some years later than the surveyed date. Before 1938, all OS maps were based on the Cassini Projection, with independent surveys of a single county or group of counties, giving rise to significant inaccuracies in outlying areas.

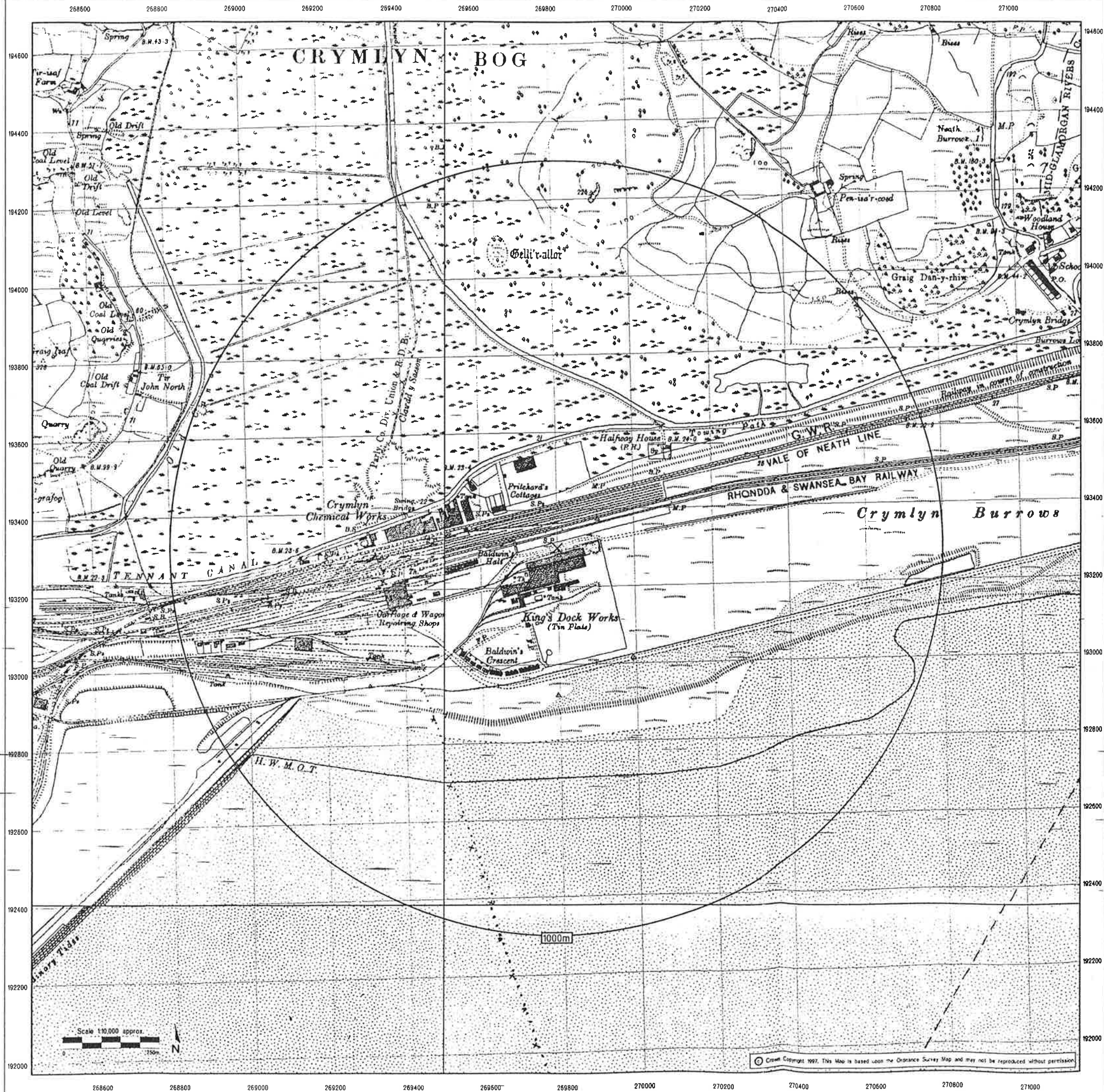
In the late 1940's a Provisional Edition was produced, which updated the 1:10,000 mapping from a number of sources. The maps appear unfinished - with all military camps and other strategic sites removed. These maps were initially overprinted with the National Grid. In 1970, the first 1:10,000 maps were produced using the Transverse Mercator Projection. The revision process continued until recently, with new editions appearing every 10 years or so for urban areas.

1900	1900
1900	1900

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Warley B69 4HW

SITE DETAILS Grid Reference 269800 193300
Freightliner Terminal Site

SWANSEA

Historical Map Legend

Quarry	Shingle	Railway over Road	Road over Railway
Gravel Pit	Sand Pit	Level Crossing	Railway over River
Other Pits		Road over River or Canal	Road over Stream
Mixed Wood	Rough Pasture	Road over Stream	
Marsh		Sunken Road	Raised Road
		Sketched Contour	Instrumental Contour

→ Arrow denotes flow of water

GLAMORGANSHIRE county
The historical maps shown were reproduced from maps predominantly held at the scale adopted for England, Wales and Scotland in the 1840's. In 1854 the 1:2500 scale was adopted for mapping urban areas; these maps were used to update the 1:10,560 maps. The published date given on the right therefore is often some years later than the surveyed date. Before 1938, all OS maps were based on the Cassini Projection, with independent surveys of a single county or group of counties, giving rise to significant inaccuracies in outlying areas.

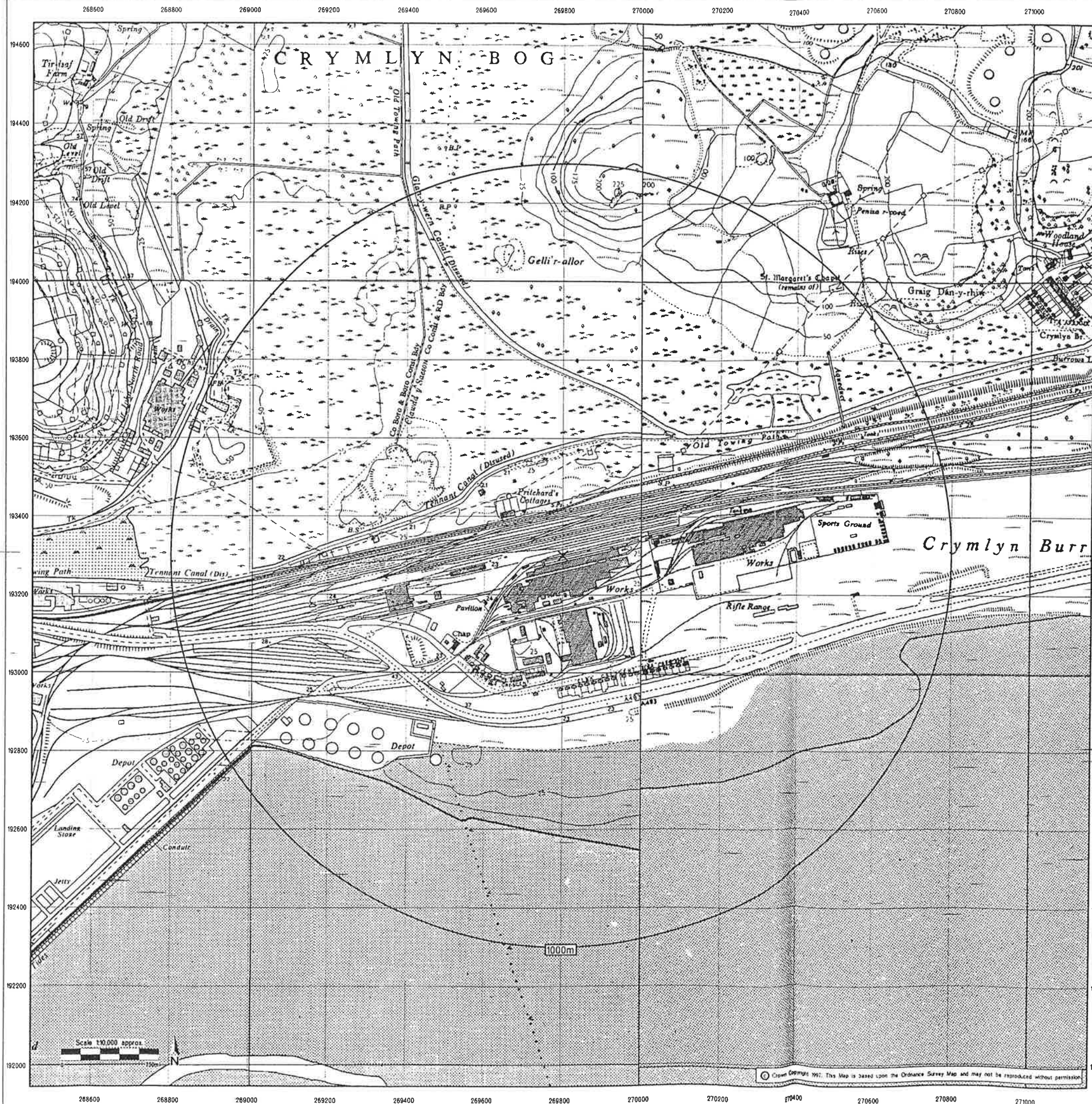
In the late 1940's, a Provisional Edition was produced, which updated the 1:10,560 mapping from a number of sources. The maps appear unfinished - with all military camps and other strategic sites removed. These maps were initially overprinted with the National Grid. In 1970, the first 1:10,000 maps were produced using the Transverse Mercator Projection. The revision process continued until recently, with new editions appearing every 10 years or so for urban areas.

1921	1921
1921	1921

Date(s) of Publication

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Warley B69 4HW

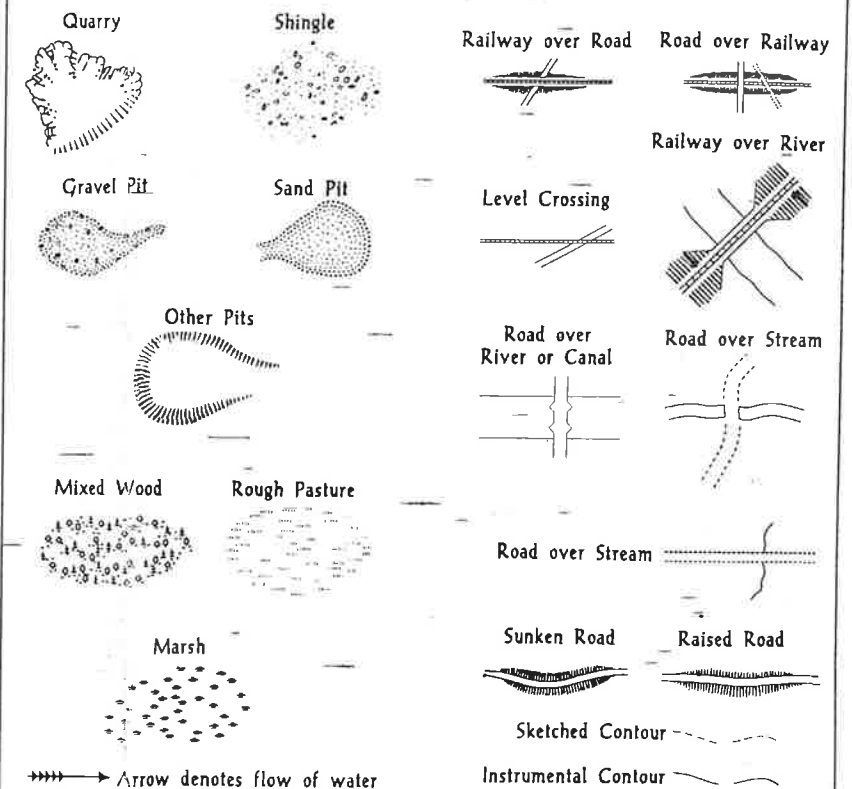
SITE DETAILS

Grid Reference 269800 193300

Freightliner Terminal Site

SWANSEA

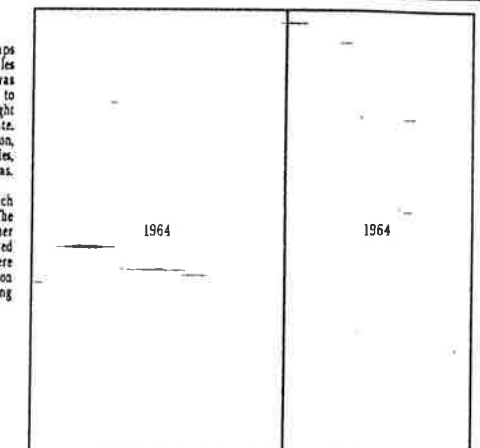
Historical Map Legend



Ordnance Survey Plan

The historical maps shown were reproduced from maps predominantly held at the scale adopted for England, Wales and Scotland in the 1840s. In 1854 the 1:25,000 scale was adopted for mapping urban areas; these maps were used to update the 1:25,000 maps. The published date given on the right therefore is often some years later than the surveyed date. Before 1936, all OS maps were based on the Cassini Projection, with independent surveys of a single county or group of counties, giving rise to significant inaccuracies in outlying areas.

In the late 1940s, a Provisional Edition was produced, which updated the 1:25,000 mapping from a number of sources. The maps appear unfinished - with all military camps and other strategic sites removed. These maps were initially overprinted with the National Grid. In 1970, the first 1:10,000 maps were produced using the Transverse Mercator Projection. The revision process continued until recently, with new editions appearing every 10 years or so for urban areas.



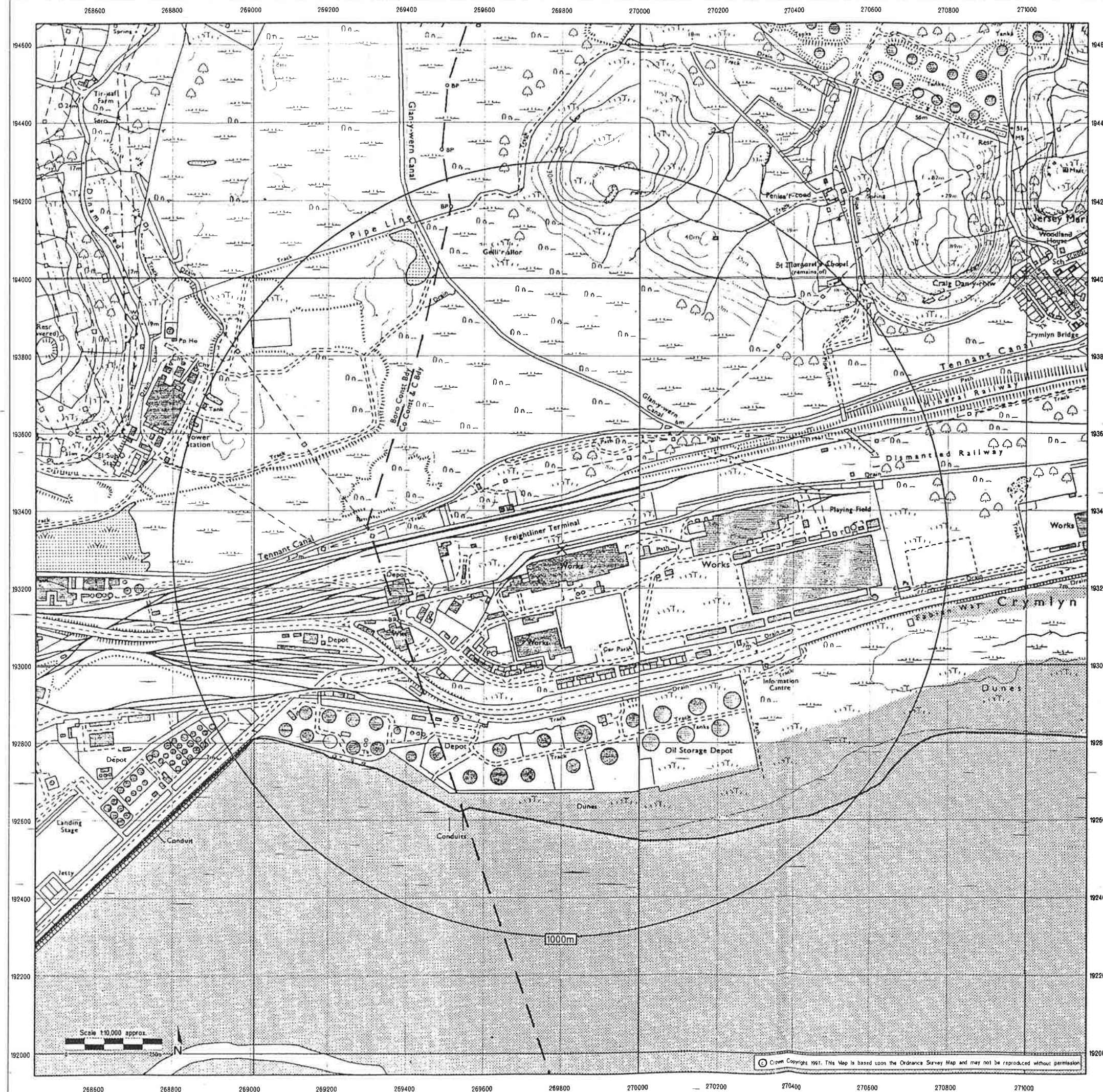
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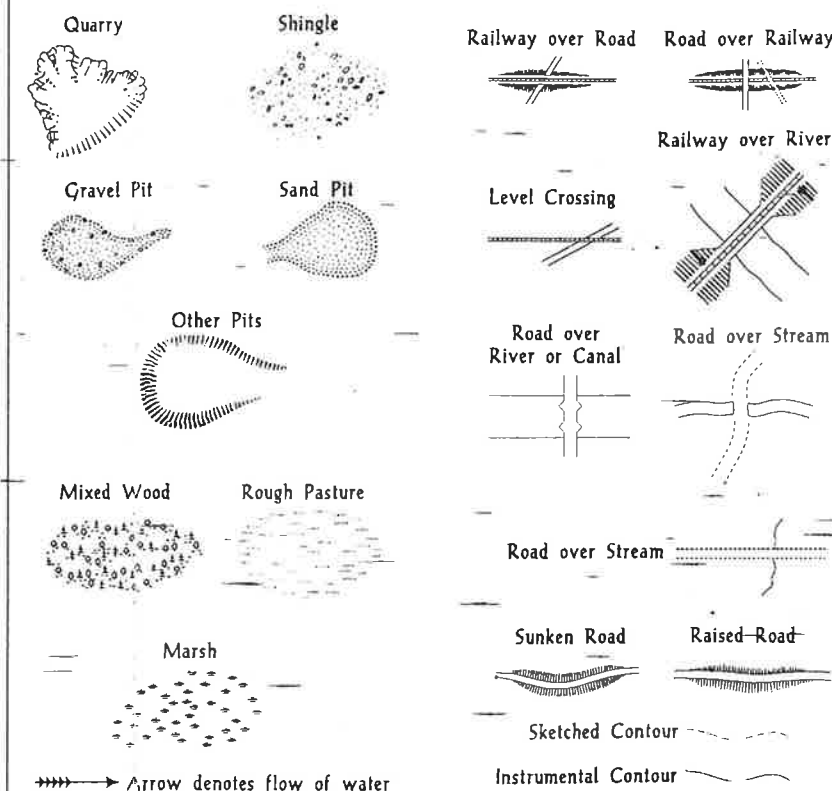
SITE DETAILS

Grid Reference 269800 193300

Freightliner Terminal Site

SWANSEA

Historical Map Legend



Ordnance Survey Plan

The historical maps shown were reproduced from maps predominantly held at the scale adopted for England, Wales and Scotland in the 1840's. In 1854 the 1:2,500 scale was adopted for mapping urban areas; these maps were used to update the 1:10,560 maps. The published date given on the right therefore is often some years later than the surveyed date. Before 1938, all OS maps were based on the Cassini Projection, with independent surveys of a single county or group of counties, giving rise to significant inaccuracies in outlying areas.

In the late 1940's a Provisional Edition was produced, which updated the 1:10,560 mapping from a number of sources. The maps appear unfinished - with all military camps and other strategic sites removed. These maps were initially overprinted with the National Grid. In 1970, the first 1:10,000 maps were produced using the Transverse Mercator Projection. The revision process continued until recently, with new editions appearing every 10 years or so for urban areas.

1979

1980

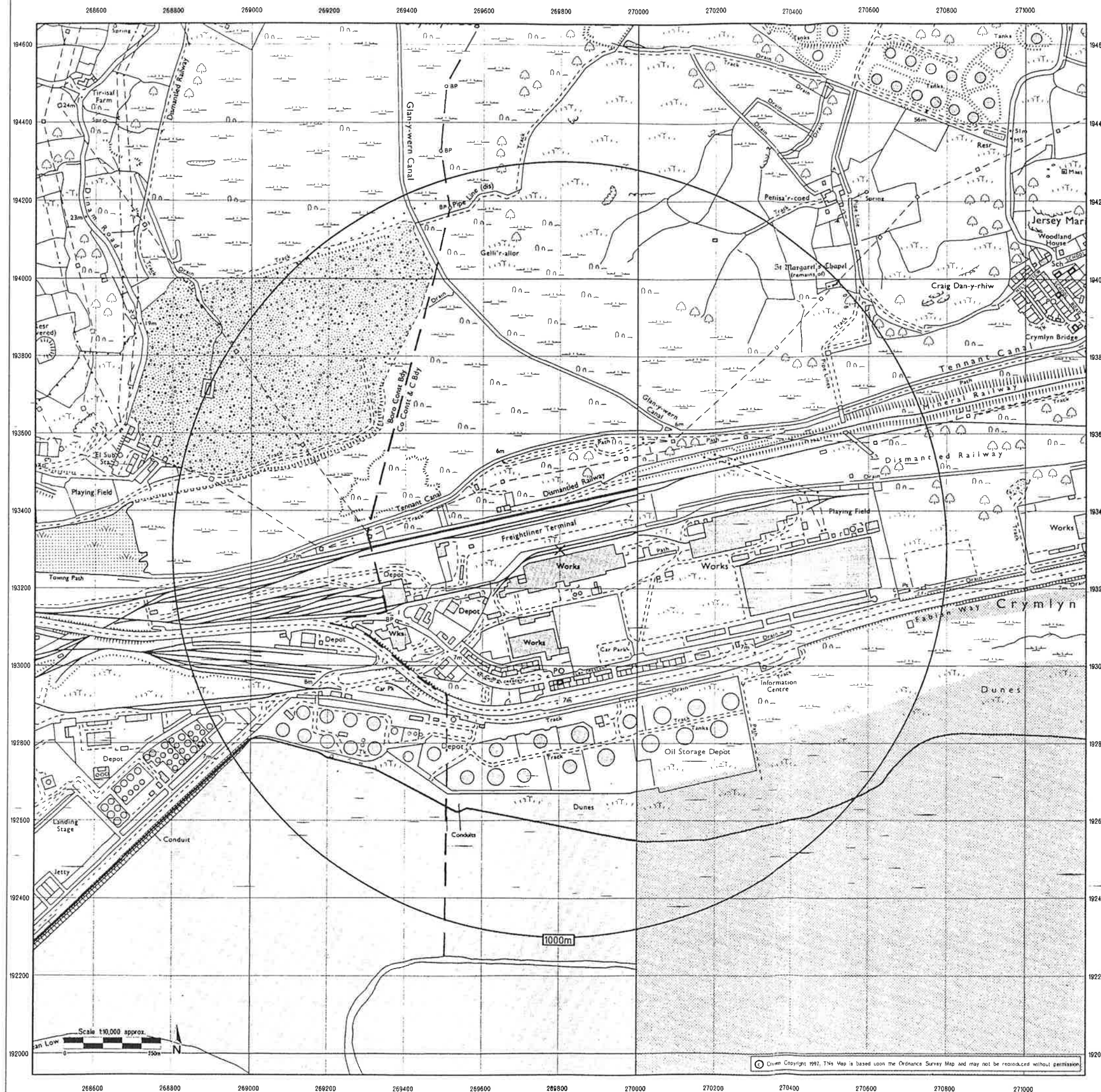
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Environmental Site Sensitivity Data

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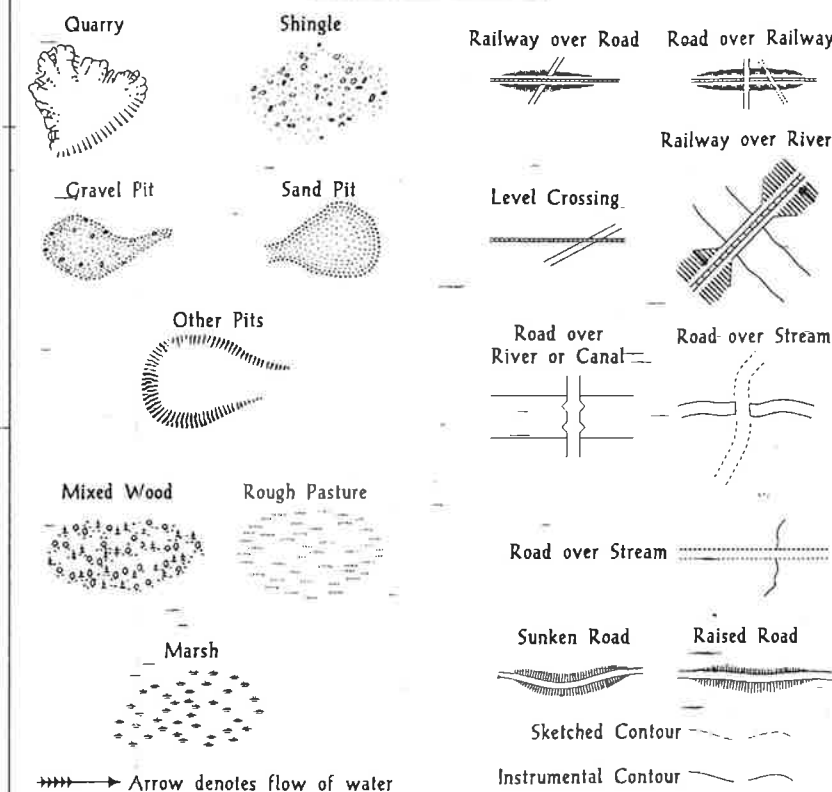
SITE DETAILS

Grid Reference 269800 193300

Freightliner Terminal Site

SWANSEA

Historical Map Legend



Ordnance Survey Plan

The historical maps shown were reproduced from maps predominantly held at the scale adopted for England, Wales and Scotland in the 1840's. In 1854 the 1:2,500 scale was adopted for mapping urban areas; these maps were used to update the 1:10,000 maps. The published date given on the right therefore is often some years later than the surveyed date. Before 1938, all OS maps were based on the Cassini Projection, with independent surveys of a single county or group of counties, giving rise to significant inaccuracies in outlying areas.

In the late 1940's, a Provisional Edition was produced, which updated the 1:10,000 mapping from a number of sources. The maps appear unfinished - with all military camps and other strategic sites removed. These maps were initially overprinted with the National Grid. In 1970, the first 1:10,000 maps were produced using the Transverse Mercator Projection. The revision process continued until recently, with new editions appearing every 10 years or so for urban areas.

1989

1980

Date(s) of Publication







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APPENDIX D
Borehole and Trial Pit Logs



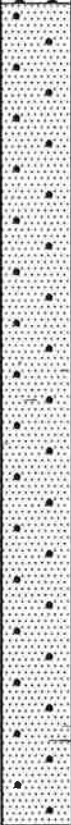
TRIAL PIT RECORD

PAGE 1 OF 1						TRIAL PIT NUMBER TP 1		
ELEVATION (metres)	DEPTH (metres)	DESCRIPTION	SYMBOL	PID	SAMPLE TYPE	SAMPLE RECOVERY	BACKFILL	DEPTH (metres)
		MADE GROUND: (Loose) light grey to black and ironstained very sandy fine to coarse angular gravel of porous slag and coal ash.						
					Chem 1			0.60
	1.10	Loose dark brown very silty organic SAND with rootlets (historic topsoil?)						1.00
	1.30	Loose to medium dense yellow-brown slightly silty fine to coarse SAND						
					Chem 2			1.90
								2.30
	2.60	END OF PIT						
REMARKS: Water seepage at 1.9m Pit collapsing below 1.3m				EXCAVATED BY		START DATE		
				EXUMA		24/09/98		
				LOGGED BY		COMPLETION DATE		
				NVP		24/09/98		
				CHECKED BY		JOB NUMBER		
						E210		
EXCAVATION METHOD				SITE				
JCB wheeled excavator				Ex Freightliner Site Neath				
				GIBB Environmental 				
ELEVATION METRES (AOD)								

CAPROGRA-1\PLOTLOG\ELTP1.P13 NVP-5 10-06-98

PAGE 1 OF 1

TRIAL PIT NUMBER TP 2

ELEVATION (metres)	DEPTH (metres)	DESCRIPTION	SYMBOL	PID	SAMPLE TYPE	SAMPLE RECOVERY	BACKFILL	DEPTH (metres)
		MADE GROUND: (Loose) black and dark brown very sandy fine to coarse angular gravel and cobbles of porous and vitreous slag and coal ash.						
	0.80	Loose to medium dense yellow-brown slightly silty fine to coarse SAND with some rootlets and dark brown very silty organic rich horizontal pockets spaced at approximately 0.5m intervals.			Chem 1			0.60 0.70
					Chem 2			1.20 1.60
	3.50	END OF PIT						

REMARKS:

Water seepage at 1.6m

Pit collapsing below 1.0m

EXCAVATED BY

EXUMA

START DATE

24/09/98

LOGGED BY

NVP

COMPLETION DATE

24/09/98

CHECKED BY

JOB NUMBER

E210

EXCAVATION METHOD

JCB wheeled excavator

SITE

Ex Freightliner Site Neath

GIBB




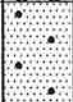
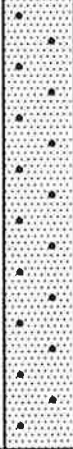


Environmental



PAGE 1 OF 1

TRIAL PIT NUMBER TP 3

C:\PROGRAM\1\PLOT\LOG\ELTP3.PI.3 NVP.5 10-06-98

ELEVATION (metres)	DEPTH (metres)	DESCRIPTION	SYMBOL	PID	SAMPLE TYPE	SAMPLE RECOVERY	BACKFILL	DEPTH (metres)
		MADE GROUND: (Loose) dark brown to black very sandy fine to coarse angular gravel of porous & vitreous slag and coal ash.						0.30
	0.50	MADE GROUND: Light brown silty clay with roots and ash.			Chem 1			0.50
	0.65	MADE GROUND: (Medium dense to dense) Black sandy fine to coarse angular gravel of ash and porous & vitreous slag with some cobble sized slag, coarse limestone gravel, occasional rootlets, bricks and metal fragments (probably iron).			Chem 2			0.65
	0.80	Loose to medium dense yellow-brown slightly silty fine to coarse SAND						1.60
								1.90
	2.60	Medium dense grey-green slightly silty fine to coarse SAND.						
	2.80	END OF PIT						

REMARKS:

Water seepage at 1.9m

Pit left open between 11:50 and 16:30, water rose to 1.60m.

Pit collapsing below 1.0m

EXCAVATED BY

EXUMA

LOGGED BY

NVP

CHECKED BY

EXCAVATION METHOD

JCB wheeled excavator

START DATE

24/09/98

COMPLETION DATE

24/09/98

JOB NUMBER

E210

SITE

Ex Freightliner Site Neath

GIBB

Environmental




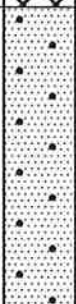
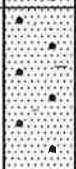


ELEVATION METRES (AOD)

TRIAL PIT RECORD

PAGE 1 OF 1

TRIAL PIT NUMBER TP 4

C:\PROGRAM-1\PILOT\LOG\ELTP4.PI.3 NVP-5 10-06-98

ELEVATION (metres)	DEPTH (metres)	DESCRIPTION	SYMBOL	PID	SAMPLE TYPE	SAMPLE RECOVERY	BACKFILL	DEPTH (metres)
		MADE GROUND: (Loose) black very sandy fine to coarse angular gravel of vitreous slag with some porous slag and coal ash.						0.40
					Chem 1			0.60
	0.90	Loose to medium dense yellow-brown slightly silty fine to coarse SAND						1.25
	1.90	Loose to medium dense grey-green fine to coarse silty SAND						
	2.50	Spongy black to brown slightly sandy clayey PEAT with many fine fibrous plant remains			Chem 2			2.50
	2.60	Medium dense yellow brown, discoloured grey green slightly silty fine to coarse SAND						2.30
	2.80	END OF PIT						

REMARKS:

Water seepage at 1.25m

Pit collapsing below 1.3m

EXCAVATED BY

EXUMA

START DATE

24/09/98

LOGGED BY

NVP

COMPLETION DATE

24/09/98

CHECKED BY

JOB NUMBER

E210

EXCAVATION METHOD

JCB wheeled excavator

SITE



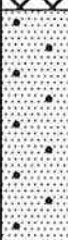
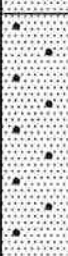
Ex Freightliner Site Neath

GIBB

Environmental



ELEVATION METRES (AOD)

ELEVATION (metres)	DEPTH (metres)	DESCRIPTION	SYMBOL	PID	SAMPLE TYPE	SAMPLE RECOVERY	BACKFILL	DEPTH (metres)
		MADE GROUND: (Loose) Dark brown to black very sandy fine to coarse angular gravel of porous slag and coal ash with much cobble and boulder sized slag.						0.40
					Chem 1			0.60
	0.90	Loose to medium dense yellow-brown slightly silty fine to coarse SAND						1.60
	1.70	Loose to medium dense yellow-brown, discoloured grey-green slight;y silty fine to coarse SAND			Chem 2			1.8
	2.50	END OF PIT						2.10

REMARKS:

Water seepage at 1.9m, rising to 1.6m

Pit collapsing below 1.0m

EXCAVATED BY

EXUMA

LOGGED BY

NVP

CHECKED BY

EXCAVATION METHOD

JCB wheeled excavator

START_DATE

24/09/98

COMPLETION DATE

24/09/98

JOB NUMBER

E210

SITE

Ex Freightliner Site Neath



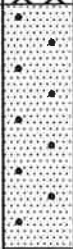
GIBB

Environmental



PAGE 1 OF 1

TRIAL PIT NUMBER TP 6

ELEVATION (metres)	DEPTH (metres)	DESCRIPTION	SYMBOL	PID	SAMPLE TYPE	SAMPLE RECOVERY	BACKFILL	DEPTH (metres)
	0.00	MADE GROUND: Light grey coarse angular limestone gravel (Rail Ballast)						
	0.40	MADE GROUND: (Loose) black very sandy fine to coarse angular porous & vitreous slag and coal ash with some cobble sized slag			Chem 1			0.50 0.70
	0.90	Loose to medium dense yellow-brown slightly silty fine to coarse SAND			Chem 2			1.20 1.40
	1.70	END OF PIT						

REMARKS:

Water seepage at 1.4m

Pit collapsing from the surface

EXCAVATED BY

EXUMA

START DATE

24/09/98

LOGGED BY

NVP

COMPLETION DATE

24/09/98

CHECKED BY

JOB NUMBER

E210

EXCAVATION METHOD

JCB wheeled excavator

SITE

Ex Freightliner Site Neath

GIBB





Environmental



PAGE 1 OF 1

TRIAL PIT NUMBER TP 7

C:\PROGRAMS\1\PLOT\LOGVELTP7.P13 NVP-6 10-06-98

ELEVATION (metres)	DEPTH (metres)	DESCRIPTION	SYMBOL	PID	SAMPLE TYPE	SAMPLE RECOVERY	BACKFILL	DEPTH (metres)
	0.25	MADE GROUND: Concrete, reinforced with a single layer of 6mm mesh.			Chem 1			
	0.45	MADE GROUND: Very sandy fine to coarse limestone gravel partially cemented (lean mix concrete)						0.45
		MADE GROUND: (Loose) light grey to black and ironstained very sandy fine to coarse angular gravel of porous slag and coal ash.						0.70
	1.15	Loose to medium dense yellow-brown slightly silty fine to coarse SAND			Chem 2			
								1.60
								2.20
	2.60	END OF PIT						

REMARKS:

Damp below 2.0m

Pit collapsing below 1.5m

EXCAVATED BY

EXUMA

LOGGED BY

NVP

CHECKED BY

EXCAVATION METHOD

JCB wheeled excavator

START DATE

24/09/98

COMPLETION DATE

24/09/98

JOB NUMBER

E210

SITE

Ex Freightliner Site Neath

GIBB

Environmental








ELEVATION METRES (AOD)

PAGE 1 OF 1

TRIAL PIT NUMBER TP 8

C:\PROGRAMS\1\PLOTLOG\ELTP8.PI 3 NVP-7 10-07-98

ELEVATION (metres)	DEPTH (metres)	DESCRIPTION	SYMBOL	PID	SAMPLE TYPE	SAMPLE RECOVERY	BACKFILL	DEPTH (metres)
	0.08	MADE GROUND: Black bitumen-bound tarmac			Chem 1			0.30 0.40
	0.20	MADE GROUND: Very sandy fine to coarse limestone gravel partially cemented (lean mix concrete)						
		MADE GROUND: (Loose) light grey to black and ironstained very sandy fine to coarse angular gravel of porous slag and coal ash.						
	1.10	Loose dark brown very silty organic SAND with rootlets (historic topsoil?)						
	1.30	Loose to medium dense yellow-brown slightly silty fine to coarse SAND			Chem 2			1.60 1.90 2.00
	2.50	END OF PIT						

REMARKS: Water seepage at 1.9m Pit collapsing below 1.0m	EXCAVATED BY	START DATE
	EXUMA	24/09/98
	LOGGED BY	COMPLETION DATE
	NVP	24/09/98
	CHECKED BY	JOB NUMBER
		E210
	EXCAVATION METHOD	SITE
	JCB wheeled excavator	Ex Freightliner Site Neath
		

ELEVATION METRES (AOD)

PAGE 1 OF 1

TRIAL PIT NUMBER TP 9

C:\PROGRA~1\PILOTLOG\TP9 PL3 NVP-7 10-07-98

ELEVATION (metres)	DEPTH (metres)	DESCRIPTION	SYMBOL	PID	SAMPLE TYPE	SAMPLE RECOVERY	BACKFILL	DEPTH (metres)
	0.20	MADE GROUND: Concrete, reinforced with a single layer of 6mm mesh. MADE GROUND: Very sandy fine to coarse limestone gravel partially cemented (lean mix concrete)						
	0.60	MADE GROUND: (Loose) light grey to black and ironstained very sandy fine to coarse angular gravel of porous slag and coal ash.			Chem 1			0.80 1.10
	1.40	Loose to medium dense yellow-brown slightly silty fine to coarse SAND						
	1.80	Loose to medium dense yellow brown, discoloured grey green slightly silty fine to coarse SAND.						
	2.60	Spongy black to brown slightly sandy clayey PEAT with many fine fibrous plant remains.			Chem 2			2.60 2.70
	2.70	Medium dense yellow brown discoloured grey green slightly silty fine to coarse SAND						
	2.90	END OF PIT						

REMARKS:

Damp below 2.0m

Pit collapsing below 1.3m

EXCAVATED BY

EXUMA

START DATE

24/09/98

LOGGED BY

NVP

COMPLETION DATE

24/09/98

CHECKED BY

JOB NUMBER

E210

EXCAVATION METHOD

JCB wheeled excavator

SITE

Ex Freightliner Site Neath









GIBB

Environmental



PAGE 1 OF 1

TRIAL PIT NUMBER TP 10

ELEVATION (metres)	DEPTH (metres)	DESCRIPTION	SYMBOL	PID	SAMPLE TYPE	SAMPLE RECOVERY	BACKFILL	DEPTH (metres)
	0.00	MADE GROUND: Light grey coarse angular limestone			Chem 1			
	0.10	gravel (Rail Ballast)						
		MADE GROUND: (Loose) black very sandy fine to coarse angular porous & vitreous slag and coal ash with some cobble and boulder sized slag and cobble sized brick						0.60
	1.10	Loose to medium dense yellow-brown slightly silty fine to coarse SAND			Chem 2			0.70
								1.60
	2.30	END OF PIT						2.00

REMARKS:

Water seepage at 2.0m

Pit collapsing from 1.2m

EXCAVATED BY

EXUMA

START DATE

24/09/98

LOGGED BY

NVP

COMPLETION DATE

24/09/98

CHECKED BY

JOB NUMBER

E210

EXCAVATION METHOD

JCB wheeled excavator

SITE

Ex Freightliner Site Neath

GIBB

Environmental



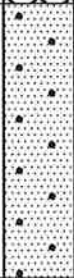





ELEVATION METRES (AOD)

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PAGE 1 OF 1

TRIAL PIT NUMBER TP 11

ELEVATION (metres)	DEPTH (metres)	DESCRIPTION	SYMBOL	PID	SAMPLE TYPE	SAMPLE RECOVERY	BACKFILL	DEPTH (metres)
		MADE GROUND: (Loose) black very sandy fine to coarse angular gravel of porous slag and coal ash with some cobble sized bricks and some medium to coarse elongated gravel sized lumps of previously molten metal (zinc?)						
	0.65	Loose to medium dense yellow-brown slightly silty fine to coarse SAND						
	1.55	Spongy dark grey to brown sandy, silty, clayey PEAT with some fine fibrous plant remains						
	1.80	END OF PIT						

REMARKS:

Pit damp below 1.55m

Pit collapsing below 1.3m

EXCAVATED BY

EXUMA

LOGGED BY

NVP

CHECKED BY

EXCAVATION METHOD

JCB wheeled excavator

START DATE

29/09/98

COMPLETION DATE

29/09/98

JOB NUMBER

E210

SITE

Ex Freightliner Site Neath

GIBB

Environmental



Date : 15/09/98		Meteorological and Site Conditions				
Operator: RF		State of ground Wind Wind Direction Cloud Cover Precipitation Temperature(deg.C) Barometric Pressure(mb)				
Equipment Used:		GI Infrared Gas Analyser		GMI Landsurveyor X	GMI Co2 Portable	
		Other: FID.				
Survey Information:						
BH	Water level (m)	O2 (%v/v)	CH4 (%v/v)	Co2 (%v/v)	VOC _L ppm	Others/Comments Depth to base of hole (m)
G2	0.80	20.90	0.00	0.00		1.50
	1.00	21.00	0.00	0.00		2.50
	1.25	20.70	0.00	0.00		3.50
	1.40	20.70	0.00	0.00		4.50
	1.90	20.70	0.00	0.00		5.50
	2.00	20.60	0.00	0.00		6.50
	2.20	20.70	0.00	0.00		7.50
	2.65	20.80	0.00	0.00		8.50
	2.70	20.80	0.00	0.00		9.50
E1	1.80	20.90	0.00	0.00		3.00
E3	DRY	20.80	0.00	0.00		1.00
	DRY	20.80	0.00	0.00		2.00
	2.00	20.80	0.00	0.00		3.00
	2.70	20.80	0.00	0.00		4.00
	2.50	20.80	0.00	0.00		5.00
	3.00	20.80	0.00	0.00		6.00
Remarks:						
The concentrations of gases recorded above are subject to the accuracy, as specified by the manufacturer, of the instrument adopted. If concentration accuracies of less than +/- 2% are required, it is recommended that gas samples are recovered and laboratory analyses are undertaken.						
Gas Monitoring Record		Project: Jersey Marine, Swansea			Contract: 158214	
Exploration Associates		Gibb, Environment Engineering			Figure:	

Sampling					Strata			
Depth	Type	Casing Depth	Date/ Water	SPT N (Cu)	Description	Depth (Thickness)	Level	Legend
0.25	B	NIL	28/09 1998		MADE GROUND: (Medium dense) black slightly silty sandy fine to coarse angular gravel of pulverised fly ash with vitreous and scoraceous slag with occasional cobbles.	G.L. (0.40)		
0.40	D	NIL				0.40		
1.50-1.95	CD B	1.50	1.50	36	Dense yellow brown slightly silty fine to coarse SAND with occasional coarse sand to fine gravel of lignite mudstone and white to black shell fragments. ... at 0.40m with some boulders (<350mm) of welded slag	(2.40)		
2.50-2.95	CD B	2.50	1.90	28		2.80-3.00		
3.50-3.95	CD B	3.50	2.00	30	Spongey grey mottled black slightly silty sandy PEAT with fine fibrous plant remains.			
4.50-4.95	CD B	4.50	2.00	26	Dense yellow brown discoloured grey green slightly silty fine to coarse SAND with occasional coarse sand to fine gravel of lignite mudstone and white to black shell fragments.	(2.90)		
5.25-5.75	B				... from 5.25m with occasional fibrous decayed plant remains			
5.90	D					5.90		
6.00-6.45	CD B	6.00	2.20	2	Spongey very soft black to brown locally sandy PEAT with many fibrous plant remains.			
6.75-7.25	B				... from 6.75m to 7.40m becomes plastic very soft locally slightly sandy very silty PEAT	(1.50)		
7.40	D					7.40		
7.50-7.95	CD B	6.50	3.40	3	Very soft blue grey slightly sandy very silty CLAY locally with occasional fibrous peaty remains.	(0.60)		
8.00	B W	8.00	3.40		End of Borehole.	8.00		
Equipment: Light cable percussion					Groundwater			
Borehole Dia (mm) 200 to 8.00m					No. Struck Behaviour		Sealed	
Casing Dia (mm) 200 to 8.00m					1 3.50		No obvious strike. Ceased drilling at 3.50m depth standing water rose from 3.20m to 2.00m in 20mins.	
Remarks					Drilled by		FF	
Water added to assist boring from 1.20m to 3.50m					Logged by		RB	
Inspection pit excavated to 1.20m (1.50Hrs).					Checked by			
Installation of a 50mm nominal diameter UPVC standpipe, slotted at 0.5mm in a 2mm sand bed from 6.50 to 1.50m with a sump to 8.00m								
See key sheet and appendices for explanations.					Form 1/0			
Borehole Record					Project		Contract	
					Jersey Marine, Swansea G.I.		158214	
					GIBB. Environmental Engineering		Borehole	
							E1(1 of 1)	
Exploration Associates								

Sampling					Strata		Depth (Thickness)	Level	Legend
Depth	Type	Casing Depth	Date/Water	SPT N (Cu)	Description				
0.25	B	NIL	29/09 1998		MADE GROUND: (Medium dense) black very sandy fine to coarse angular gravel of slaggy bituminous waste ash and coal with occasional cobbles.	G.L.			
0.50	B	NIL				(0.50)			
1.00		1.00	DRY 30/09		Dense Yellow brown slightly silty fine to coarse SAND (with a strong chemical bituminous odour from 1.00m to 6.00m).	0.50			
1.50-1.95	CB	1.50	1.20	33	... from 1.50m to 2.00m with occasional cobble to boulder sized red welded pumiced/scoraceous slag (foreshore wash?) ... from 1.50m becomes grey green.				
2.50-2.95	SB	2.50	2.00	22					
3.50-3.95	SB	3.50	2.50	3					
4.50-4.95	CB	4.50	2.00	5	... from 4.30m with some to occasional fine to coarse rounded gravel of predominantly sandstone and occasional cobbles with a single subrounded cobble of red welded pumiced /scoraceous slag.	(7.40)			
5.25-5.75									
6.00-6.45	SB	6.00	2.20	17NR	... from 6.00m with shell fragments				
6.75-7.25									
7.50-7.95	CB	7.50	2.25	8	... from 7.50m to 7.80m with shells				
7.90	B	8.00	2.25			7.90			
8.00						8.00			
2.00					Soft blue grey slightly sandy very silty CLAY with occasional fine to coarse rounded gravel of mudstone and sandstone. End of Borehole.				
Equipment: Light cable percussion					Groundwater		Sealed		
Borehole Dia (mm) 200 to 8.00m					No. Struck Behaviour		1 2.00 Rose to 1.00m in 20 mins 1.60/1.30/1.10 in 5/10/15 mins		
Casing Dia (mm) 200 to 8.00m							Drilled by FF Logged by RB Checked by		
Remarks		Water added to assist boring from 1.00m to 2.00m Jet washed rig before accessing borehole. Inspection pit excavated to 1.20m (30mins). Contamination samples obtained from 2.50m to 3.50m (3No). Installation of a 50mm nominal diameter UPVC standpipe, plotted at 0.5mm and installed in a 2mm sand bed from 6.00m to 2.00m with a sump to 8.00m.							
See key sheet and appendices for explanations.		Form 1/0							
Borehole Record					Project		Contract 158214		
					Jersey Marine, Swansea G.I. GIBB, Environmental Engineering		Borehole E2(1 of 1)		
Exploration Associates									

Sampling					Strata		Depth (Thickness)	Level	Legend
Depth	Type	Casing Depth	Date/ Water	SPT N (Cu)	Description				
0.50-1.00	B	NIL	28/09 1998 DRY		MADE GROUND: (Very Dense) grey slightly sandy fine medium to coarse angular gravel of predominantly scoraceous slag	G.L.			
1.20-1.50	CD B	1.20	DRY	50/75	MADE GROUND: Very dense black sandy fine to coarse angular gravel of pulverised fly ash with scoraceous and vitreous slag brick with occasional cobbles and boulders**	(0.80)			
2.00-2.50	CD B	2.00	DRY	46	Dense yellow brown discoloured grey slightly silty fine to coarse SAND with occasional fine to medium sub-rounded gravel of sandstone and mudstone with occasional fine gravel sized shell fragments	1.60			
3.00-3.50	CD B	3.00	2.00	46		(3.20)			
4.00-4.50	CD B	4.00	2.70	34	...at 4.00m with occasional fine fibrous peaty inclusions				
4.80-5.00	D					4.80			
5.00-5.50	CD B	5.00	2.50	19	Spongey black to brown locally slightly sandy PEAT with many fibrous plant remains	(0.70)			
4.70-5.50					...from 5.00m to 5.50m becomes firm plastic slightly sandy very silty PEAT with some fibrous organic remains	5.50			
6.00-6.50	B				Soft grey very silty CLAY with fibrous vegetative matter**	(0.80)			
6.50-7.00	CD	6.50	3.00	25	Dense brown slightly silty fine to coarse SAND with occasional fibrous plat remains and soft peaty inclusions.	6.50			
6.50		6.50	29/09	 End of Borehole.				
Equipment: Light cable percussion					Groundwater				
Borehole Dia (mm) 200 to 6.50m					No. Struck Behaviour Sealed		Drilled by PO Logged by RB Checked by		
Casing Dia (mm) 200 to 6.50m					1 3.00 No obvious strikes, water maintained between 2.00 and 3.00m during drilling.				
Remarks					Form 1/0				
Chiselled from 1.30m to 1.60m (45 mins) Water added to assist boring from 1.60m to 5.50m Inspection pit excavated to 1.20m (2hrs) Gas tests taken from 1.00m to 6.00m at 1.00m intervals. Installation of a 50mm nominal diameter UPVC stand pipe, slotted at 0.5mm in a 2.0mm sand bed from 5.50m to 2.50m with a sump to 6.50m.									
See key sheet and appendices for explanations.									
Borehole Record					Project		Contract		
					Jersey Marine, Swansea G.I. GIBB. Environmental Engineering		158214		
Exploration Associates							Borehole E3(1 of 1)		


Sampling					Strata			
Depth	Type	Casing Depth	Date/ Water	SPT N (Cu)	Description	Depth (Thickness)	Level	Legend
0.30-0.60	B	NIL	29/09 1998		MADE GROUND: Very dense grey reinforced concrete.	G.L.		
0.60-1.20	B	NIL			MADE GROUND: Very dense black to grey slightly sandy fine to coarse angular gravel of predominantly scoraceous slag with many cobbles.	0.30 0.60		
1.20-1.65 1.20-1.60	C B	1.20	DRY	50/ 85	MADE GROUND: Very dense black sandy fine to coarse angular gravel of pulverised fly ash with ash slag (vitreous and scoraceous) siltstone brick and shells with occasional cobbles and boulders (<300mm)	(1.20) 1.80		
2.00-2.45	SD	2.00	DRY	49	Dense locally very dense yellow brown slightly silty fine to coarse SAND with occasional fine gravel of mudstone and rare slag (reworked natural / wind blown)			
2.50-3.00	B							
3.00-3.45	SD	3.00	2.20	56				
3.50-4.00	B					(3.70)		
4.00-4.45	SD	4.00	2.00	39	from 4.00m slag absent with occasional fibrous plant remains			
4.50-5.00	B				from 4.50m to 5.00m with peaty inclusions			
5.00-5.45	SD	5.00	2.00 3.50	49				
5.00			30/09 3.00					
5.50-5.70	B					5.50		
5.70-6.00	B				Plastic firm dark brown to black slightly sandy very silty PEAT with many fine fibrous plant remains.	5.70		
6.00-6.45	C	6.00	3.00	50/ 20		(0.90)		
6.00-6.50	B				Very dense dark grey very sandy fine to coarse rounded GRAVEL of predominantly sandstone	6.60		
6.60-7.00	B					(0.40)		
7.00-7.45	C	7.00	3.00	50/ 40	Spongy (firm) dark brown to black slightly sandy silty PEAT with many fibrous plant remains.	7.00		
7.00-7.50	B					(0.80)		
7.80-8.00	B				Very dense black slightly sandy sub-rounded to rounded COBBLES of sandstone and quartz with some fine to coarse sub-rounded to rounded gravel.	7.80		
8.00-8.45	SD	8.00	4.70	8		8.00		
8.00-8.50	B				Soft blue grey slightly sandy very silty CLAY with occasional fibrous plant remains and peaty inclusions with occasional fine to coarse rounded gravel.			
9.00-9.45	SD	9.00	5.10	7	Soft locally grading to very soft slightly sandy very silty CLAY			
9.00-9.50	B				from 9.00m to 9.50m with some fine to coarse gravel of predominantly sandstone with fine to medium gravel sized inclusions of fibrous brown peat			
					at 10.00m becomes very loose slightly			
Equipment: Light cable percussion					Groundwater: No Struck Behaviour Sealed			
Borehole Dia (mm) 200 to 18.00m 150 to 20.2m		Casing Dia (mm) 200 to 18.00m 150 to 20.20m		1" 5.70 rose to 3.70m in 20 mins 5.00/4.50/4.00 in 5/10/15 mins		Drilled by PO Logged by RB Checked by		
Remarks: Chiselled from 1.30m to 1.60m (45 mins), 6.10m to 6.30m (30 mins), 7.20m to 7.50m (45 mins) Water added to assist boring from 1.20m to 5.70m Excavate inspection pit to 1.20m (75mins). Gas testing at 1.00m centres from 1.00m to 5.00m.								
See key sheet and appendices for explanations.					Form 1/0			
Borehole Record					Project: Jersey Marine, Swansea G.I. GIBB, Environmental Engineering		Contract: 158214	
Exploration Associates							Borehole: G1(1 of 3)	

Sampling					Strata		Depth (Thickness)	Level	Legend
Depth	Type	Casing Depth	Date/Water	SPT N (Cu)	Description				
10.00-10.45 10.00-10.50	S B	10.00	30/09 4.50	4	sandy very clayey SILT				
11.50-11.45	S	11.50	5.00	3	at 11.50m becomes sandy				
12.50-13.00	S				at 12.50m becomes very soft blue grey sandy very silty CLAY with lenses of fine to coarse sand				
13.00-13.45	S	13.00	3.90	2	at 13.00m becomes slightly sandy very silty CLAY with very closely spaced partings with a coating <1mm of fine to medium sand	(10.50)			
14.00-14.50	B				at 14.00m becomes sandy				
14.50-14.55	S	14.50	4.20	0	at 14.50m grades to very loose sandy very clayey SILT				
15.50-16.00	B				at 15.50m grades to sandy very silty CLAY / very clayey SILT with occasional shell fragments				
16.00-16.45	S	16.00	4.20	4					
17.00-17.50	B								
17.50-17.95	S	17.50	4.50	4	at 17.50m slightly sandy				
18.00		18.00	4.00 01/10						
		18.00				18.50			
					Very dense grey slightly clayey slightly sandy sub-rounded to rounded COBBLES of predominantly sandstone with some fine to coarse sub-rounded to rounded gravel. from 19.00m becomes slightly sandy fine to coarse GRAVEL of sandstone (grey and red) quartz mudstone and siltstone with some cobbles	(1.70)			
Equipment: light cable percussion					Groundwater No. Struck Behaviour		Sealed		
Borehole Dia (mm) 200 to 18.00m 150 to 20.2m		Casing Dia (mm) 200 to 18.00m 150 to 20.20m				Drilled by PO Logged by RB Checked by			
Remarks See key sheet and appendices for explanations.									
Borehole Record					Project Jersey Marine, Swansea G.I. GIBB Environmental Engineering		Contract 158214		
Exploration Associates							Borehole G1(2 of 3)		

Sampling					Strata		Depth (Thickness)	Level	Legend	
Depth	Type	Casing Depth	Date/ Water	SPT N (Cu)	Description					
			01/10		End of Borehole.		20.20			
Equipment: light cable percussion					Groundwater No. Struck Behaviour		Sealed			
Borehole Dia (mm) 200 to 18.00m 150 to 20.2m		Casing Dia (mm) 200 to 18.00m 150 to 20.20m						Drilled by PO Logged by RB Checked by		
Remarks: See key sheet and appendices for explanations.										
Borehole Record					Project Jersey Marine, Swansea G.I. GIBB. Environmental Engineering		Contract 158214			
Exploration Associates							Borehole G1(3 of 3)			

Form 1/0

Sampling					Strata			
Depth	Type	Casing Depth	Date/ Water	SPT N (Cu)	Description	Depth (Thickness)	Level	Legend
			06/10 1998 DRY		MADE GROUND: Black gravelly ash fill **	G.L. (0.40)	7.24	
0.40						0.40	6.84	
0.75-1.25					MADE GROUND: Black mottled yellow fine to coarse sand with occasional fine to medium subrounded gravel or slag	(1.60)		
1.50-1.95		1.50	0.80	14				
1.50-1.95								
					Medium dense brown fine to coarse SAND	2.00	5.24	
2.50-2.95		2.50	1.00	12				
2.50-2.95								
2.50-2.95								
3.50-3.95		3.50	1.25	11				
3.50-3.95								
3.50-3.95								
4.10					... from 4.10 occasional subrounded coarse gravel and cobbles of sandstone			
4.50-4.95		4.50	1.40	50/ 110				
4.50-4.95								
4.10								
5.00		5.00	2.20			(5.60)		
		5.00	1.40		5.10 to 6.30 some gravel and cobbles			
5.50-5.95		5.50	1.90	50/ 125				
5.50-5.95								
6.50-6.95		6.50	2.00	27				
6.50-6.95								
7.50-7.95		7.50	2.20	4		7.60	-0.36	
7.50-7.95								
					Soft grey slightly sandy very silty CLAY with occasional lenses of peat			
8.50-8.95		8.50	2.65	7				
8.50-8.95								
					...from 9.20 very sandy	(2.65)		
9.50-9.95		9.50	2.70	2				
9.50-9.95								
Equipment: Dando 150					Groundwater		Ground Level	
					No. Struck Behaviour		Coordinates	
					Sealed		7.24 m OD	
					1 4.10 - Rose to 1.70m in 20 mins		269610.12 mE	
					3.20/2.50/2.00 in 5/10/15 mins		193233.82 mN	
Borehole Dia (mm)							Drilled by FF	
200 to 17.50m							Logged by OT	
Casing Dia (mm)							Checked by	
200 to 17.50m								
Remarks					Form 1/0			
Chiselled from 4.20m to 4.50m (60 mins), 4.60m to 5.00m (90 mins), 5.00m to 5.50m (90 mins), 5.80m to 6.20m (75 mins)								
Jet wash rig and equipment 45 mins								
Move to borehole location 90 mins								
Dig inspection pit 60 mins								
9 No. Gas tests taken see separate sheet								
Interupted by Engineer to terminate borehole due to location of near by badger set wiring 60 mins								
Borehole Record					Project		Contract	
					Jersey Marine, Swansea G.I.		158214	
					G168. Environmental Engineering		Borehole	
							G2(1 of 2)	
Exploration Associates								

Sampling					Strata					
Depth	Type	Casing Depth	Date/Water	SPT N (Cu)	Description	Depth (Thickness)	Level	Legend		
10.25-10.75	B	10.50	07/10 3.30		Loose grey very silty SAND	10.25	-3.01			
10.50		10.50	08/10 2.60							
11.00-11.45	B	11.00	3.00	3						
11.00-11.45										
12.50-12.95	B	12.50	3.20	2						
13.25-13.75	B									
14.00-14.45	B	14.00	3.40	9		(7.25)				
14.00-14.45										
14.75-15.25	B									
15.50-15.95	B	15.50	3.60	6						
15.50-15.95										
15.50-15.95										
16.25-16.75	B									
17.00-17.45	B	17.00	3.80	7						
17.00-17.45										
17.50		17.50	3.80		End of Borehole.	17.50	-10.26			
Equipment: Dando 150					Groundwater No. Struck Behaviour		Sealed	Ground Level Coordinates	7.24 m OD 269610.12 193233.82	ME mm
Borehole Dia (mm) 200 to 17.50m		Casing Dia (mm) 200 to 17.50m				Drilled by Logged by Checked by		FF OT		
Remarks										
See key sheet and appendices for explanations.										
Borehole Record					Project		Contract			
					Jersey Marine, Swansea G.I. GIBB. Environmental Engineering		158214			
Exploration Associates							Borehole			
							G2(2 of 2)			

Form 1/0

Sampling					Strata			
Depth	Type	Casing Depth	Date/Water	SPT N (Cu)	Description	Depth (Thickness)	Level	Legend
			02/10 1998		MADE GROUND: Reinforced concrete **	G.L.	8.08	
0.60-1.20	C				MADE GROUND: Very compacted hardcore **	0.30	7.78	
1.20-1.70	C	1.20	DRY	50/95	MADE GROUND: Very dense black to grey slightly sandy fine to coarse angular gravel of ash, slag and brick fragments and wooden objects and occasional cobbles (and boulders **)	0.60	7.48	
2.00-2.50	S	2.00	1.80	47	Dense to locally very dense yellow brown slightly silty fine to coarse SAND	(1.30)		
3.00-3.50	S	3.00	2.00	52		1.90	6.18	
4.00-4.50	S	4.00	3.00	49		(3.60)		
5.00-5.50	D	5.00	4.20		... from 5.00 to 5.50 with peaty inclusions	5.50	2.58	
6.00-6.50	S	6.00	4.00	34	Plastic firm dark brown slightly sandy very clayey PEAT with some fine fibrous plant remains.	(0.40)		
7.00-7.50	S	7.00	3.20	35	Dense grey brown slightly silty fine to coarse SAND with occasional fibrous plant remains and peaty inclusions	5.90	2.18	
8.00-8.50	S	8.00	2.50	40	... from 8.00 becoming grey	(2.70)		
8.60-9.00	D	8.00	2.00			8.60	-0.52	
9.00-9.50	U(15)	9.00	2.70		Soft grey slightly clayey slightly sandy SILT with occasional shell fragments	(1.90)		
9.50-10.00	D							
Equipment: Light Cable Percussion					Groundwater		Ground Level 8.08 m OD	
Borehole Dia (mm) 200 to 21.70m					No. Struck Behaviour		Coordinates 269734.53 193357.98	
Casing Dia (mm) 200 to 21.70m					1 20-50 Rose to 17.90m in 20 mins 19.20/18.70/18.30 in 5/10/15 mins		Sealed	
Remarks					Drilled by WO		Logged by RB	
See key sheet and appendices for explanations					Checked by			
Borehole Record					Project		Contract 158214	
Exploration Associates					Jersey Marine, Swansea G.I. GIBB. Environmental Engineering		Borehole G3(1 of 3)	

Sampling					Strata				
Depth	Type	Casing Depth	Date/Water	SPT N (Cu)	Description	Depth (Thickness)	Level	Legend	
10.00	U(7)	10.00	05/10 3.20						
10.45-10.50						10.50	-2.42		
11.00-11.50					Loose grey very silty fine to coarse SAND				
11.50	S	11.50	3.00	4					
12.90-13.00	U(35)	13.00	3.00						
13.45-13.50									
14.50-15.00	B								
15.00	S	15.00	8.00			(9.70)			
16.50	P	16.50							
17.50-18.00	B								
18.00	S	18.00	12.00	8					
19.00-19.50	B								
19.50	S	19.50	13.50	2					
20.00		20.00	18.90 06/10						
Equipment: Light Cable Percussion					Groundwater No. Struck Behaviour		Sealed	Ground Level Coordinates 8.08 m OD 269784.53 193357.98	
Borehole Dia (mm) 200 to 21.70m		Casing Dia (mm) 200 to 21.70m					Drilled by WO Logged by RB Checked by		
Remarks See key sheet and appendices for explanations									
Borehole Record					Project Jersey Marine, Swansea G.I. GIBB. Environmental Engineering		Contract 158214		
Exploration Associates							Borehole G3(2 of 3)		

Form 1/0

Sampling					Strata				
Depth	Type	Casing Depth	Date/Water	SPT N (Cu)	Description	Depth (Thickness)	Level	Legend	
		20.00	06/10			20.20	-12.12		
20.50-21.00					Dense brown slightly sand fine to coarse subangular to subrounded GRAVEL and occasional cobbles of sandstone				
21.00-21.70		21.00	17.50	50/10		(1.80)			
21.70		21.70	18.00	50/20		22.00	-13.92		
21.70			18.00		End of Borehole.				
Equipment: Light Cable Percussion					Groundwater No. Struck Behaviour		Sealed	Ground Level Coordinates	8.08 m OD 269784.53 193357.98 mE mN
Borehole Dia (mm) 200 to 21.70m		Casing Dia (mm) 200 to 21.70m				Drilled by Logged by Checked by		WO RB	
Remarks									
See key sheet and appendices for explanation									
Borehole Record					Project		Contract		158214
					Jersey Marine, Swansea G.I. GIBB. Environmental Engineering		Borehole		G3(3 of 3)
Exploration Associates									

APPENDIX E

Previous Ground Investigations



TESTING
No. 0980



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Newby House,
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SA10 7DR

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All correspondence to be addressed to the Laboratory Manager

**Freightliner Access Road
Jersey Marine
Ground Investigation Report**

Laboratory Reference No.: 01437/R784/RLS

Client:
Head of Engineering
Design and Construction Consultancy
Technical Services Department
Neath Port Talbot County Borough Council
Civic Centre
Penllergaer
Swansea

01437/R784

LABORDY PRIDDOEDD A DEUNYDDIAU CYNGOR BWRDEISTREF SIROL CASTELL-NEDD PORT TALBOT
THE SOILS AND MATERIALS LABORATORY OF NEATH PORT TALBOT COUNTY BOROUGH COUNCIL

CONTENTS

1.	INTRODUCTION	1
2.	SITE DESCRIPTION AND GEOLOGY	2
3.	GEOLOGY	3
4.	GROUND INVESTIGATION	4
4.1	Fieldwork	
4.2	Laboratory Testing	
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5.1	Made Ground	
5.2	Blown Sand	
5.3	Ground Water	
6.	ENGINEERING DISCUSSION AND RECOMMENDATIONS	6

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FIGURES

APPENDICES

Appendix A:	Trial Pit Logs
Appendix B:	Laboratory Test Results.

DRAWING

W2057/TP1:	Trial Pit Locations
------------	---------------------

1. INTRODUCTION

Earlswood Materials Laboratory was instructed by the Head of Engineering of Neath Port Talbot County Borough Council to undertake a ground investigation for a proposed new access to the Freightliner depot at Jersey Marine. This report describes the investigations carried out, presents the results obtained, and makes recommendations for design and construction of the proposed works.

2. SITE DESCRIPTION

The site is located to the north of A483 Fabian Way at Jersey Marine, between the Gower Chemicals works and the Ford plant. The location and topography of the site is shown on Drawing W2507/TP1 enclosed with this report.

The proposed access road route commences at a junction with Elba Crescent at the south of the Gower Chemicals site. It then follows an existing road running parallel to the railway track serving the Ford plant for approximately 70m. It then crosses the railway track and then runs parallel to the north side of the track to finish in an area of dense scrub land. The area around the site is generally level and is mainly occupied by various industrial premises including Gower Chemicals, Ford, Shell UK and ERF Trucks.

Historic Ordnance Survey maps at 25" to 1 mile Scale dated 1880 and 1917 have been consulted to determine former land use on the site. The 1880 map indicates that the site was an area of rough grazing land. The 1917 map indicates railway locomotive sheds, workshops and associated yards in the area to the north of the present railway line, and fields to the south. The present Gower Chemicals works occupies the former railway sheds and workshops.

3. GEOLOGY

The 1:10560 Scale geological map (SS69SE) indicates that the site is underlain by Blown Sand overlying the Middle Coal Measures. It is possible that Alluvium may be present between the Blown Sand and the ~~Alluvium~~ Middle Coal Measures.

4. GROUND INVESTIGATION

4.1 Fieldwork

Ground investigation fieldwork was undertaken on 24th and 25th September 1996, and comprised four trial pits (TP1, 2, 4, and 5) and one road core (at location TP3). The trial pit and road core locations are shown on drawing W2507/TP1 enclosed with this report.

The trial pits are logged by an engineering geologist in accordance with BS5930:1981, and the logs are presented in the Appendix A.

4.2 Laboratory Testing

California bearing ratio (CBR) tests were carried out on selected soil samples in accordance with BS1377:Part 4:1990 Clause 7.4.

The road core was logged, and the compressive strength of the concrete was determined in accordance with BS1881:Part 120:1993.

Selected soil samples were screened for contamination. This testing was undertaken by Anchem Analytical Laboratories. Additional analysis of mineral oils was undertaken by Hyder Environmental.

The results of laboratory testing are presented in Appendix B.

5. GROUND CONDITIONS

The ground conditions revealed by the investigation comprised Made Ground overlying Blown Sand.

5.1 Made Ground

The Made Ground is between 0.6m and 2.4m thick and consists mainly of medium dense, dark grey or black, usually gravelly, sand containing slag, clinker, coke, brick, concrete, ash and glass fragments.

The results of California Bearing Ratio tests indicate that the CBR value of the Made Ground may be assumed to be greater than 15%.

The results of chemical tests indicate that the Made Ground in the vicinity of the existing level crossing is heavily contaminated with oil, with concentrations up to 2.3% being measured. Loss of ignition results of around 40% were measured, indicating a high content of combustible material, which may include organic matter and coal.

Further analysis identified that the oils consist mainly of hydrocarbons typical of diesel fuel oil and lubricating oil. Samples also contained various polycyclic aromatic hydrocarbons typical of coal tar, with total polycyclic aromatic hydrocarbon contents of 48 and 18mg/kg being measured, indicating slight contamination by coal tar.

5.2 Blown Sand

Deposits of Blown Sand were encountered beneath the Made Ground, consisting mainly of loose to medium dense orange brown fine to medium sand.

The CBR value of this stratum is expected to be in excess of 15%.

5.3 Ground Water

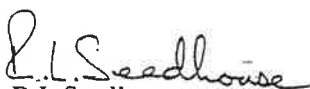
Ground water was encountered at depths between 1.6 and 2.1m.

6. ENGINEERING DISCUSSION AND RECOMMENDATIONS

The formation for the proposed road is likely to be mainly within the Made Ground, but the underlying sand may be encountered in some cases. Provided that compaction is applied to the formation, a CBR of 15% is achievable in both cases. Therefore, a capping layer will not be required.

The Made Ground should be treated as contaminated, the principal contaminants being diesel fuel and lubricating oil. It is recommended that any exposed surfaces are covered as soon as practicable with pavement materials or 500mm thickness of clean, inert soil cover. The area of Made Ground exposed at any time should be kept to the minimum practicable. A substantial proportion of the materials making up the Made Ground are potentially combustible and therefore care must be taken to avoid fires on, or close to, the Made Ground.

It is recommended that site operatives wear overalls, boots, and gloves at all times to minimise skin contact with the soil. It is also recommended that eating, drinking and smoking is prohibited within working areas. Washing facilities should be provided on site, and should be used before meal breaks and before personnel leave the site, to minimise the risk of ingestion of contaminants.


R.L. Seedhouse

Geotechnical Engineer



P.T.E. Tucker

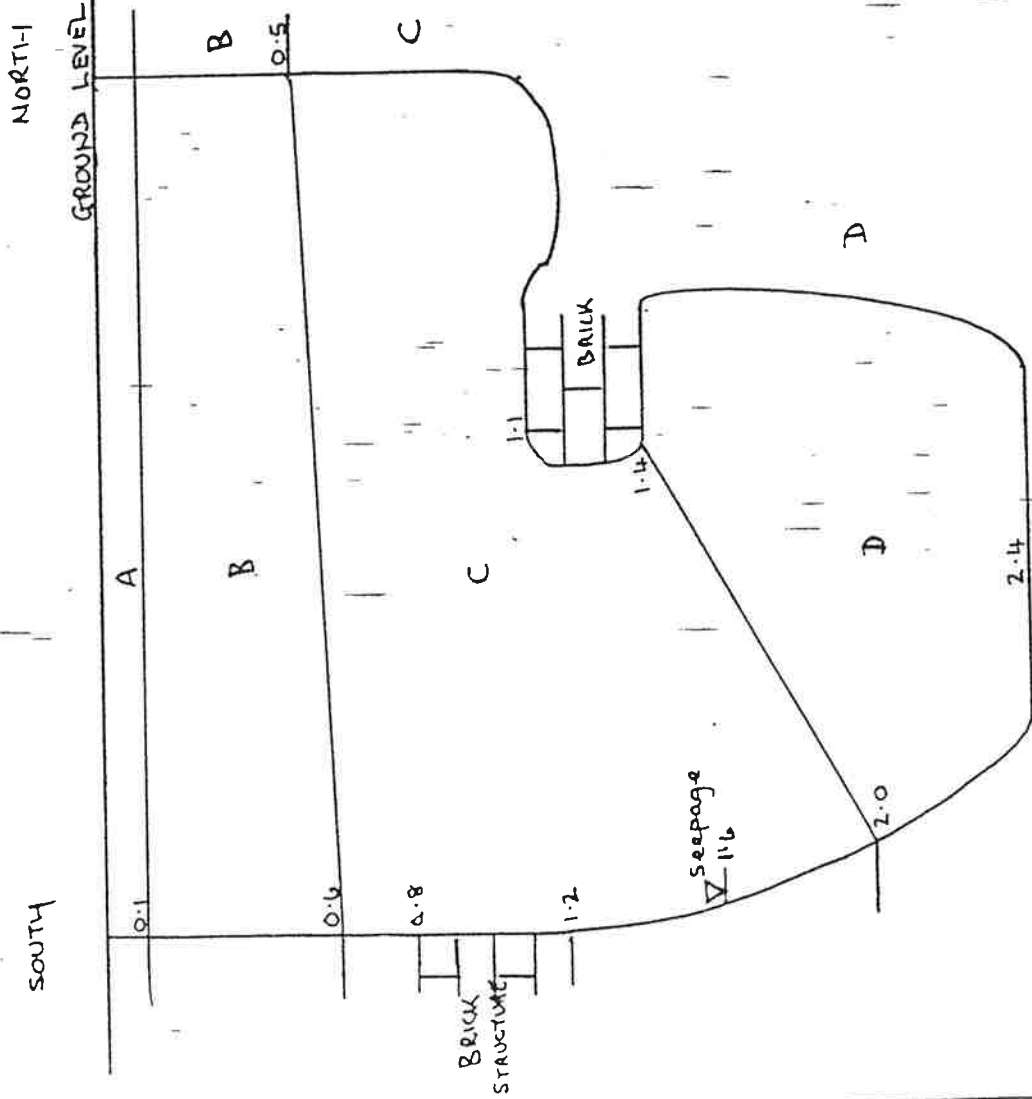
Laboratory Manager

Date: 6th November 1996

REFERENCES

1. GEOLOGICAL SURVEY OF GREAT BRITAIN (England and Wales) 1:10,560 scale sheet SN679SE
2. BS5930:1981. Code of practice for site investigations.
3. BS1377:1990 British Standard methods of test for soils for civil engineering purposes.
4. BS1881:Part120:1993. Testing concrete: Method for determination of the compressive strength of concrete cores.

Appendix
Trial Pit Logs
TP1, TP2, TP4, TP5



A Bitumen bound Surfacing materials

B Dense slag aggregate of gravel size with some sand fines

C Grey black gravelly (clinker, coke, sandstone) sand (mainly natural with sand size fragments of coke) - medium dense? Pieces of brick and concrete.

D Grey black fine medium sand (mainly natural with sand size fragments of coke and ash) with some limestone aggregate and lumps of lean mix concrete - medium dense?

E Orange brown fine to medium SAND - loose to medium dense? (BLOWN SAND)

FREIGHTLINER ACCESS

TRIAL PIT 1

FIGURE

SCALE 1:200

PIT DIMENSIONS: 2.2m X 0.70m X 2.4m
ALL DEPTHS ARE IN METRES BELOW GROUND LEVEL

Earlswood Materials Laboratory

Job No.:

01437

TP2

Sheet 1 of 1

Equipment:
Hand excavated pit.

Job: **Freightliner Access Road**

Client: **Neath Port Talbot C.B.C.**

Ground Level

Coordinates

Dates

27/06/1996

27/06/1996

Strata Descriptions

Red.
Level

Legend

Depth

Sample Depth

Sample
No.

SPT
/CPT

Core
Recovery

Remarks

Water Records

TCR SCR RQD

Levels Piezo.

Bitumen bound surfacing materials
(MADE GROUND)

Black sand and fine medium (with
coarse) gravel of mainly ash and
coke (MADE GROUND)

Black sandy to very sandy (mainly
natural with coke and clinker)
angular mainly sandstone gravel
aggregate (MADE GROUND)

Orange fine to medium SAND -
medium dense? (BLOWN SAND)

End of Borehole

Remarks

Pit dimensions: 0.45m X 0.70m X1.0m. Pit dry.

Key

U Undisturbed sample
P Piston sample
B Bulk disturbed sample
D Small disturbed sample
W Water sample

S SPT (split spoon)
C SPT (solid cone)
▽ Water strike
▼ Water level

Logged By:

JCO

Scale
1:50

Earlswood Materials Laboratory

Job No.:

01437

TP5

Sheet 1 of 1

Equipment:
Pit excavated by JCB.

Job: Freightliner Access Road

Client: Neath Port Talbot C.B.C.

Ground Level

Coordinates

Dates

24/09/1996

24/09/1996

Strata Descriptions

Red.
Level

Legend

Depth

Sample Depth

Sample
No.

SPT
/CPT

Core
Recovery

Remarks

Water Records

Levels Piezo.

Grey black fine to medium slightly
gravelly fine medium sand (natural with
much coke fines) with many roots and
rootlets - loose to medium dense? (MADE
GROUND)

Orange brown fine to medium SAND
- medium dense? (BLOWN SAND)

End of Borehole

(0.50)

0.50

0.40

1 B

(1.50)

2.00

Remarks

Pit dimensions: 1.0m X 2.5m X 2.0m.
Groundwater seepage at 2.0m depth.
Sides became very unstable once
groundwater encountered.

Key

U Undisturbed sample
P Piston sample
B Bulk disturbed sample
D Small disturbed sample
W Water sample

S SPT (split spoon)
C SPT (solid cone)
▽ Water strike
▼ Water level

Logged By:

JCO

Scale
1:50

Appendix B.
Laboratory Test Results.

SUMMARY OF CALIFORNIA BEARING RATIO TESTS

Scheme: Freightliner Access, Jersey Marine

Sheet 1
of 1

Key: VH Vibrating hammer compaction (3 layers)
BS2.5 British Standard 2.5kg drop hammer
BS4.5 British Standard 4.5kg drop hammer

T = Top B = Bottom A = Average

Hole No.	Sample No.	Depth (m)	Compaction Method	Surcharge (Equivalent Construction) (mm)	Bulk Density (Mg/m ³)	Dry Density (Mg/m ³)	Moisture Content %	CBR Value %
TP1	B2	1.0	BS2.5	150	1.75	1.47	T 18 B 18 A 18	T B 62 A
TP2	B1	0.3-0.6	BS2.5	150	1.55	1.32	T 17 B 18 A 18	T 37 B 36 A 37
TP4	B1	0.4	BS2.5	150	1.52	1.32	T 16 B- 13 A 15	T 25 B 44 A 34

LABORATORY CORE REPORT

Page of
Date 25-Sep-1996

LABORATORY REPORT No.: 01437/01437/1
Sample No.: Z0147/01437/1

Scheme Client Location	Freightliner Access, Jersey Marine HEAD OF ENGINEERING (NPTCBC) T3		
Surface Material Logged By Operators	Concrete GM GJE & NPD		
Core Drilled Road Condition	24-Sep-1996 Sound	Core Diameter Road Texture	150 mm Rough

Layer Ref.	Layer Thickness	Layer Type	Agg. Size	Grading	Binder Type	Main Aggregate	Voids	Recovery
A	220	Other (see remarks)	20.0	Well Graded	Cement	Limestone	Few or None	Totally intact
B	90	Granular Sub-Base	40.0	Well Graded	None	Slag	Few or None	Total but broken/fragmented
C	130	Granular Sub-Base	40.0	Well Graded	None	Limestone	Few or None	Incomplete

Remarks: LAYER A IS A CONCRETE SLAB WITH 8mm DIAMETER REINFORCEMENT, 140mm FROM TOP SURFACE

HEAD OF ENGINEERING (NPTCBC)
DEPT. OF TECHNICAL SERVICES
CIVIC CENTRE
PENLLERGAER
SWANSEA

SA4 1GH

P.T.E. Tucker
Laboratory Manager

LABORATORY TEST REPORT

LABORATORY REPORT No.: 01437/96/L01437

Page 1 of 1
Date 25-Sep-1996

Sample No. : L01437

COMPRESSIVE STRENGTH OF CONCRETE CORES TO B.S. 1881: PART 120 1983

Scheme Client Site Ref. Location	Freightliner Access, Jersey Marine HEAD OF ENGINEERING (NPTCBC) FREIGHTLINER ACCESS ROAD, JERSEY MARINE T3		
Material Specification	FIELDWORK		
Contractor Source			Ticket No:
Date Supplied Date Sampled	24-Sep-1996	Date Received Date Tested	24-Sep-1996 25-Sep-1996

TEST RESULTS

CORE NO.	1
DENSITY Kg/m3	2381
% VOIDS	1.5%
AGE	UNKNOWN
STRENGTH N/mm2	57.5
ESTIMATED IN SITU CUBE STRENGTH N/mm2	56.5
METHOD OF END PREPARATION	CUT & GROUND

Remarks :

MR S. REES
HEAD OF ENGINEERING (NPTCBC)
DEPT. OF TECHNICAL SERVICES
CIVIC CENTRE
PENLLERGAER
SWANSEA

SA4 1GH

P.T.E. Tucker
Laboratory Manager



TESTING
No. 0934

ANCHEM ANALYTICAL LABORATORIES



Mr. P. Tucker, Neath Port Talbot County B.C., Earlswood Materials Laboratory, Neath Abbey Business Park, Neath.	Unit 5a D'Arcy Business Park D'Arcy Way Llandarcy Neath SA10 6EJ Tel : 0792 323223 Fax : 0792 323236
	Laboratory Analysis Report
	No. 17272/96/RJL
	Date 21st October 1996
Sample No. 14636/1 to 4	Date sample received 2/10/96
Date sample tested 3rd to 18/10/96	

Sample

4 Soil Samples from Freightliner Access, Jersey

Marine off Elba Crescent, 01437, labelled:-

14636/1 - T1 B2 1.0.

14636/2 - T2 0.3 - 0.6.

14636/3 - T4 B1 0.4.

14636/4 - T5 B1 0.4.

Not sampled by us.

- We have analysed the above samples as requested in accordance with documented in-house procedures and our results are as follows:-

Signed

(G.D. Cotter)

on behalf of Anchem Analytical Laboratories

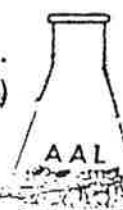
Laboratory Analysis Report No. 17272/96/RJL (Cont.)

	14636/1	14636/2	14636/3	14636/4
pH	8.0	8.0	7.9	7.6
% Material passing a 2mm sieve	50	52	64	94
% Total Sulphate (as SO ₃)	<0.01	0.04	0.08	<0.01
% Loss on Ignition *	12.3	38.8	40.5	8.6
% Material Recovered at SG 1.6*	7	24	38	4
Total Cyanide (as CN) *	<1	<1	1	<1
Total Phenolic Compounds *	2	2	1	6
Toluene Soluble Material *	<50	51000	12000	<50
Mineral Oil *	-	6300	763	-
Total Oil *	-	23000	4500	-
Total Cadmium (as Cd)	1.0	<1	5.5	1.8
Total Lead (as Pb)	158	180	1970	214
Total Chromium (as Cr)	121	153	83	49
Hexavalent Chromium (as Cr) *	<1	<1	<1	<1
Total Mercury (as Hg) *	0.1	<0.1	2.0	0.3
Total Selenium (as Se) *	0.5	0.7	1.6	0.7
Total Copper (as Cu)	-	-	-	109
Total Nickel (as Ni)	-	-	-	30
Total Zinc (as Zn)	-	-	-	395

Results are quoted in mg/Kg (p.p.m.) unless otherwise stated and are expressed on air dried material passing a 2mm test sieve, with the exception of total phenolic compounds which is expressed on an "as received" basis. pH And total sulphate analysis based on 9.5 and 5.5 of British Standard 1377:Part 3:1990, electrometric and gravimetric analysis respectively. Metals with the exception of Chromium VI refer to aqua regia-soluble species, analysis by A.A.S. Mercury and selenium analysed by vapour generation A.A.S. Toluene soluble material refers to oil, pitch, tar, grease compounds etc. Total oil and mineral oil refer to tetrachloroethylene soluble species and are calculated using HMSO parameters, analysis by FTIR. The material recovered at S.G. 1.6 consisted mainly of bituminous and non carbonaceous material with a low content of coal.

* - These analyses are not included within the scope of our NAMAS accreditation.

Signed.....
(G.D. Gottle)



ANCHEM ANALYTICAL LABORATORIES



Unit 5a D'Arcy Business Park D'Arcy Way Llandarcy Neath SA10 6EJ Tel: 01792 323223 Fax: 01792 323236

Mr. P. Tucker, Neath Port Talbot County B.C., Earlswood Material Laboratory, Neath Abbey Business Park, Neath, SA10 7DR.	Laboratory Analysis Report No. 17271/96/RJL
	Date. 21st October 1996
	Date Sample Received. 2/10/96
	Date Sample Tested. 17/10/96.
	Sample No. 14636/2 & 3

Sample

2 Soil Samples, labelled:-
 Freightliner Access Jersey Marine off Elba Crescent.
 14636/2 - T2 0.3 - 0.6, 01437.
 14636/3 - T4 B1 0.4, 01437.

Not sampled by us.

An analysis has been carried out the above samples as requested and the results are as follows:-

PAH

	14636/2	14636/3
Benzo (b) fluoranthene	21.5	0.57
Benzo (k) fluoranthene	12.8	0.22
Benzo (a) pyrene	31.6	0.54
Benzo (ghi) perylene	19.8	0.67
Fluoranthene	69.2	0.93
Indeno (1,2,3, - cd) pyrene	14.6	0.35
Total PAH	170	3.3

All results are quoted in mg/Kg (p.p.m.).

Signed: G.D. Cottle (G.D. Cottle)
 On Behalf of Anchem Analytical Laboratories.





Consulting

TEST CERTIFICATE

SAMPLE REF NO: S1223039

Hyder Environmental
Southern Laboratories
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Bridgend CF31 3NA

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Fax: +44 (0)1656 646 525


Earlswood Materials Laboratory
Newby House
Neath Abbey Business Park
Neath Abbey
Neath

Report Date 31-Oct-96

Date Received 24-Oct-96
Date Completed 31-Oct-96

SAMPLE DESCRIPTION 01437 T2 0.3-0.6M

Determinand	Result	Units	Method	Lab No
Dried Solids % Total	78.5	%		1
GC Mass Spec. - see attached report				1
Persistent Mineral Oil Dry Weight	1760	mg/kg		1


I. Down
Operations Manager-South

Page 1 of 1

Further information on methods of analysis available on request
† Indicates determinand analysed by external sub-contractor
N - see attached comments
Laboratory Accreditation Nos 1(Bridgend) = 1229 2(Ruabon) = 0897



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Neath Abbey
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SA10 7DR

DS/RG/F1/6411

31 October 1996

GCMS ANALYSIS

DATE TAKEN: 29/10/96

SAMPLE DESCRIPTION: 01437 T2 0.3-0.6M

Sample S1223039 was found to contain the following:

DETERMINAND	RESULT	UNITS
D ₈ Naphthalene (Internal Std)	1000	µg/kg
Naphthalene	1050	µg/kg
Methyl Naphthalene Isomer	858	µg/kg
Methyl Naphthalene Isomer	332	µg/kg
1,1'-Biphenyl	352	µg/kg
Dimethyl Naphthalene Isomers	2059	µg/kg
1,2-Dihydro Acenaphthalene	1058	µg/kg
Methyl Biphenyl Isomer	200	µg/kg
Dibenzofuran	995	µg/kg
Trimethyl Naphthalene Isomers	1835	µg/kg
9H-Fluorene	1672	µg/kg
Methyl Biphenyl Isomer	275	µg/kg
Methyl Biphenyl Isomer	179	µg/kg
Methyl Dibenzofuran Isomer	1191	µg/kg
Methyl Fluorene Isomer	305	µg/kg
Methyl Fluorene Isomer	337	µg/kg
Methyl Fluorene Isomer	198	µg/kg

Compounds found were identified by library searching against NIST library and quantified relative to D₈ Naphthalene, the internal standard.

D SIMONS
Organic Chemistry Manager

Page 1 of 2

Further information on methods of analysis on request

*Indicates determinand not covered by NAMAS Accreditation

†Indicates determinand analysed by external sub-contractor



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Neath Abbey Business Park
Neath Abbey
Neath
SA10 7DR

DS/RG/F1/6411

31 October 1996

GCMS ANALYSIS

DATE TAKEN: 29/10/96

SAMPLE DESCRIPTION: 01437 T2 0.3-0.6M

Sample S1223039 was found to contain the following:

DETERMINAND	RESULT	UNITS
9H-Fluoren-9-Ol	231	µg/kg
Dibenzothiophene	440	µg/kg
Phenanthrene	7722	µg/kg
Anthracene	1915	µg/kg
Methyl Anthracene Isomers	1892	µg/kg
Methyl Anthracene Isomers	1833	µg/kg
Methyl Phenanthrene Isomer	795	µg/kg
2-Phenylnaphthalene	997	µg/kg
Fluoranthene	6822	µg/kg
Pyrene	5605	µg/kg
Methyl Pyrene Isomers	2638	µg/kg
Triphenylene	796	µg/kg
Benz A Anthracene	1366	µg/kg
Benzo J Fluoranthene Isomer	584	µg/kg
Benzo J Fluoranthene Isomer	140	µg/kg
Benzo J Fluoranthene Isomer	148	µg/kg

All the above are PAH compounds typical of coal tar. In addition to the above the sample was found to contain approximately 30,000 micrograms per kilogram of hydrocarbons typical of diesel or fuel oil.

Compounds found were identified by library searching against NIST library and quantified relative to D₈-Naphthalene, the internal standard.


D SIMONS
Organic Chemistry Manager

Page 2 of 2

Further information on methods of analysis on request

*Indicates determinand not covered by NAMAS Accreditation

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Consulting

TEST CERTIFICATE

SAMPLE REF NO: S1223040

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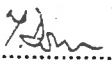
Report Date 31-Oct-96

Date Received 24-Oct-96

Date Completed 31-Oct-96

SAMPLE DESCRIPTION 01437 T4 B1 0.4M

Determinand	Result	Units	Method	Lab No
Dried Solids % Total	86.8	%		1
GC Mass Spec. - see attached report				1
Persistent Mineral Oil Dry Weight	607	mg/kg		1


I. Down
Operations Manager-South

Page 1 of 1

Further information on methods of analysis available on request
† Indicates determinand analysed by external sub-contractor
N - see attached comments
Laboratory Accreditation Nos 1(Bridgend) = 1229 2(Rumcor) = 0897



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31 October 1996

GCMS ANALYSIS

DATE TAKEN: 30/10/96

SAMPLE DESCRIPTION: 01437 T4 0.4M

Sample S1223040 was found to contain the following:

DETERMINAND	RESULT	UNITS
D ₈ Naphthalene (Internal Std)	100	µg/kg
Naphthalene	337	µg/kg
Methyl Naphthalene Isomer	717	µg/kg
Methyl Naphthalene Isomer	168	µg/kg
1,1'-Biphenyl	221	µg/kg
Dimethyl Naphthalene Isomers	1839	µg/kg
1,2-Dihydro Acenaphthalene	315	µg/kg
Dibenzofuran	245	µg/kg
Trimethyl Naphthalene Isomers	766	µg/kg
Methyl Biphenyl Isomer	175	µg/kg
Methyl Dibenzofuran Isomer	138	µg/kg
Methyl Dibenzofuran Isomer	336	µg/kg
Methyl Fluorene Isomer	146	µg/kg
Methyl Fluorene Isomer	186	µg/kg
9H-Fluoren-9-One	148	µg/kg
Dibenzothiophene	163	µg/kg
Phenanthrene	1937	µg/kg
Anthracene	349	µg/kg
Methyl Anthracene Isomer	2002	µg/kg
Dimethyl Phenanthrene Isomer	291	µg/kg

Compounds found were identified by library searching against NIST library and quantified relative to D₈ Naphthalene, the internal standard.

D SIMONS
Organic Chemistry Manager

Page 1 of 2

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31 October 1996

GCMS ANALYSIS

DATE TAKEN: 30/10/96

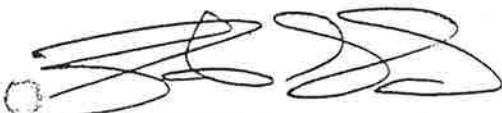
SAMPLE DESCRIPTION: 01437 T4 0.4M

Sample S1223040 was found to contain the following:

DETERMINAND	RESULT	UNITS
Fluoranthene	2713	µg/kg
Pyrene	2406	µg/kg
Triphenylene	1020	µg/kg
Benz A Anthracene	1025	µg/kg

All the above are PAH compounds typical of coal tar. In addition to the above the sample was found to contain approximately 40,000 micrograms per kilogram of hydrocarbons typical of diesel or fuel oil, and approximately 560,000 micrograms per kilogram of hydrocarbons typical of a lubricating oil eg. engine oil.

Compounds found were identified by library searching against NIST library and quantified relative to D₈ Naphthalene, the internal standard.



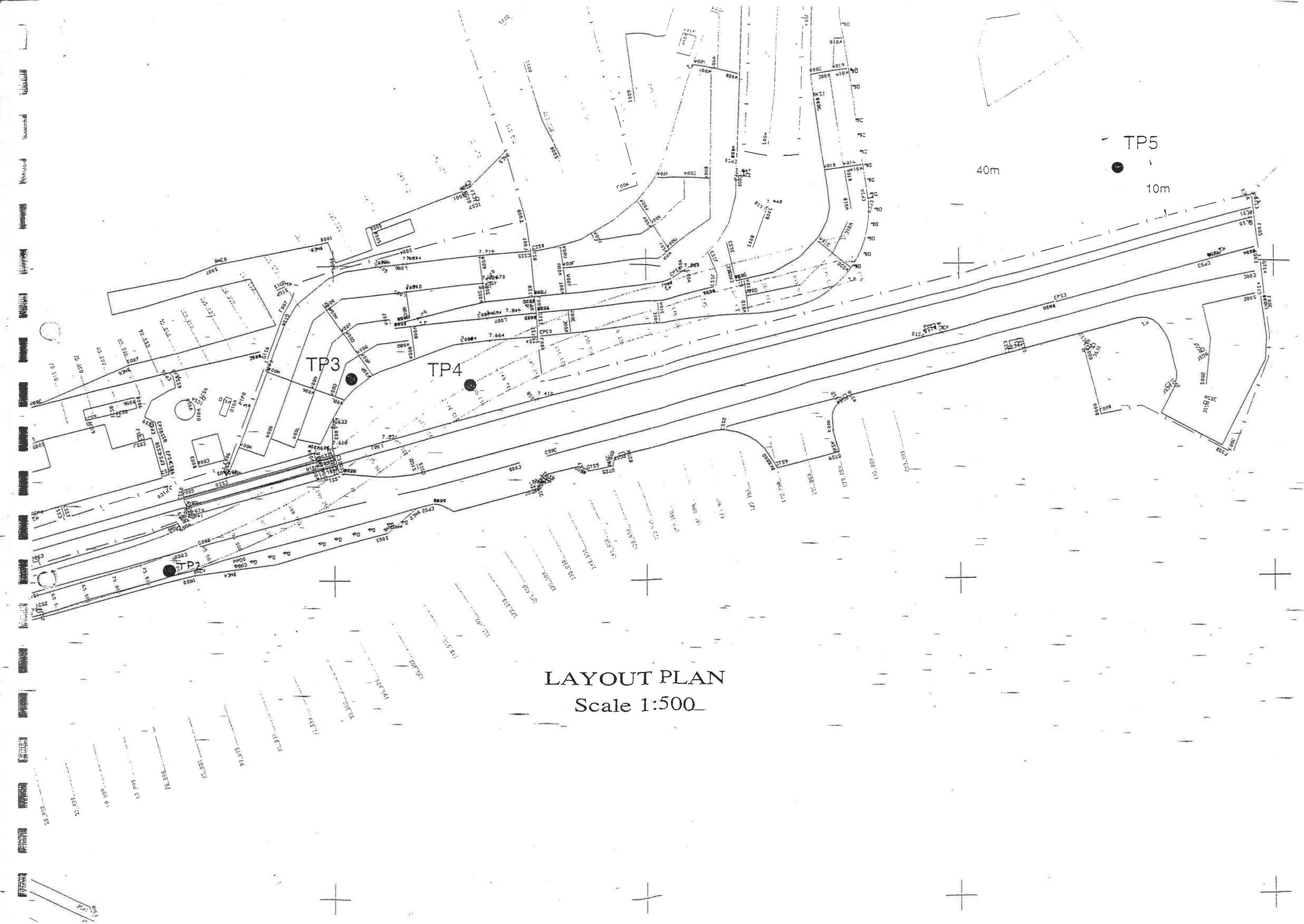
D SIMONS
Organic Chemistry Manager

Page 2 of 2

Further information on methods of analysis on request

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Golder Associates (UK) Ltd.

CONSULTING GEOTECHNICAL AND MINING ENGINEERS

REPORT TO NEATH BOROUGH COUNCIL
ON GROUND INVESTIGATION AT
THE FREIGHTLINER TERMINAL SITE,
JERSEY MARINE

Distribution:

1 copy - Neath Borough Council

1 copy - Golder Associates

March 1989

8853018

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1. INTRODUCTION

Golder Associates (UK) Ltd. have been instructed by Neath Borough Council, letter reference PH/VLH.10.20, dated 11th August 1988, to undertake a ground investigation at the former Freightliner Terminal site, Jersey Marine (Figure 1). The object of the ground investigation was to determine the nature and extent of the superficial deposits present within the site in order to allow an assessment of the foundation requirements on the site.

This report contains a factual account of the ground investigation undertaken, including trial pit and borehole logs and laboratory test results. Engineering recommendations relating to the geotechnical aspects of foundation design and construction are also included.

2. THE SITE AND PROPOSED DEVELOPMENT

The site is located to the west of Jersey Marine in the vicinity of Crymlyn Burrows (Figure 2). A number of railway sidings occupy the north of the site beyond which is a large expanse of marshy land referred to as Crymlyn Bog. The southern site boundary is located adjacent to Ford Motor Corporation's Swansea Motor Components factory. The southern areas of the site are occupied by dense tree and shrub growth. The eastern site boundary borders waste land which is occupied by dense trees and shrubs with some evidence of recent tipping of made ground. The western boundary borders derelict land previously occupied by offices of the former Freightliner company.

The site is relatively flat lying and occupies approximately 6.8 hectares. The site is roughly rectangular in shape and is extensively covered with a concrete hardstanding. The proposed development will comprise the construction of a number of single storey light industrial developments of conventional portal frame design. Site infrastructure, comprising the construction of access roads and parking areas and installation of services will also be required. The proposed site layout is shown in Figure 2.

3. GEOLOGY

A general review of the site geology has been undertaken by examination of the 1:10,560 geological map of the area (Reference 1). The site is shown to be underlain by extensive superficial deposits, a significant proportion of which comprise wind blown sand of recent origin. Bedrock comprising essentially sandstone and mudstone of the Lower Pennant Measures of the Upper Coal Measures Series, is present beneath these deposits at depths in excess of 20m. A borehole drilled within Ford Motor Corporation's factory, approximately 130m south of the site, encountered up to 17m of superficial deposits comprising sand and clay overlying sandstone and mudstone bedrock. The ground investigation described in this report encountered similar conditions to those described above.

It is considered unlikely that the site is underlain by shallow coal mineworkings and therefore the threat posed to surface development by mining related ground subsidence is considered remote.

4. GROUND INVESTIGATION

4.1 General

Fieldwork, comprising the excavation of fourteen trial pits and five cable percussion boreholes, was undertaken in April and November 1988 respectively. The trial pit and borehole locations are shown in Figure 2. The fieldwork was undertaken at all times under the supervision of a member of Golder Associates engineering staff, who supervised the excavation and logged all the trial pits and boreholes. Detailed trial pit and borehole logs are given in Appendix I. All fieldwork was carried out in accordance with BS 5930 (Reference 2).

4.2 Trial Pits

The trial pits were excavated to determine the ground conditions at shallow depth and obtain soil samples for laboratory testing. A total of fourteen trial pits were excavated by a JCB MK 3 belonging to Stadium Transport Ltd. of Neath. The pits were excavated to a maximum depth of 3.08m. Large bulk samples were taken at various depths and generally at each significant change of soil type. Special attention was paid at all times to the recording of groundwater entries and pit wall stability.

4.3 Cable Percussion Boreholes

Five cable percussion boreholes were drilled at the positions shown on Figure 2, by BB Drilling Ltd. of Nottingham. Standard penetration tests were undertaken at approximately 1m intervals to approximately 10m below ground level and thereafter at approximately 1.5m intervals to determine the consistency/relative density of the superficial deposits. In general, large bulk samples were taken over the test range for detailed logging and laboratory testing chiselling techniques were occasionally employed. In order to aid boring in the made ground. Water was added to the borings in order to maintain a positive water head and prevent disturbance at the base of boreholes in sand and silt deposits and to assist borehole advancement and sample recovery. The majority of boreholes were terminated at 20m below existing ground level.

Groundwater entries and levels were recorded in two boreholes, however, since water was added during boring it was not always possible to establish accurately the groundwater table. The depths of strata encountered, samples taken, in-situ tests carried out and test results are given on the borehole logs, Appendix I.

4.4 Laboratory Testing

Laboratory testing was carried out on large bulk samples recovered from the trial pits and boreholes. The following tests were undertaken:

-
- Atterberg limits and moisture content determinations on samples displaying cohesive properties.
 - Particle size distribution tests by sieve and hydrometer analysis on granular and cohesive samples respectively.
 - Chemical tests to determine the sulphate, pH and organic matter content of samples of natural and made ground deposits.

The chemical tests and hydrometer analyses were undertaken by Thyssen Ltd. of Llanelli and University College, Swansea. The natural moisture content, Atterberg limit tests and the particle size distribution tests by sieve analysis were undertaken by Golder Associates (UK) Ltd. All laboratory tests were carried out in accordance with BS 1377 (Reference 3). The laboratory test results are presented in Appendix II.

5. GROUND CONDITIONS

5.1 General

The results of this investigation indicate that the general ground conditions at the site comprise made ground of variable thickness and composition, overlying thick natural deposits of recent and alluvial origin. Groundwater was encountered at shallow depth in all the trial pits and boreholes. A geological section through the site is shown in Figure 3.

5.2 Made Ground

Made ground was encountered in all the trial pits and the majority of boreholes. The deposit is characteristically heterogeneous in composition and variable in thickness and comprises three general material types as follows:

- Loose gravel, cobble and boulder sized angular ash, slag and coal fragments
- Loose silty fine to medium sand with some to occasional cobble and boulder sized brick and masonry fragments
- Medium dense silty fine to medium sand

The full thickness of the made ground deposits was determined in all the trial pits and boreholes. A maximum recorded thickness of 3.5m was encountered in borehole 2, however, in the majority of cases this deposit ranges in thickness from 1 to 1.5m.

Standard penetration tests (SPT) were undertaken at various depths in these deposits and the results indicate a medium dense to dense relative density with 'N' values in the range of 21 to 33 and a mean of 25. It should be stressed that a relatively small number of tests were carried out and therefore the results may not be exactly representative of the conditions across the entire site.

A single particle size distribution test by sieve analysis was undertaken on a sample of made ground recovered from borehole 2. The result of this analysis confirms the deposit as comprising essentially a sandy fine to coarse gravel. Due to unavoidable sampling bias material larger than cobble size is excluded from the test. Due to the heterogeneous nature of made ground material it is likely that material of cobble size or greater should be present within the made ground at this site. The particle size distribution test curve is given in Appendix II.

Five chemical tests were undertaken on selected samples of made ground. Total sulphate concentrations lie in the range 0.019 to 0.45 percent and pH values in the range 7 to 9.9. The results are given in Appendix II.

5.3 Recent Deposits

Recent deposits were encountered below the made ground deposits in all the boreholes and trial pits. The deposit is characterised by moderately thick deposits of wind blown sand with peat bands and occasional clay and silt horizons. The following material types have been identified at the site:

- Medium dense to dense slightly silty fine to medium sand with occasional fine to coarse subrounded gravel, cobbles and shell fragments (wind blown sand).
- Spongy odorous peat with partially decayed wood fragments.
- Firm very silty clay/clayey silt.

This deposit was fully penetrated by all the boreholes. A maximum recorded thickness of 12.50m was encountered in borehole 1A, however, in the majority of cases typical thicknesses lie in the range of 4.5 to 8m. A thick peat band was encountered in all the boreholes at 3.5 to 5.5m below existing ground level. The peat is typically thickest in the western and central areas of the site where boreholes 1A, 1, 2 and 3, encountered a 1 to 1.5m thick peat band at 3.5 to 4m below existing ground level. Elsewhere, the peat band is much thinner e.g. 0.5m thick in borehole 4.

Standard penetration tests were undertaken at various depths within these deposits. The resulting 'N' values exhibit a wide range from 4 to 44 and a mean of 21, thus confirming a medium dense relative density. The majority

of these tests were undertaken in the wind blown sand. A single test undertaken in clay/silt material in borehole 1A recorded an 'N' value of 11. A plot of SPT 'N' value versus depth is shown in Figure 4.

A number of particle size distribution tests by sieve analysis were undertaken on selected bulk samples of the wind blown sand. The results confirm the deposit as comprising essentially a silty fine to medium sand with occasional fine to medium gravel. The curves exhibit a uniform grading, confirming the sand to be of wind blow origin. The particle size distribution test curves are given in Appendix II. Two chemical tests were undertaken on samples of wind blown sand. Total sulphate concentrations lie in the range 0.014 to 0.019 percent and pH value in the range 8.4 to 9.4. Three organic matter content tests were undertaken on samples of peat recovered from the boreholes. The resulting organic matter contents, determined by loss on ignition at 600 degrees centigrade, lie in the range 37.36 to 65.90 percent. Chemical test results are given in Appendix II.

5.4 Alluvial Deposits

Alluvial deposits were encountered in all the boreholes at depth below the made ground and recent deposits. The full thickness of these deposits was not determined. A maximum recorded thickness of 13m was encountered in borehole 4. The deposit can be broadly divided into two principal material types as follows:

- Loose and medium dense/soft and firm sandy clayey and very clayey silt, and slightly to very silty clay with occasional to some fine to coarse gravel, shell fragments with occasional organic traces.

- Loose and medium dense silty fine to medium sand.

Standard penetration tests were undertaken in these deposits at various depths. The resulting 'N' values lie in the range 4 to 29 with a mean of 15, thus confirming a medium dense relative density. A plot of SPT 'N' value versus depth for the alluvial deposits is shown in Figure 5. Based on these results, it is possible to estimate the equivalent undrained shear strength of these materials by use of the following approximate empirical relationship (Reference 4):

$$\text{shear strength} = 6 \text{ 'N' (kN/m}^2\text{)}$$

where 'N' = SPT result

This applies to materials with plasticity indices up to 15, as is the case for the alluvial deposits at this site. The resulting equivalent undrained shear strengths lie in the range of approximately 30 to 130 kN/m², indicating a consistency ranging from soft to firm/stiff.

Five natural moisture content and Atterberg limit tests were undertaken on selected samples of cohesive material recovered from the boreholes. Natural moisture contents lie in the range 30 to 40 percent. Liquid and plastic limits lie in the range 24 to 37 and 12 to 27 percent respectively.

Particle size distribution tests by hydrometer analysis were undertaken on two samples of silt/clay. The resulting test curves are presented in Appendix II. As shown, the samples comprise essentially a sandy and very sandy clayey silt with some to occasional gravel.

5.5 Groundwater

Groundwater was encountered in all the trial pits and boreholes. Moderately strong and strong seepage rates were observed from the recent deposits and at the interface between the made ground and the underlying recent deposits at depths ranging from 1 to 2m below existing ground level. Water was added during boring of the cable percussion boreholes in order to maintain a positive water head and hence reduce disturbance at the base of the borehole. In such cases, it was not possible to identify the depth of any groundwater seepage.

Groundwater levels are subject to seasonal variations and therefore the levels recorded during the fieldwork period should be regarded as a guide only. We do not anticipate significant-tidal variations in the ground water level at this site.

6. ENGINEERING RECOMMENDATIONS

6.1 General

The proposed development consists of a number of light industrial single storey buildings and associated access roads. The future use of the units is not known at present thus a design load of 30 kN/m^2 has been estimated as a conservative upper limit for the purpose of foundation recommendations. The size of the buildings is in the order of 45 by 18m.

Ground conditions at the site consist of made ground overlying recent deposits of wind blown sand and peat which in turn overlie alluvial deposits of a silty clayey nature. A high ground water table at 1m below ground level was encountered on the site.

6.2 Foundation Design and Construction

The assumed ground profile and associated engineering parameters utilised in analysing the foundation design are given in Figure 6. The allowable bearing capacity of the medium dense wind blown sand below the made ground will be approximately 100 kN/m^2 which is adequate to support the anticipated imposed loads.

The major problem associated with building on the proposed site is the order of magnitude of settlement resulting from the imposed load. The settlement is made up of three components:

- immediate settlement
- consolidation settlement
- secondary compression

The various options for foundation design are discussed below together with a critique of their anticipated performance with particular emphasis on settlement.

6.2.1 Conventional Spread Foundations

For low loadings of 30 kN/m^2 conventional strip footings of say 1m wide at a nominal depth of 0.5m are generally adequate for transferring imposed loads to the ground. However, in this case the anticipated total settlements will be in the order of 75mm . This gives a considerable range of differential settlement, and angular distortion up to $1:150$. Since the future use of the buildings is not known at present it is not possible to comment on whether or not this is a tolerable value. It is however, not recommended to utilise strip footings at this site since the associated settlements could prove detrimental to structural integrity of the buildings.

6.2.2 Narrow Strip (trench fill) Foundations

To avoid the detrimental effects of excessive settlement due to the peat it may be possible to found on the medium dense sandy deposits below the peat layer. To construct this foundation, a trench could be excavated to a

depth below the peat and filled with suitably compacted lean mix concrete. Following this, conventional spread foundations could be placed directly onto the concrete trench fill.

However, construction of this foundation configuration is likely to be impractical due to the depth of excavation for the trenches: in some parts of the site up to 6m below ground level, and the need to dewater on a large-scale and/or provide shuttering to stabilise the excavation.

6.2.3 Raft Foundation

Often a raft is chosen as a foundation solution when large differential settlements are thought to be problematic. Calculations based on a large flexible raft 45m by 18m, close to ground surface, have yielded total settlements in the order of 100mm. The zone of influence of such a large loaded area extends to the firm clays of the alluvial deposits at a depth of approximately 10m, and their compression adds significantly to the resulting large settlements.

An alternative configuration is that such a raft be split into three discrete rigid rafts of smaller dimensions, 15m x 18m. Analysis of this configuration shows that total settlements are in the order of 65mm and differential settlements leading to angular distortion of up to 1:200 are still possible.

It is therefore not recommended to adopt this option, as tolerable settlements are not known at present.

6.2.4 Small Diameter Driven Piles to Alluvial Deposits

As is the case at this site, where poor ground conditions are encountered close to the ground surface, the appropriate solution may be to found the structure on piles driven to a suitable depth to mobilise adequate strength to support the structure.

An analysis for driven reinforced concrete piles to support a load of 30 kN/m² over an area of one factory unit shows that a suitable configuration would be 0.5m diameter piles on a grid spacing of 3m centres in the order of 15 to 20m long. This configuration will mobilise the required carrying capacity with an associated factor of safety of approximately 3. No significant settlements are associated with this option, and although it is likely to be an acceptable solution, the cost of piling and associated work is generally quite high, and may not be warranted as a cost effective solution in this case.

6.2.5 Ground Treatment Prior to Construction

Ground treatment prior to construction in the form of preloading would cause the majority of the predicted settlement (see Section 6.2.3) to take place within a pre-determined time period. Settlement in the granular material is not time dependent and will take place immediately the preload is placed. Consolidation settlement and secondary compression are both time dependent, and the latter, although of relatively small magnitude, will continue to occur after 100 per cent consolidation has taken place.

The calculated time period for 90 per cent consolidation of the compressible layers will be approximately 40 days, during which most of the settlement will have taken place. Further settlement will occur after this period associated with the remainder of the consolidation settlement plus secondary compression, but will only contribute approximately an additional 10 per cent to the total settlement.

The preloading should impose a load equal to or greater than the anticipated uniformly distributed load from the buildings. It is recommended that during the preloading stage, monitoring should be carried out of the excess pore water pressures in selected strata, including the compressible peat layer, in addition to monitoring of total and relative settlements within the strata. This will enable an accurate determination of the progress of the consolidation settlement to be made, which is necessary to provide instructions to remove the preload and then commence construction. The anticipated time period of 40 days is based on assumed material properties and may vary according to actual material properties existing on site.

On removal of the preload and prior to construction some rebound of the ground will occur, and will be in the order of 30 per cent of the total settlement occurring under the preload. Thus the overall effect of the preloading procedure will cause 70 per cent of the predicted settlement to have occurred by the start of construction phase. Upon removal of the preload, the natural ground surface should be proof rolled and prepared

(e.g. by the addition of a base fill if required) for structural foundations. Large raft foundations would then be a suitable foundation with associated total settlements in the order of approximately 25mm.

6.3 Recommendations

In the previous sub-section, various options for foundation design are considered. Strip footings and narrow trench fill foundations are dismissed due to the likelihood of excessive settlement and construction difficulties and costs respectively. The option of a raft bearing on natural untreated ground is unsatisfactory also due to likelihood of excessive settlements.

A piled foundation is likely to incur a relatively high cost. The high cost of piling is associated with the structural design of the piles, pile caps and capping beams together with material costs, and the cost of the relatively high degree of supervision required in their installation. Alternatively, preloading requires only occasional monitoring and would not involve additional foundation material costs greater than that required for a raft foundation. The major cost associated with preloading is the acquisition and importation of fill onto the site, but is likely to be lower than the cost of design and installation of piles. A suitable fill material would consist of general hardcore, builder's rubble or similar material, but excluding any organic materials or household refuse. Preload fill should be placed only over the areas of the proposed structures or roadways.

Alternatively it may prove worthwhile to investigate the option of utilising the existing hardstanding which covers a large area of the site to support the proposed structures. An appraisal of the current condition of the concrete and mesh reinforcement could offer an opportunity for substantially reducing the cost of foundations should it be possible to found directly on the hardstanding. The relatively light loads of the proposed single storey industrial units may not exceed loads previously imposed on the hardstanding. Past usage of the site as a freight terminal handling containers suggests that the existing slab may offer adequate support for the anticipated development. It is therefore recommended that further investigation into this aspect of the site be carried out as part of a detailed foundation design for structures on the site, as if it proves possible to found the factory units on the hardstanding without the need for ground treatment or piling, this will result in a considerable cost saving to the project.

6.4 Stability of Excavations

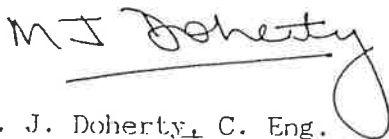
Excavations which may be necessary on site for the installation of services may be made stable by forming temporary side slopes of 1.5 horizontal to 1 vertical. However, this is only the case for excavation up to 1m below present ground level. For depths below this level, significant seepage rates due to the ground water level being at shallow depth, may require additional stabilisation measures. Pumping from a sump located at the bottom of the excavation may be adequate to control seepage in some excavations. It is anticipated that temporary or permanent sheeting will

be required for excavations in excess of approximately 1.5m deep or for excavations which are to be left open for a long period of time. Seepage rates into excavations will be dependent on the prevailing weather conditions and may vary with tidal conditions.

6.5 Subsurface Concrete

The results of chemical tests to determine sulphate levels indicate concentrations in the range 0.014 to 0.45 percent. Based on the upper value recorded in this range, it is recommended that Class 2 concrete should be used in cases where subsurface concrete is to be used.

GOLDER ASSOCIATES (UK) LTD.



M. J. Doherty, C. Eng.



P. H. Seymour, C. Eng.

LIST OF REFERENCES

1. British Geological Survey of Great Britain. Geological Map Sheet No. SS 96 SE. Scale 1:10,560.
2. British Standards Institute 5930, 'Site Investigation', 1981.
3. British Standards Institute 1377, 'Methods of Testing Soils for Civil Engineering Purposes', 1975.
4. Site Investigation - A Handbook for Engineers C.R.I. Clayton, N.E. Simons, M. C. Matthews. Granada 1982.

APPENDIX I - RESULTS OF FIELD WORK

Key to Trial Pit and Borehole Logs

Trial Pit Logs

Borehole Logs

KEY TO TRIAL PIT AND BOREHOLE LOGS

D	disturbed sample, jar
B	disturbed sample, bulk
U102	undisturbed sample, 102mm diameter
U102*	undisturbed sample, no recovery
S(56)	standard penetration test ('N' value - blows/300mm)
S(100)*	standard penetration test, full 300mm penetration not achieved, 'N' value obtained by extrapolation.
S(50r)	standard penetration test, refusal to driving, (penetration of less than 75mm for 50 blows)
C(46)	cone penetration test ('N' value - blows/300mm)
V(30)	field vane test (undrained shear strength - kN/m).

NOTES:

1. Shell and auger boring techniques have been used in this investigation. These methods inevitably result in some mixing of layered soils. In addition, fine materials may be washed from granular soils during the drilling.
2. The groundwater levels shown on the exploratory hole records are those observed at the time of the investigation. The rate of boring may not allow the recording of equilibrium water levels. Groundwater levels may be subject to seasonal variation.

KEY TO TRIAL PIT AND BOREHOLE LOGS (Cont'd...)

3. It was frequently not possible to inspect strata in situ because of unstable conditions in the trial pits. The density of cohesionless strata and shear strengths of cohesive strata have therefore been estimated from excavated spoil and may vary from those in situ.
4. Any comments made in this report are based on information at exploratory hole locations and it should be noted that variations may exist between these holes.
5. It should be noted that a comprehensive study of all available historical records e.g. old Ordnance Survey maps, has not been carried out. The comments provided in this report are based on the results of exploratory holes, together with a review of selected data.



PROJECT		Freight Liner, Jersey Marine				TRIAL PIT No. 1	
CLIENT		Neath Borough Council		CONTRACTOR		Stadium Transport	
MACHINE TYPE		JCB MkIII		LOCATION		See site plan	
SIZE OF PIT		1 x 5 x 0.5		GROUND SURFACE ELEVATION, mOD		LOGGED BY GduP	
DATE EXCAVATED		18.4.88		FINAL DEPTH, m		3.08	
DOWNHOLE DEPTH, m	SAMPLES/TESTS		SYMBOLIC LOG	ELEVATION, mOD	DEPTH, m	GEOLOGICAL DESCRIPTION	
	DEPTH, m						
	FROM	TO					
0						<p>Loose black fine to coarse angular gravel composed of ash and coal particles many cobbles and occasional boulders. (MADE GROUND)</p>	
1	1.00	1.50	1	B			
2	2.00	3.00	2	B	2.00	<p>Medium dense pale to dark brown slightly silty fine to medium SAND with some rootlets. (RECENT DEPOSITS)</p>	
3					3.08		
REMARKS							
1. Strong groundwater seepage at 1.3m.							
SCALE 1 : 25		Golder Associates			TRIAL PIT LOG		PROJECT No. 8853018

PROJECT		Freight Liner, Jersey Marine		TRIAL PIT No. 2	
CLIENT		Neath Borough Council		SHEET 1 of 1	
MACHINE TYPE		JCB MKIII		CONTRACTOR Stadium Transport	
SIZE OF PIT		1 x 5 x 0.5		LOCATION See site plan	
DATE EXCAVATED		18.4.88		GROUND SURFACE ELEVATION, mOD	
				FINAL DEPTH, m 2.44	
LOGGED BY		GduP		DRAWN BY	
				GduP	

DOWNHOLE DEPTH, m	SAMPLES/TESTS				SYMBOLIC LOG	ELEVATION, m.O.D	DEPTH, m	GEOLOGICAL DESCRIPTION
	DEPTH, m		No.	TYPE				
	FROM	TO						
0								

REMARKS			
1. Groundwater seepage at 1.5m.			
SCALE 1:25	Golder Associates	TRIAL PIT LOG	PROJECT No. 8853018



PROJECT	Freight Liner, Jersey Marine		TRIAL PIT No. 3
CLIENT	Heath Borough Council	CONTRACTOR	Stadium Transport
MACHINE TYPE	JCB MH111	LOCATION	See site plan
SIZE OF PIT	1 x 5 x 0.5	GROUND SURFACE ELEVATION, m O.D.	LOGGED BY GduP
DATE EXCAVATED	16.4.88	FINAL DEPTH, m	DRAWN BY GduP

DOWNHOLE DEPTH, m	SAMPLES/TESTS				SYMBOLIC LOG	ELEVATION, m O.O.	DEPTH, m	GEOLOGICAL DESCRIPTION
	DEPTH, m		No.	TYPE				
	FROM	TO						
0	0.00	0.92	1	B				Loose black sandy gravel sized ash with occasional cobbles (MADE GROUND)
1	0.92	2.30	2	B			0.92	Medium dense yellow brown fine to medium SAND (RECENT DEPOSITS)
2							2.30	
3								
4								

REMARKS

1. Strong groundwater seepage at 2.3m.
2. Unstable pit walls at 2.3m

PROJECT		Freight Liner, Jersey Marine		TRIAL PIT No. 5	
CLIENT		Neath Borough Council		CONTRACTOR Stadium Transport	
MACHINE TYPE		JCB MkIII		LOCATION See site plan	
SIZE OF PIT		1 x 5 x 0.5		GROUND SURFACE ELEVATION, mOD	
DATE EXCAVATED		16.4.88		FINAL DEPTH, m 2.40	
LOGGED BY		Gdup		DRAWN BY Gdup	

DOWNHOLE DEPTH, m	SAMPLES/TESTS				SYMBOLIC LOG	ELEVATION, m O.D.	DEPTH, m	GEOLOGICAL DESCRIPTION
	DEPTH, m		No.	TYPE				
	FROM	TO						
0	0.00	1.00	1	B				Loose black sandy gravel composed of ash with occasional cobbles (MADE GROUND)
1							1.00	
2								Medium dense yellow brown/light grey fine to medium SAND with some rootlets and pockets of dense brown silty SAND (RECENT DEPOSITS)
							2.40	
3								
4								

REMARKS			
1. Strong groundwater seepage at 1.0m.			
SCALE 1: 25	Golder Associates	TRIAL PIT LOG	PROJECT No. 8853018

PROJECT Freight Liner, Jersey Marine		CONTRACTOR Stadium Transport		TRIAL PIT No. 6	
CLIENT Neath Borough Council		LOCATION See site plan		SHEET 1 OF 1	
MACHINE TYPE JCB MK1111		GROUND SURFACE ELEVATION, m O.D.		LOGGED BY Gdu1'	
SIZE OF PIT 1 x 5 x 0.5		FINAL DEPTH, m 1.20		DRAWN BY Gdu1'	
DATE EXCAVATED 18.4.88					

DOWNHOLE DEPTH, m	SAMPLES/TESTS				SYMBOLIC LOG	ELEVATION, m.O.D.	DEPTH, m	GEOLOGICAL DESCRIPTION
	DEPTH, m		No.	TYPE				
	FROM	TO						
0	0.00	1.40	1	B				Loose black sandy gravel composed of ash with occasional cobbles. (MADE GROUND)
1						1.40		
							1.70	Medium dense yellow brown/light grey fine to medium SAND with some rootlets and pockets of dense brown silty SAND (RECENT DEPOSITS)
2								
3								

REMARKS

1. Strong groundwater seepage at 1.4m.

PROJECT Freight Liner, Jersey Marine		CONTRACTOR Stadium Transport		TRIAL PIT No. 7	
CLIENT Neath Borough Council		LOCATION See site plan		SHEET 1 of 1	
MACHINE TYPE JCB MkIII		GROUND SURFACE ELEVATION, m.O.D.		LOGGED BY GduP	
SIZE OF PIT 1 x 5 x 0.5		FINAL DEPTH, m 1.50m		DRAWN BY GduP	
DATE EXCAVATED 10.4.88					

DOWNHOLE DEPTH, m	SAMPLES/TESTS				SYMBOLIC LOG	ELEVATION, m O.D.	DEPTH, m	GEOLOGICAL DESCRIPTION
	DEPTH, m		No.	TYPE				
	FROM	TO						
					X			Loose black sandy gravel composed of ash with occasional cobbles. (MADE GROUND)
					X		1.30	
					X		1.50	Medium dense yellow brown/light grey SAND with some rootlets and pockets of dense brown silty SAND. (RECENT DEPOSITS)

REMARKS	
1. Strong groundwater seepage at 1.3m. 2. Pit walls unstable beneath 1.3m. 3. No samples taken.	
SCALE 1:25	Golder Associates TRIAL PIT LOG PROJECT No. 8853018

PROJECT		Freight Liner, Jersey Marine				TRIAL PIT No. 8		
CLIENT		Neath Borough Council		CONTRACTOR		Stadium Transport		
MACHINE TYPE		JCB MkIII		LOCATION		See site plan		
SIZE OF PIT		1 x 5 x 0.5		GROUND SURFACE ELEVATION, mOD		LOGGED BY		
DATE EXCAVATED		18.4.98		FINAL DEPTH, m		1.80		
DRAWN BY		Gdup						
DOWNHOLE DEPTH, m	SAMPLES/TESTS				SYMBOLIC LOG	ELEVATION, mOD	DEPTH, m	GEOLOGICAL DESCRIPTION
	DEPTH, m		No.	TYPE				
	FROM	TO						
0								
1								Loose black sandy gravel composed of ash with occasional cobbles. (MADE GROUND)
2								Medium dense yellow brown/light grey fine to medium SAND with some rootlets and pockets of dense brown silty SAND (RECENT DEPOSITS)
3								
4								
REMARKS								
1. Strong groundwater seepage at 1.2m. 2. Pit walls unstable below 1.2m. 3. No samples taken.								
SCALE 1: 25			Golder Associates			TRIAL PIT LOG		PROJECT No. 8853018

PROJECT		Freight Liner, Jersey Marine		TRIAL PIT No.9	
CLIENT		Neath Borough Council		CONTRACTOR	
MACHINE TYPE		JCR MkIII		Stadium Transoort	
SIZE OF PIT		1 x 5 x 0.5		LOCATION	
DATE EXCAVATED		18.4.88		See site plan	
				GROUND SURFACE ELEVATION, mOD	
				FINAL DEPTH, m	
				2.20	
				LOGGED BY	
				GdUP	
				DRAWN BY	
				GdUP	

DOWNHOLE DEPTH, m	SAMPLES/TESTS				SYMBOLIC LOG	ELEVATION, m.0.0	DEPTH, m	GEOLOGICAL DESCRIPTION
	DEPTH, m		No.	TYPE				
	FROM	TO						
0								Loose black sandy gravel composed of ash with occasional cobbles, (MADE GROUND)
1						1.30		
2								Medium dense yellow brown/light grey fine to medium SAND with some rootlets and pockets of dense brown silty SAND (RECENT DEPOSITS)
						2.20		

REMARKS			
1. Groundwater seepage at 1.8m. 2. Pit walls unstable below 1.8m. 3. No samples taken.			
SCALE 1: 25	Golder Associates	TRIAL PIT LOG	PROJECT No. 8853018

APPENDIX F

— Analytical Results

FREIGHTLINER SITE

PROVISIONAL GROUNDWATER TESTING RESULTS

Laboratory Ref	GW65570	GW65571	GW65572	GW65573	GW65566	GW65568
Client Ref	E1	E2	E3	E4	E5	E6
Sample Date	01-Oct-98	01-Oct-98	01-Oct-98	01-Oct-98	29-Sep-98	29-Sep-98
Arsenic (mg/l)	0.009	0.051	0.028	0.043	<0.005	<0.005
Boron (mg/l)	0.13	0.19	0.18	0.16	0.16	0.12
Cadmium (mg/l)	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005
Chromium (mg/l)	< 0.03	< 0.03	0.07	< 0.03	< 0.03	< 0.03
Chromium 6 (mg/l)	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Copper (mg/l)	0.02	0.04	0.32	0.03	< 0.05	0.03
Lead (mg/l)	< 0.05	0.06	0.18	< 0.05	< 0.05	< 0.05
Mercury (µg/l)	< 0.02	0.14	0.04	0.03	< 0.02	< 0.02
Nickel (mg/l)	0.03	0.06	0.1	< 0.03	< 0.03	< 0.03
Oil ID GC/FID (mg/l)	< 0.15	< 0.15	< 0.15	< 0.15	< 0.15	< 0.15
Selenium (mg/l)	< 0.002	< 0.002	< 0.002	< 0.002	< 0.002	< 0.002
Zinc (mg/l)	0.08	0.26	0.61	0.05	0.03	0.03

PROVISIONAL RESULTS - GROUNDWATER

Laboratory Ref	GW65570	GW65571	GW65572	GW65573	GW65566	GW65568	GW65569
Client Ref	E1	E2	E3	E4	E5	E6	Trip Blank
Sample Date	01/10/98	01/10/98	01/10/98	01/10/98	29/09/98	29/09/98	29/09/98
Units	ug/l	ug/l	ug/l	ug/l	ug/l	ug/l	ug/l
DETERMINAND							
DICHLORODIFLUOROMETHANE	LT 2.0	LT 2.0	LT 2.0	LT 2.0	LT 2.0	LT 2.0	LT 2.0
CHLOROMETHANE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
VINYL CHLORIDE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
TRICHLOROFLUOROMETHANE	62.0	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
1,1-DICHLOROETHENE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
DICHLOROMETHANE	LT 25	LT 25	LT 25	LT 25	LT 25	LT 25	LT 25
TRANS-1,2-DICHLOROETHENE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
1,1-DICHLOROETHANE	1.7	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
2,2-DICHLOROPROPANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
CIS-1,2-DICHLOROETHENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
BROMOCHLOROMETHANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
TRICHLOROMETHANE	LT 1.0	LT 1.0	3.4	LT 1.0	35.0	11.8	LT 1.0
1,1,1-TRICHLOROETHANE	3.2	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
1,1-DICHLOROPROPENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
TETRACHLOROMETHANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
BENZENE	LT 1.0	1.1	LT 1.0	1.0	LT 1.0	LT 1.0	LT 1.0
1,2-DICHLOROETHANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
TRICHLOROETHENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
1,2-DICHLOROPROPANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
DIBROMOMETHANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
BROMODICHLOROMETHANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	10.4	3.9	LT 1.0
TRANS-1,3-DICHLOROPROPENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
TOLUENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
CIS-1,3-DICHLOROPROPENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
1,1,2-TRICHLOROETHANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
TETRACHLOROETHENE	1.2	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
1,3-DICHLOROPROPANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
DIBROMOCHLOROMETHANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	2.0	1.1	LT 1.0
1,2-DIBROMOETHANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
CHLOROBENZENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
1,1,1,2-TETRACHLOROETHANE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
ETHYLBENZENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
M/P XYLENE	LT 2.0	7.7	LT 2.0	4.5	LT 2.0	LT 2.0	LT 2.0
O-XYLENE	LT 1.0	2.5	LT 1.0	2.3	LT 1.0	LT 1.0	LT 1.0
STYRENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
TRIBROMOMETHANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
ISOPROPYLBENZENE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
BROMOBENZENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
1,1,2,2-TETRACHLOROETHANE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
1,2,3-TRICHLOROPROPANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
N-PROPYLBENZENE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
2-CHLOROTOLUENE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
1,3,5-TRIMETHYLBENZENE	LT 1.5	33.9	LT 1.5	31.7	LT 1.5	LT 1.5	LT 1.5
4-CHLOROTOLUENE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
TERT-BUTYLBENZENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
1,2,4-TRIMETHYLBENZENE	LT 1.5	17.6	LT 1.5	9.8	LT 1.5	LT 1.5	LT 1.5
SEC-BUTYLBENZENE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
1,4-DICHLOROBENZENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
P-ISOPROPYLTOLUENE	LT 1.0	6.4	LT 1.0	6.0	LT 1.0	LT 1.0	LT 1.0
1,3-DICHLOROBENZENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
1,2-DICHLOROBENZENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
N-BUTYLBENZENE	LT 1.0	6.6	LT 1.0	6.1	LT 1.0	LT 1.0	LT 1.0
1,2-DIBROMO-3-CHLOROPROPANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
1,2,4-TRICHLOROBENZENE	LT 3.0	LT 3.0	LT 3.0	LT 3.0	LT 3.0	LT 3.0	LT 3.0
HEXACHLOROBUTADIENE	LT 2.0	LT 2.0	LT 2.0	LT 2.0	LT 2.0	LT 2.0	LT 2.0
NAPHTHALENE	LT 3.5	LT 3.5	LT 3.5	LT 3.5	LT 3.5	LT 3.5	LT 3.5
1,2,3-TRICHLOROBENZENE	LT 3.0	LT 3.0	LT 3.0	LT 3.0	LT 3.0	LT 3.0	LT 3.0
TOTAL	68	76	3	61	47	17	0

Gibb Ltd
Freightliner Project
Provisional Report

15/10/98

VOC RESULTS FROM TRIAL PITS

	SO63984 TP1 @ 0.6-1.0m ug/kg	SO63985 TP1 @ 1.9-2.3m ug/kg	SO63986 TP2 @ 0.6-0.7m ug/kg	SO63987 TP2 @ 1.2-1.6m ug/kg	SO63988 TP3 @ 0.3-0.5m ug/kg	SO63989 TP3 @ 0.5-0.65m ug/kg	SO63990 TP4 @ 0.4-0.6m ug/kg	SO63991 TP4 @ 2.5-2.6m ug/kg	SO63992 TP5 @ 0.4-0.6m ug/kg	SO63993 TP5 @ 1.8-2.1m ug/kg	SO63994 TP6 @ 0.5-0.7m ug/kg
DETERMINAND											
DICHLORODIFLUOROMETHANE	LT 20	LT 15	LT 20	LT 200	LT 20	LT 40	LT 20	LT 20	LT 40	LT 20	LT 20
CHLOROMETHANE	LT 15	LT 15	LT 15	LT 150	LT 15	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
VINYL CHLORIDE	LT 15	LT 15	LT 15	LT 150	LT 15	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
TRICHLOROFLUOROMETHANE	LT 15	LT 15	LT 15	LT 150	LT 15	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
1,1-DICHLOROETHENE	LT 25	LT 250	LT 25	LT 2500	LT 25	LT 30	LT 250	LT 25	LT 30	LT 25	LT 250
DICHLOROMETHANE	LT 15	LT 15	LT 15	LT 150	LT 15	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
TRANS-1,2-DICHLOROETHENE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
1,1-DICHLOROETHANE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
2,2-DICHLOROPROPANE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
CIS-1,2-DICHLOROETHENE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
BROMOCHLOROMETHANE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
TRICHLOROMETHANE	LT 10	88.1	LT 10	LT 100	LT 10	86	106	LT 10	86	LT 10	35.7
1,1,1-TRICHLOROETHANE	4.4	49.3	3.2	LT 100	3.1	10.3	51.5	3.7	11.2	3.5	45.3
1,1-DICHLOROPROPENE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
TETRACHLOROMETHANE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
BENZENE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
1,2-DICHLOROETHANE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
TRICHLOROETHENE	1.5	16.4	1.1	LT 100	LT 10	2.8	13.5	LT 10	2.8	LT 10	12.6
1,2-DICHLOROPROPANE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
DIBROMOMETHANE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
BROMODICHLOROMETHANE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
TRANS-1,3-DICHLOROPROPENE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
TOLUENE	30	231	3.2	LT 100	20	20.5	63.9	30	13.3	3.3	60.2
CIS-1,3-DICHLOROPROPENE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
1,1,2-TRICHLOROETHANE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
TETRACHLOROETHENE	LT 10	10.7	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
1,3-DICHLOROPROPANE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
DIBROMOCHLOROMETHANE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
1,2-DIBROMOETHANE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
CHLOROBENZENE	LT 15	LT 15	LT 15	LT 150	LT 15	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
1,1,1,2-TETRACHLOROETHANE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
ETHYLBENZENE	2	32.5	LT 20	LT 200	LT 20	4.7	21	LT 20	LT 40	LT 20	20.2
M/P XYLENE	LT 10	11.8	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
O-XYLENE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
STYRENE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
TRIBROMOMETHANE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
ISOPROPYLBENZENE	LT 15	LT 15	LT 15	LT 150	LT 15	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
BROMOBENZENE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
1,1,2,2-TETRACHLOROETHANE	LT 15	LT 15	LT 15	LT 150	LT 15	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
1,2,3-TRICHLOROPROPANE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
N-PROPYLBENZENE	LT 15	LT 15	LT 15	LT 150	LT 15	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
2-CHLOROTOLUENE	LT 15	LT 15	LT 15	LT 150	LT 15	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
1,3,5-TRIMETHYLBENZENE	LT 15	LT 15	LT 15	LT 150	LT 15	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
4-CHLOROTOLUENE	LT 15	LT 15	LT 15	LT 150	LT 15	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
TERT-BUTYLBENZENE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
1,2,4-TRIMETHYLBENZENE	LT 15	LT 15	LT 15	LT 150	LT 15	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
SEC-BUTYLBENZENE	LT 15	LT 15	LT 15	LT 150	LT 15	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
1,4-DICHLOROBENZENE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
P-ISOPROPYLTOLUENE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
1,3-DICHLOROBENZENE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
1,2-DICHLOROBENZENE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
N-BUTYLBENZENE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
1,2-DIBROMO-3-CHLOROPROPANE	LT 10	LT 10	LT 10	LT 100	LT 10	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
1,2,4-TRICHLOROBENZENE	LT 30	LT 30	LT 30	LT 300	LT 30	LT 60	LT 30	LT 30	LT 60	LT 30	LT 30
HEXACHLOROBUTADIENE	LT 20	LT 20	LT 20	LT 200	LT 20	LT 40	LT 20	LT 20	LT 40	LT 20	LT 20
NAPHTHALENE	LT 35	LT 35	LT 35	LT 350	40	LT 70	LT 35	LT 35	LT 70	LT 35	LT 35
1,2,3-TRICHLOROBENZENE	LT 30	LT 30	LT 30	LT 300	LT 30	LT 60	LT 30	LT 30	LT 60	LT 30	LT 30
TOTAL	10.9	439.8	7.5	0.0	9.1	46.9	180.2	6.7	35.9	6.8	174.0

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VOC RESULTS FROM TRIAL PITS

	SO63995 TP6 @ 1.2-1.4m ug/kg	SO63996 I TP7 @ 0.45-0.7m ug/kg	SO63997 TP7 @ 1.5-2.2m ug/kg	SO63998 TP8 @ 0.3-0.4m ug/kg	SO63999 TP8 @ 1.5-2.0m ug/kg	SO64000 TP9 @ 0.8-1.1m ug/kg	SO64001 TP9 @ 2.5-2.7m ug/kg	SO64002 TP10 @ 0.6-0.7m ug/kg	SO64003 TP10 @ 1.5-2.0m ug/kg
DETERMINAND									
DICHLORODIFLUOROMETHANE	LT 20	LT 40	LT 40	LT 40	LT 20	LT 20	LT 40	LT 20	LT 20
CHLOROMETHANE	LT 15	LT 30	LT 30	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
VINYL CHLORIDE	LT 15	LT 30	LT 30	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
TRICHLOROFLUOROMETHANE	LT 15	LT 30	LT 30	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
1,1-DICHLOROETHENE	LT 15	LT 30	LT 30	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
DICHLOROMETHANE	LT 250	LT 50	LT 50	LT 50	LT 25	LT 25	64.2	LT 25	LT 25
TRANS-1,2-DICHLOROETHENE	LT 15	LT 30	LT 30	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
1,1-DICHLOROETHANE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
2,2-DICHLOROPROPANE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
CIS-1,2-DICHLOROETHENE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
BROMOCHLOROMETHANE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
TRICHLOROMETHANE	316	20	20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
1,1,1-TRICHLOROETHANE	71.9	10.0	10.1	9.5	2.9	3.1	9.1	53.2	2.5
1,1-DICHLOROPROPENE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
TETRACHLOROMETHANE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
BENZENE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
1,2-DICHLOROETHANE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
TRICHLOROETHENE	168	28	3.7	6.9	1.2	LT 10	2.8	13.7	LT 10
1,2-DICHLOROPROPANE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
DIBROMOMETHANE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
BROMODICHLOROMETHANE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
TRANS-1,3-DICHLOROPROPENE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
TOLUENE	122.0	11.3	15.1	6.4	5.3	2.7	8.6	35.2	3.3
CIS-1,3-DICHLOROPROPENE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
1,1,2-TRICHLOROETHANE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
TETRACHLOROETHENE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
1,3-DICHLOROPROPANE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
DIBROMOCHLOROMETHANE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
1,2-DIBROMOETHANE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
CHLOROBENZENE	LT 15	LT 30	LT 30	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
ETHYLBENZENE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
M/P XYLENE	25	LT 40	4.8	LT 40	LT 20	LT 10	LT 20	LT 20	LT 20
O-XYLENE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
STYRENE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
TRIBROMOMETHANE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
ISOPROPYLBENZENE	LT 15	LT 30	LT 30	LT 30	LT 15	LT 15	167	LT 15	LT 15
BROMOBENZENE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
1,1,2,2-TETRACHLOROETHANE	LT 15	LT 30	LT 30	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
1,2,3-TRICHLOROPROPANE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	LT 20	LT 10	LT 10
N-PROPYLBENZENE	LT 15	LT 30	LT 30	LT 30	LT 15	LT 15	69.8	LT 15	LT 15
2-CHLOROTOLUENE	LT 15	LT 30	LT 30	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
1,3,5-TRIMETHYLBENZENE	LT 15	LT 30	LT 30	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
4-CHLOROTOLUENE	LT 15	LT 30	LT 30	LT 30	LT 15	LT 15	LT 30	LT 15	LT 15
TERT-BUTYLBENZENE	LT 10	LT 20	LT 20	LT 20	LT 10	LT 10	24.2	LT 10	LT 10
1,2,4-TRIMETHYLBENZENE	LT 15	LT 15	LT 15	LT 15	LT 15	LT 15	LT 15	LT 15	LT 15
SEC-BUTYLBENZENE	LT 15	LT 15	LT 15	LT 15	LT 15	LT 15	528	LT 15	LT 15
1,4-DICHLOROBENZENE	LT 10	LT 30	LT 30	LT 30	LT 10	LT 10	LT 30	LT 10	LT 10
P-ISOPROPYLTOLUENE	LT 10	LT 30	LT 30	LT 30	LT 10	LT 10	LT 30	LT 10	LT 10
1,3-DICHLOROBENZENE	LT 10	LT 30	LT 30	LT 30	LT 10	LT 10	LT 30	LT 10	LT 10
1,2-DICHLOROBENZENE	LT 10	LT 30	LT 30	LT 30	LT 10	LT 10	LT 30	LT 10	LT 10
N-BUTYLBENZENE	LT 10	LT 30	LT 30	LT 30	LT 10	LT 10	139	LT 10	LT 10
1,2-DIBROMO-3-CHLOROPROPANE	LT 10	LT 30	LT 30	LT 30	LT 10	LT 10	LT 30	LT 10	LT 10
1,2,4-TRICHLOROBENZENE	LT 30	LT 60	LT 60	LT 60	LT 30	LT 30	LT 60	LT 30	LT 30
HEXACHLOROBUTADIENE	LT 20	LT 40	LT 40	LT 40	LT 20	LT 20	LT 40	LT 20	LT 20
NAPHTHALENE	LT 35	7.4	LT 70	LT 70	LT 35	LT 35	LT 70	LT 35	LT 35
1,2,3-TRICHLOROBENZENE	LT 30	LT 60	LT 60	LT 60	LT 30	LT 30	LT 60	LT 30	LT 30
TOTAL	267.1	33.5	35.7	22.8	9.4	5.9	1012.7	102.1	5.8

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Gibb Ltd
Freightliner Project

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Freightliner Project - E210

	Units	Lab	Hydr Ref		SO63984		SO63985		SO63986		SO63987		SO63988		SO63989	
			Client Ref		TP1 @ 0.6-1.0m		TP1 @ 1.9-2.3m		TP2 @ 0.6-0.7m		TP2 @ 1.2-1.6m		TP3 @ 0.3-0.5m		TP3 @ 0.5-0.65m	
			Sample Date	Method	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98
Arsenic	mg/kg	1	<1		9	52					7	24	13			
Boron water sol	mg/kg	1	4.3		0.2	0.5					<0.1	0.8	0.2			
Cadmium	mg/kg	1	<1.0		<1.0	4.5					<1.0	1.2	<1.0			
Chromium	mg/kg	1	44.0		3.0	21.0					5.0	10.0	24.0			
Chromium VI	mg/kg	2	<1		<1						<1		<1			
Copper	mg/kg	1	1.0		6.0	441.0					2.0	56.0				
Dried Solids	%	1	87.8		82.4	85.3					82.2	80.4	85.4			
Lead	mg/kg	1	<10.0		<10.0	407.0					<10.0	61.0	49.0			
Mercury	mg/kg	1	<0.1		<0.1	0.4					<0.1	0.1	<0.1			
Nickel	mg/kg	1	<5.0		<5.0	47.0					<5.0	52.0	29.0			
TPH by GC-FID	mg/kg	1	<3.42		<3.64	4.59 (Petrol)					<3.65	<3.73	<3.51			
Selenium	mg/kg	1	3		<1	1					<1	<1	<1			
Zinc	mg/kg	1	<1.0		22.0	3550					18.0	166.0	78.0			

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Freightliner Project - E210

	Units	Lab	Method	Hydr Ref		Client Ref		Sample Date		SO63990		SO63991		SO63992		SO63993		SO63994		SO63995	
				TP4 @ 0.4-0.6m		TP4 @ 2.5-2.6m		TP5 @ 0.4-0.6m		TP4 @ 0.4-0.6m		TP4 @ 2.5-2.6m		TP5 @ 0.4-0.6m		TP5 @ 1.8-2.1m		TP6 @ 0.5-0.7m		TP6 @ 1.2-1.4m	
				24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98
Arsenic	mg/kg	1		91		4		33								6		29		8	
Boron water sol	mg/kg	1		0.4		1.5		0.2								0.1		0.6		0.2	
Cadmium	mg/kg	1		2.7		<1.0		1.1								<1.0		<1.0		<1.0	
Chromium	mg/kg	1		3.0		4.0		107.0								4.0		54.0		4.0	
Chromium VI	mg/kg	2		<1		<1		<1								<1		<1		<1	
Copper	mg/kg	1		63.0		5.0		171.0								<1.0		134.0		<1.0	
Dried Solids	%	1		85.8		70.4		87.3								81.1		84.8		82.9	
Lead	mg/kg	1		61.0		<10.0		95.0								<10.0		147.0		<10.0	
Mercury	mg/kg	1		0.5		<0.1		<0.1								<0.1		0.1		<0.1	
Nickel	mg/kg	1		20.0		<5.0		67.0								<5.0		45.0		<5.0	
TPH by GC-FID	mg/kg	1		13.1		<4.26		<3.44								<3.70		<3.54		<3.62	
(Petrol)																					
Selenium	mg/kg	1		2		<1		<1								<1		<1		<1	
Zinc	mg/kg	1		181.0		12.0		544.0								15.0		330.0		15.0	

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Freightliner Project - E210

		Hydr Ref	SO63996	SO63997	SO63998	SO63999	SO64000	SO64001
		Client Ref	TP7 @ 0.45-0.7m	TP7 @ 1.6-2.2m	TP8 @ 0.3-0.4m	TP8 @ 1.6-2.0m	TP9 @ 0.8-1.1m	TP9 @ 2.6-2.7m
		Sample Date	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98	24-Sep-98
Units	Lab	Method						
mg/kg	1		24	8	55	12	18	6
mg/kg	1		0.5	0.2	0.4	<0.1	2.3	6.6
mg/kg	1		<1.0	1.5	3.5	<1.0	<1.0	<1.0
mg/kg	1		10.0	4.0	19.0	3.0	25.0	3.0
mg/kg	2		<1	<1	<1	<1	<1	<1
mg/kg	1		98.0	10.0	191.0	12.0	51.0	5.0
%	1		76.6	81.5	83.4	81.1	70.4	47.1
mg/kg	1		60.0	<9.0	242.0	12.0	48.0	<10.0
mg/kg	1		0.2	<0.1	0.2	<0.1	<0.1	<0.1
mg/kg	1		52.0	5.0	74.0	<5.0	32.0	<5.0
mg/kg	1		<3.92	<3.68	<3.60	<3.70	<4.26	<6.37
TPH by GC-FID								
mg/kg	1		1	<1	<1	<1	1	<1
mg/kg	1		207.0	202.0	407.0	68.0	132.0	23.0
Selenium								
Zinc								

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Lab accreditation Nos 1(Bridgend)=1229 2(Runcorn)=0897
* Indicates determinand not covered by UKAS accreditation
Indicates analysis by sub-contractor

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Freightliner Project - E210

Hydr Ref: SO64002 SO64003

Client Ref TP10 @ 0.6-0.7m TP10 @ 1.6-2.0m

Sample Date 24-Sep-98 24-Sep-98

	Units	Lab	Method	
Arsenic	mg/kg	1	196	17
Boron water sol	mg/kg	1	0.2	<0.1
Cadmium	mg/kg	1	3.8	<1.0
Chromium	mg/kg	1	23.0	4.0
Chromium VI	mg/kg	2	<1	<1
Copper	mg/kg	1	310.0	31.0
Dried Solids	%	1	80.5	82.1
Lead	mg/kg	1	109.0	<10.0
Mercury	mg/kg	1	<0.1	<0.1
Nickel	mg/kg	1	76.0	7.0
TPH by GC-FID	mg/kg	1	< 3.73	< 3.65
Selenium	mg/kg	1	<1	<1
Zinc	mg/kg	1	216.0	107.0

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PROVISIONAL RESULTS - GROUNDWATER

Laboratory Ref	GW65570	GW65571	GW65572	GW65573	GW65566	GW65568	GW65569
Client Ref	E1	E2	E3	E4	E5	E6	Trip Blank
Sample Date	01/10/98	01/10/98	01/10/98	01/10/98	29/09/98	29/09/98	29/09/98
Units	ug/l	ug/l	ug/l	ug/l	ug/l	ug/l	ug/l
DETERMINAND							
DICHLORODIFLUOROMETHANE	LT 2.0	LT 2.0	LT 2.0	LT 2.0	LT 2.0	LT 2.0	LT 2.0
CHLOROMETHANE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
VINYL CHLORIDE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
TRICHLOROFLUOROMETHANE	62.0	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
1,1-DICHLOROETHENE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
DICHLOROMETHANE	LT 25	LT 25	LT 25	LT 25	LT 25	LT 25	LT 25
TRANS-1,2-DICHLOROETHENE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
1,1-DICHLOROETHANE	1.7	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
2,2-DICHLOROPROPANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
CIS-1,2-DICHLOROETHENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
BROMOCHLOROMETHANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
TRICHLOROMETHANE	LT 1.0	LT 1.0	3.4	LT 1.0	35.0	11.8	LT 1.0
1,1,1-TRICHLOROETHANE	3.2	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
1,1-DICHLOROPROPENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
TETRACHLOROMETHANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
BENZENE	LT 1.0	1.1	LT 1.0	1.0	LT 1.0	LT 1.0	LT 1.0
1,2-DICHLOROETHANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
TRICHLOROETHENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
1,2-DICHLOROPROPANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
DIBROMOMETHANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
BROMODICHLOROMETHANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	10.4	3.9	LT 1.0
TRANS-1,3-DICHLOROPROPENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
TOLUENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
CIS-1,3-DICHLOROPROPENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
1,1,2-TRICHLOROETHANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
TETRACHLOROETHENE	1.2	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
1,3-DICHLOROPROPANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
DIBROMOCHLOROMETHANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	2.0	1.1	LT 1.0
1,2-DIBROMOETHANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
CHLOROBENZENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
1,1,1,2-TETRACHLOROETHANE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
ETHYLBENZENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
M/P XYLENE	LT 2.0	7.7	LT 2.0	4.5	LT 2.0	LT 2.0	LT 2.0
O-XYLENE	LT 1.0	2.5	LT 1.0	2.3	LT 1.0	LT 1.0	LT 1.0
STYRENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
TRIBROMOMETHANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
ISOPROPYLBENZENE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
BROMOBENZENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
1,1,2,2-TETRACHLOROETHANE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
1,2,3-TRICHLOROPROPANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
N-PROPYLBENZENE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
2-CHLOROTOLUENE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
1,3,5-TRIMETHYLBENZENE	LT 1.5	33.9	LT 1.5	31.7	LT 1.5	LT 1.5	LT 1.5
4-CHLOROTOLUENE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
TERT-BUTYLBENZENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
1,2,4-TRIMETHYLBENZENE	LT 1.5	17.6	LT 1.5	9.8	LT 1.5	LT 1.5	LT 1.5
SEC-BUTYLBENZENE	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5	LT 1.5
1,4-DICHLOROBENZENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
P-ISOPROPYLTOLUENE	LT 1.0	6.4	LT 1.0	6.0	LT 1.0	LT 1.0	LT 1.0
1,3-DICHLOROBENZENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
1,2-DICHLOROBENZENE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
N-BUTYLBENZENE	LT 1.0	6.6	LT 1.0	6.1	LT 1.0	LT 1.0	LT 1.0
1,2-DIBROMO-3-CHLOROPROPANE	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0	LT 1.0
1,2,4-TRICHLOROBENZENE	LT 3.0	LT 3.0	LT 3.0	LT 3.0	LT 3.0	LT 3.0	LT 3.0
HEXACHLOROBUTADIENE	LT 2.0	LT 2.0	LT 2.0	LT 2.0	LT 2.0	LT 2.0	LT 2.0
NAPHTHALENE	LT 3.5	LT 3.5	LT 3.5	LT 3.5	LT 3.5	LT 3.5	LT 3.5
1,2,3-TRICHLOROBENZENE	LT 3.0	LT 3.0	LT 3.0	LT 3.0	LT 3.0	LT 3.0	LT 3.0
TOTAL	68	76	3	61	47	17	0

Gibb Ltd
Freightliner Project
Provisional Report

15/10/98

FREIGHTLINER SITE **PROVISIONAL GROUNDWATER TESTING RESULTS**

Laboratory Ref	GW65570	GW65571	GW65572	GW65573	GW65566	GW65568
Client Ref	E1	E2	E3	E4	E5	E6
Sample Date	01-Oct-98	01-Oct-98	01-Oct-98	01-Oct-98	29-Sep-98	29-Sep-98
Arsenic (mg/l)	0.009	0.051	0.028	0.043	<0.005	<0.005
Boron (mg/l)	0.13	0.19	0.18	0.16	0.16	0.12
Cadmium (mg/l)	<0.005	<0.005	<0.005	<0.005	<0.005	<0.005
Chromium (mg/l)	<0.03	<0.03	0.07	<0.03	<0.03	<0.03
Chromium 6 (mg/l)	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01
Copper (mg/l)	0.02	0.04	0.32	0.03	<0.05	0.03
Lead (mg/l)	<0.05	0.06	0.18	<0.05	<0.05	<0.05
Mercury (µg/l)	<0.02	0.14	0.04	0.03	<0.02	<0.02
Nickel (mg/l)	0.03	0.06	0.1	<0.03	<0.03	<0.03
Oil ID GC/FID (mg/l)	<0.15	<0.15	<0.15	<0.15	<0.15	<0.15
Selenium (mg/l)	<0.002	<0.002	<0.002	<0.002	<0.002	<0.002
Zinc (mg/l)	0.08	0.26	0.61	0.05	0.03	0.03

APPENDIX G

Well Development Records

GIBB ENVIRONMENTAL WELL DEVELOPMENT FIELD RECORD

PROJECT NUMBER	E210
PROJECT NAME	FREIGHTLINER, NEATH
FACILITY/LOCATION	FORMER FREIGHTLINER SITE
MEASURED BY	N V PARRY
DATE	01-Oct-98
WELL DESIGNATION	BH E1

Development DATA			
Well Development Date:	01-Oct-98	Start Time:	07:50
		Finish Time:	09:15
Depth from TOC to Top of Sediment Before Developing:	m	After Development:	m
Total Well Depth (actual depth w/o sediment from TOC):	8.00	m	
Casing Stick-up (TOC to Ground Surface):	0 cm (or):	Casing Recess (Ground Surface to TOC):	m
Screen Length:	4.50	m	Depth to Top Screen Slot: 1.50 m
Depth from TOC to Static Water before Developing:	1.25	m	After Developing: 1.25 m
Length of Water Column:	4.75	m	Water Level is: -0.25 m Above / Below Top Screen Slot
Well Diameter:	50	mm	Borehole/Sandpack Diameter: 150 mm
Volume of Water Loss During Drilling (if used):	0	litres	
Volume of Water in Well and Sandpack (before development):	24.25	litres	assuming a sandpack porosity of 20%
Volume of Water to Remove for Development:	121.2	litres	i.e. 5 x well volume
Depth from TOC to Static Water 24 hours after Development:	m		

Note development should continue until the following conditions are met:

- 1) Well water is reasonably clear
- 2) Removal of at least five well volumes (including saturated filter annulus plus water loss during drilling; or evacuation of all available water from well (unable to fill bailer after ten minutes, wait for recharge). Purging after development requires the removal of at least three well volumes.

FIELD MEASUREMENTS					
Parameter	Equipment I.D.	1st Reading	2nd Reading	3rd Reading	4th Reading
Temperature deg. C	-	14.8	14.8	14.7	14.7
pH	-	7	7.2	7.1	7.1
Specific Conductivity μ S	-	17	13	12	12
No. of Litres Removed	-	15	90	122	128
Time	-	08:08	08:55	09:05	09:10
TOTAL VOLUME OF WATER REMOV-135 Litres					
Comments:					

GENERAL DATA	
Weather:	overcast, cool, dry
	Air temp C: 14.5
Type and Size of Well Developing Equip	Disposable bailer
Description of Surge Technique (if used):	
Physical Description of Water:	Dark brown, oily sheen

GIBB ENVIRONMENTAL WELL DEVELOPMENT FIELD RECORD

PROJECT NUMBER	E210
PROJECT NAME	FREIGHTLINER, NEATH
FACILITY/LOCATION	FORMER FREIGHTLINER SITE
MEASURED BY	N V PARRY
DATE	01-Oct-98
WELL DESIGNATION	BH E3

Development DATA			
Well Development Date:	01-Oct-98	Start Time:	10:05
		Finish Time:	10:55
Depth from TOC to Top of Sediment Before Developing:	6.00 m	After Development:	6.20 m
Total Well Depth (actual depth w/o sediment from TOC):	6.50 m		
Casing Stick-up (TOC to Ground Surface):	43 cm (or):	Casing Recess (Ground Surface to TOC):	m
Screen Length:	3.00 m	Depth to Top Screen Slot:	2.00 m
Depth from TOC to Static Water before Developing:	2.18 m	After Developing:	2.21 m
Length of Water Column:	2.82 m	Water Level is:	0.18 m Above / Below Top Screen Slot
Well Diameter:	50 mm	Borehole/Sandpack Diameter:	150 mm
Volume of Water Loss During Drilling (if used):	0.00 litres		
Volume of Water in Well and Sandpack (before development):	14.40 litres	assuming a sandpack porosity of 20%	
Volume of Water to Remove for Development:	71.98 litres	i.e. 5 x well volume	
Depth from TOC to Static Water 24 hours after Development:	m		

Note development should continue until the following conditions are met:

- 1) Well water is reasonably clear
- 2) Removal of at least five well volumes (including saturated filter annulus plus water loss during drilling; or evacuation of all available water from well (unable to fill bailer after ten minutes, wait for recharge). Purging after development requires the removal of at least three well volumes.

FIELD MEASUREMENTS					
Parameter	Equipment I.D.	1st Reading	2nd Reading	3rd Reading	4th Reading
Temperature deg. C		14.3	14.0	14.1	14
pH		6.9	7.0	6.9	6.9
Specific Conductivity μ S		8	7	7	7
No. of Litres Removed		10	82	90	110
Time		10:12	10:30	10:32	10:35
TOTAL VOLUME OF WATER REMOVED 120 Litres					
Comments:					

GENERAL DATA	
Weather:	overcast, cool, dry
	Air Temp C: 15.7
Type and Size of Well Developing Equip	Disposable bailer
Description of Surge Technique (if used):	
Physical Description of Water:	Dark brown, becoming clear

GIBB ENVIRONMENTAL WELL DEVELOPMENT FIELD RECORD

PROJECT NUMBER	E210
PROJECT NAME	FREIGHTLINER, NEATH
FACILITY/LOCATION	FORMER FREIGHTLINER SITE
MEASURED BY	N V PARRY
DATE	01-Oct-98
WELL DESIGNATION	BH E2

Development DATA			
Well Development Date:	01-Oct-98	Start Time:	09:25
		Finish Time:	
Depth from TOC to Top of Sediment Before Developing:	m	After Development:	6.68 m
Total Well Depth (actual depth w/o sediment from TOC):	8.00 m		
Casing Stick-up (TOC to Ground Surface):	0 cm (or):	Casing Recess (Ground Surface to TOC):	m
Screen Length:	4.00 m	Depth to Top Screen Slot:	1.50 m
Depth from TOC to Static Water before Developing:	1.13 m	After Developing:	2.21 m
Length of Water Column:	4.37 m	Water Level is:	-0.37 m Above / Below Top Screen Slot
Well Diameter:	50 mm	Borehole/Sandpack Diameter:	150 mm
Volume of Water Loss During Drilling (if used):	0.00 litres		
Volume of Water in Well and Sandpack (before development):	22.31 litres	assuming a sandpack porosity of 20%	
Volume of Water to Remove for Development:	111.55 litres	i.e. 5 x well volume	
Depth from TOC to Static Water 24 hours after Development:	m		

Note development should continue until the following conditions are met:

- 1) Well water is reasonably clear
- 2) Removal of at least five well volumes (including saturated filter annulus plus water loss during drilling, or evacuation of all available water from well (unable to fill bailer after ten minutes, wait for recharge). Purging after development requires the removal of at least three well volumes.

FIELD MEASUREMENTS					
Parameter	Equipment I.D.	1st Reading	2nd Reading	3rd Reading	4th Reading
Temperature deg. C	-	13.6	13.0	13.1	13.1
pH	-	7	6.9	6.9	6.8
Specific Conductivity μ S	-	10	12	11	12
No. of Litres Removed	-	10	120	130	145
Time	-	09:30	9:50	9:55	10:10
TOTAL VOLUME OF WATER REMOVED 135 Litres					
Comments:					

GENERAL DATA	
Weather:	overcast, cool, dry
	Air temp C: 17
Type and Size of Well Developing Equip	Disposable bailer
Description of Surge Technique (if used):	
Physical Description of Water:	Dark brown, oily sheen, very strong organic (diesel?) smell

APPENDIX H

Gas Monitoring Results

Freightliner Terminal - Gas Monitoring Results - 16 October 1998

BH No	Gas Concentration (%)			Groundwater r Depth (m)	Cover Type
	O ₂	CO ₂	CH ₄		
E1	2	2.6	82	1.3	Flush
E2	20.2	0.2	0	1.12	Flush
E3	5	1.7	24	1.66 (BGL)	Raised (0.2m)

Atmospheric pressure: 1008; Temperature 15degrees C