

5 September 2024

**Emma Jones**

Authorised on behalf of Natural Resources Wales

Wales Permitting Centre  
Cathays Park  
King Edward VII Avenue  
Cardiff  
CF10 3NQ

Dear Emma,

**RE: Notice requiring further information, Application number: PAN-0022125**

Thank you for your Schedule 5 Notice 3 dated 8/8/24 requesting further information regarding the Groundwater Risk Assessment provided in support of an environmental permit to discharge treated sewage effluent to land at Llyn Gwynant Campsite.

We have summarised the issues you have raised below together with our response to each issue.

In the interest of attempting to reach agreement, or at least narrow the points of difference on these issues, we kindly request a video conference with your technical expert(s) to discuss these matters. Please nominate your appropriate expert(s) and a series of dates/times that are convenient for your team to attend this session.

**1. Groundwater Receptor and Environmental Standard**

You have stated that our assessment “...has focused on the Afon Glaslyn surface water body whereas Groundwater itself should be considered a receptor”. You have also requested a comparison of groundwater quality data in down-gradient boreholes with the relevant environmental standard or MRV.

We sought clarity on this aspect and Peter Garden relayed our query (via email on 30/8/24) asking why the groundwater quality within the relatively confined 300 m distance extending downgradient from the irrigation field to surface water (the Afon Glaslyn) is of concern given our assessment has shown there is a very minor (and undetectable) effect on the downgradient Afon Glaslyn. We queried NRW’s concern with regards to any very localised non-hazardous pollutant (e.g. ammonium-nitrogen) impact, particularly considering any impacted groundwater is entirely confined within the property boundary. We queried whether NRW was concerned with the stygofauna within the groundwater system, or some other aspect? We requested guidance on this aspect from your expert.

On 1/9/24 Asta Smith responded “...groundwater is the water stored in soil and rocks underground that are known as aquifers. It is a critical and often forgotten part of the water cycle. Groundwater is a vital

*resource, sustaining our springs, rivers, and wetlands, providing habitats for lots of species. It can be abstracted for drinking water or for use by industry and farms by using boreholes with pumps. Groundwater currently supplies about 5% of the public water supply in Wales but in rural areas, groundwater may be the only viable water source for isolated properties.”*

We don't disagree with this definition of groundwater; however, our query as to the basis for requiring concentrations of non-hazardous pollutants in the localised downgradient groundwater system to be less than the drinking water standard (DWS) or some minimum reporting value has not been addressed.

We are not disputing the need to protect groundwater resources generally, and certainly not where there is potential for adverse impact on any downgradient receiving environment or groundwater user. However, again, our conceptual groundwater model shows that the shallow groundwater from the wastewater irrigation field flows to the Afon Glaslyn, which intercepts the shallow groundwater to the west of the site, and with the lake intercepts the shallow groundwater to the south. We have also noted that the impermeable clay layer approximately 2 m below ground level provides an aquitard to prevent migration of the shallow groundwater to deeper aquifers. Therefore, any impacted groundwater is expected to be entirely confined within the site boundary and therefore the proposed discharge will have no adverse effect on groundwater beyond the site boundary. Furthermore, and again our risk assessment has outlined this, there are no downgradient groundwater users, with the nearest groundwater user being the Campsite water supply borehole located 300 m upgradient and abstracting from rock at a depth of 110 m.

We also note that the fine-grained shallow strata at the site (silt and clay) would not be considered a superficial aquifer in terms of the British Geological Survey definition of a superficial aquifer as “permeable, unconsolidated (loose) deposits, e.g. sands and gravels”<sup>1</sup>. To repeat commentary again from our risk assessment report, the shallow strata at the site would more appropriately be considered non-productive strata.

## **2. Attenuation and Dilution Model**

While as discussed above we question why groundwater concentrations of non-hazardous pollutants downgradient of the irrigation field must achieve DWS, we have provided a theoretical assessment of attenuation and dilution in the groundwater system using the Environmental Agency's Infiltration Worksheet V3.0 (released March 2022). Our assessment of ammonium-nitrogen attenuation and dilution using this model and applying site specific data is presented as Attachment 1.

Please note that this assessment worksheet tool only assesses attenuation and dilution in the groundwater system and does not model ammonium-nitrogen uptake to the pasture crop within the overlying soil horizon of the 0.5 hectare irrigation field. As our assessment has outlined, ammonium-nitrogen is being removed from this system as harvested grass crop which is carted offsite (i.e. the irrigation field comprises of a cut-and-carry pasture system). Therefore, for this campsite irrigation system, which our risk assessment has noted is a seasonable operation with peak discharge times coinciding with periods of peak grass growth, the concentration of substance in discharge will not be the same as the concentration of the substance entering the infiltration system (i.e. refer to Infiltration Worksheet cell D11).

Further groundwater quality monitoring data is required to confirm the upgradient groundwater concentration used in the modelling (which has thus far been based on one sample only collected from

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<sup>1</sup> <https://www.bgs.ac.uk/datasets/aquifer-designation-data/>

the existing upgradient borehole) and to compare this modelled downgradient concentration with monitoring data.

### **3. Monitoring Boreholes**

We are supportive of ongoing monitoring of groundwater quality upgradient and downgradient of the irrigation field, even if a groundwater compliance point is not appropriate in this instance.

A layout plan showing the location of the 3 existing boreholes and 3 additional proposed boreholes is attached as Attachment 2. Please note that the naming of the monitoring boreholes/wells has been updated from previous reporting.

The existing Boreholes (MW2, M3 and MW4) have been used to assess groundwater flow direction and travel time as outlined in our risk assessment report. A sketch drawing of the construction of these existing boreholes is provided as Attachment 3, including proposed modifications to add bentonite and sealed and lockable surface boxes flush with ground level.

Additional Boreholes are proposed to be drilled as follows:

1. MW1 – Upgradient
2. MW5 – 100m downgradient of Irrigation Field
3. MW6 – 200m downgradient of Irrigation Field

These boreholes are proposed to be installed in October 2024 by Dragon Drilling Ltd using a hollow stem auger drilling method. These boreholes will be constructed in accordance with Environment Agency Guidance on the design and installation of groundwater quality monitoring points Science Report SC020093, January 2006. We request feedback from NRW regarding the proposed borehole locations prior to their installation.

Once installed, boreholes will be purged to develop the boreholes and water quality samples will be collected and sent to an analytical laboratory. As per Section 6.2 of our risk assessment report, proposed test parameters are ammonium-nitrogen and orthophosphate as P. Bi-annual groundwater sampling is proposed. Please provide any feedback on the proposed sampling parameters and frequency.

### **4. Alternative Proposal for a Direct Surface Water Discharge**

As an alternative to a land discharge, in early 2023 we understand that Peter Garden queried whether a permit for direct discharge of treated wastewater to surface water (the Afon Glaslyn) could be granted. We understand that feedback at this time was that a permit for a surface water discharge would not be granted, however no technical explanation for this response was provided.

While we consider the proposed land irrigation of treated wastewater to provide the best option to minimise adverse impacts on the receiving environment, for our records we request that you please provide an explanation as to why a surface water discharge cannot be granted subject to appropriate assessment of environmental effects demonstrating that impacts are suitably minor.

Yours sincerely,

Dan Garden

Environmental Engineer

Tom Garden

Hydrogeologist

**Attachments:**

1. Environment Agency Infiltration Worksheet (V3.0) – Ammonium-Nitrogen Attenuation and Dilution Model
2. Monitoring Borehole Layout Plan
3. Existing Borehole Details

**Attachment 1:** Environment Agency Infiltration Worksheet (V3.0) –  
Ammonium-Nitrogen Attenuation and Dilution Model



## Groundwater risk assessment for treated effluent discharges to infiltration systems

### Infiltration Worksheet , Release v3.0


Date of Workbook Issue: March 2022

This worksheet has been produced in combination with the document: H1 Annex J5 User Manual version 2.0 (Environment Agency, 2014).

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**IMPORTANT:** To enable MS Excel worksheet, click the Microsoft Office Button  Excel Options, click Add-Ins. In the Manage box, select Excel Add-ins. Click Go. Select **Analysis ToolPak** and **Analysis ToolPak-VBA** (to calculate error functions)

#### Details to be completed for each assessment

Site Name:	Llyn Gwynant Campsite		
Site Address:	Nant Gwynant, LL554NW		
Completed by:	DG, TG		
Date:	4-Sep-24	Version:	2
Substance	Ammonium		
Environmental Standard (C <sub>T</sub> )	0.5	mg/l	Origin of C <sub>T</sub> : DWS

This spreadsheet has been developed as a tool to assist groundwater risk assessment for effluent discharges to infiltration systems. The following worksheets are available:

[Infiltration System](#)  
[Attenuation unsatzone](#)  
[Dilution](#)  
[Attenuation satzone](#)  
[Summary](#)  
[Simple calcs](#)

Site details entered on this page are automatically copied to each worksheet.

The worksheet uses the following colour coding:

	Worksheet option with pull down menu
	Data entry
	Data origin / justification should be noted in cells coloured yellow and fully documented in subsequent reports.
	Data carried forward from an earlier worksheet
	Calculation

It is recommended that a copy of the original worksheet is saved (all data fields in the original copy are blank).

Infiltration Worksheet



Infiltration System

Substance	Ammonium	From introduction sheet
Compliance value or environmental standard	$5.00E-01$ mg/l	From introduction sheet

This sheet allows user to enter effluent concentration and details of infiltration system

Input Parameters

Standard entry

Concentration of substance in discharge (entering infiltration system)	$C_e$	$2.30E+00$	mg/l	Average daily leaching losses to GW at 2.3 mg/L with proposed wastewater discharge at 5 mg/L and 55% removal in irrigation area via plant (grass) uptake
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Type of treatment plant

Treatment plant

Water use and percolation rate (for use only with septic tanks and package treatment plants)

Number of persons	p			Not valid for this treatment plant option
Water use		$1.80E+02$	litres/person/day	Not valid for this treatment plant option
Percolation rate	Vp		s/mm	Not valid for this treatment plant option

Specify discharge (Q1) or calculate based on use (Q2)

Specified discharge Q1

Discharge rate	Q1	$1.42E+01$	m <sup>3</sup> /d	Table 2 of GWRA
Calculated discharge	Q2	$0.00E+00$	m <sup>3</sup> /d	Value specified by user and not calculated

Area of drainage field and hydraulic loading

Specify area of drainage field or calculate based on percolation rate

Specify

Enter area of drainage field	A	$5.00E+03$	m <sup>2</sup>	Area specified in Table 4 of GWRA
Calculated area of drainage field	A	$0.00E+00$	m <sup>2</sup>	Value specified by user and not calculated
Calculated infiltration rate	Inf	$2.84E-03$	m/d	

Site being assessed: Llyn Gwynant Campsite  
Completed by: DG, TG  
Date: 4-Sep-24  
Version: 2

## Infiltration Worksheet

## Attenuation unsaturated zone



This sheet calculates attenuation factor for the unsaturated zone; concentration at base of unsaturated zone and discharge consent limit

Contaminant	Ammonium			
Compliance value or environmental standard	C <sub>T</sub>	5.00E-01	mg/l	From introduction sheet
Concentration of substance in substance in discharge (entering infiltration system)	C <sub>e</sub>	2.30E+00	mg/l	From introduction sheet
				From infiltration sheet
Input Parameters	Variable	Value	Unit	Source of parameter value
Standard entry				
Drainage Layer				
Infiltration rate	Inf	2.84E-03	m/d	From infiltration sheet
Thickness of drainage layer	S <sub>1</sub>	1.00E+00	m	Assuming water table at 1mbgl
Water filled porosity	θ <sub>1</sub>	3.00E-01	fraction	Estimate for silt.
Bulk density	ρ <sub>1</sub>	1.60E+00	g/cm <sup>3</sup>	Estimate for silt.
Calculated dispersivity	D <sub>1</sub>	1.00E-01	m	calculated
Option to select degradation		Degradation occurs - sorbed and dissolved phases		
Half life for degradation of substance	t <sub>1/2</sub>	7.30E+02	days	
Calculated decay rate	λ <sub>1</sub>	9.50E-04	days <sup>-1</sup>	calculated (very low value set if no degradation) Calculated from half life (above)
Enter method of defining partition co-efficient (using pull down list)		User specified value for partition coefficient		
Entry if specify partition coefficient (option)				
Soil water partition coefficient	K <sub>d1</sub>	1.00E+00	l/kg	
Entry for organic chemicals (option)				
Fraction of organic carbon (in soil)	f <sub>oc1</sub>	1.00E-02	fraction	Not valid - User specified value used
Organic carbon partition coefficient	K <sub>oc1</sub>	1.00E+01	l/kg	Not valid - User specified value used
Soil water partition coefficient used in assessment	K <sub>d1</sub>	1.00E+00	l/kg	Specified value
Retardation factor	Rf <sub>u1</sub>	6.33E+00		
Unretarded travel time (no dispersion)	t <sub>u1</sub>	1.06E+02	d	
Unretarded travel time (with dispersion)	t <sub>u1</sub>	9.51E+01	d	
Retarded travel time (with dispersion)	t <sub>r1</sub>	6.02E+02	d	
Attenuation factor	AF <sub>u1</sub>	1.82E+00		
Unsaturated Zone				
Thickness of unsaturated zone below drainage field	S <sub>2</sub>	1.00E+00	m	Assuming water table at 1mbgl
Water filled porosity	θ <sub>2</sub>	2.00E-01	fraction	Assumed at 0.2
Bulk density of unsaturated zone	ρ <sub>2</sub>	1.60E+00	g/cm <sup>3</sup>	Guess
Calculated dispersivity	D <sub>2</sub>	1.00E-01	m	calculated
Option to select degradation		Degradation occurs - sorbed and dissolved phases		
Half life for degradation of substance	t <sub>1/2</sub>	7.30E+02	days	
Calculated decay rate	λ <sub>2</sub>	9.50E-04	days <sup>-1</sup>	calculated (very low value set if no degradation) Default value of 1/10 <sup>99</sup> used
Fraction of rapid flow through unsaturated zone	B	0.00E+00	fraction	
Enter method of defining partition co-efficient (using pull down list)		User specified value for partition coefficient		
Entry if specify partition coefficient (option)				
Soil water partition coefficient	K <sub>d2</sub>	1.00E+00	l/kg	
Entry for organic chemicals (option)				
Fraction of organic carbon (in soil)	f <sub>oc2</sub>	1.00E-02	fraction	Not valid - User specified value used
Organic carbon partition coefficient	K <sub>oc2</sub>	1.00E+01	l/kg	Not valid - User specified value used
Soil water partition coefficient used in assessment	K <sub>d2</sub>	1.00E+00	l/kg	Specified value
Retardation factor	Rf <sub>u2</sub>	9.00E+00		
Unretarded travel time (no dispersion)	t <sub>u2</sub>	7.04E+01	d	
Unretarded travel time (with dispersion)	t <sub>u2</sub>	6.34E+01	d	
Retarded travel time (with dispersion)	t <sub>r2</sub>	5.70E+02	d	
Attenuation factor	AF <sub>u2</sub>	1.77E+00		
Total unretarded travel time	t <sub>u1</sub> + t <sub>u2</sub>	1.76E+02	d	
Total retarded travel time	t <sub>r1</sub> + t <sub>r2</sub>	1.30E+03	d	
Attenuation factor and discharge consent limit				
Drainage layer attenuation factor	AF <sub>u1</sub>	1.82E+00		
Unsaturated zone attenuation factor	AF <sub>u2</sub>	1.77E+00		
Concentration at base of drainage layer	C <sub>db</sub>	1.26E+00	mg/l	
Concentration at base of unsaturated zone	C <sub>wt</sub>	7.15E-01	mg/l	
		and		

Site being assessed: Llyn Gwynant Campsite

Completed by: DG, TG  
Date: 4-Sep-24

Version: 2



## Infiltration Worksheet



### Dilution

Substance		Ammonium		
Compliance value or environmental standard	C <sub>T</sub>	5.00E-01	mg/l	From introduction sheet
Source concentration	C <sub>e</sub>	2.30E+00	mg/l	From infiltration sheet
Concentration at base of drainage layer	C <sub>wt</sub>	7.15E-01	mg/l	From atten_unsatzone sheet

This sheet calculates the dilution factor for groundwater dilution below the drainage field.  
Substance concentration in groundwater and discharge consent limit

#### Input Parameters

Standard entry

Infiltration	Inf	2.84E-03	m/d	From infiltration sheet
Area of drainage field	A	5.00E+03	m <sup>2</sup>	From infiltration sheet

Entry for groundwater flow below site

Length of drainage field in direction of groundwater flow	L	8.00E+01	m
Saturated aquifer thickness	da	3.00E+00	m
Hydraulic Conductivity of aquifer in which dilution occurs	K	1.00E-01	m/d
Hydraulic gradient of water table	i	3.70E-02	fraction
Width of drainage field perpendicular to groundwater flow	w	6.25E+01	m
Background concentration of substance in groundwater up-gradient of site	Cu	4.00E-02	mg/l

Survey Plan
From Test Pits, Blue Clay
Freeze & Cherry 1979 (Table 2.2, silt)
From piezometric survey May 2023
Survey Plan
From upgradient monitoring at detection limit

Define mixing zone depth by specifying or calculating depth (using pull down list)

Enter mixing zone thickness	Mz	5.00E+00	m	Not valid - Value calculated
Calculated mixing zone thickness	Mz	3.00E+00	m	
Groundwater flow (mixing zone) below drainage field	Gw	0.69	m <sup>3</sup> /d	

#### Dilution factor and discharge consent limit

Dilution Factor	DF	1.048855634		
Headroom Factor	HF	1.044947183		
Unsaturated zone attenuation factor	AFu	1.77E+00		From infiltration sheet
Concentration in groundwater below drainage field	C <sub>gw</sub>	6.83E-01	mg/l	
		or		
Environmental Permit limit value	EPL <sub>2</sub>	1.681231515	mg/l	

Site being assessed:	Llyn Gwynant Campsite
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Concentration immediately downgradient of drainage field exceeds target concentration

## Infiltration Worksheet

### Attenuation in saturated zone

Input Parameters	Variable	Value	Unit	Source
Substance		Ammonium		From introduction sheet
Compliance value or environmental standard	C <sub>i</sub>	5.00E-01	mg/l	From introduction sheet
Source concentration	C <sub>0</sub>	2.30E+00	mg/l	From infiltration sheet
Dilution Factor	DF	1.05E+00		from dilution sheet
Unsaturated zone attenuation factor	AF <sub>u</sub>	1.77E+00		From atten_unsatzone sheet

Variable	Value	Unit	Source of parameter value
Concentration in groundwater below drainage field	C <sub>gw</sub>	6.83E-01	mg/l from dilution sheet
Option to select degradation	No degradation occurs		
Half life for degradation of substance	t <sub>1/2</sub>	7.30E+02	days
Calculated decay rate	λ	1.00E-09	days <sup>-1</sup> calculated (very low value set if no degradation)
Width of drainage field	W	6.25E+01	m from dilution sheet
Mixing zone thickness	Mz	3.00E+00	m from dilution sheet
Bulk density of aquifer materials	ρ	1.80E+00	g/cm <sup>3</sup> Estimate for silts
Effective porosity of aquifer	n	1.00E-02	fraction Estimate for silts
Hydraulic gradient	i <sub>corr</sub>	7.94E-01	fraction from dilution sheet (adjusted)
Hydraulic conductivity of saturated aquifer	K	1.00E-01	m/d from dilution sheet
Distance to compliance point	x	1.00E+02	m

Option to select time	Use steady state (recommended)		
Enter time	t	1.00E+02	days
Time since pollutant entered groundwater	t	1.00E+09	days
Parameters values determined from options			
Partition coefficient	K <sub>d</sub>	0.00E+00	l/kg see options
Longitudinal dispersivity	ax	4.42E+00	m see options
Transverse dispersivity	az	4.42E-01	m see options
Vertical dispersivity	ay	4.42E-02	m see options

Calculated Parameters	Variable	Value	Unit
Groundwater flow velocity	v	7.94E+00	m/d
Retardation factor	R <sub>f</sub>	1.00E+00	fraction
Decay rate used	λ	1.00E-09	d <sup>-1</sup>
Hydraulic gradient used in aquifer flow down-gradient	i <sub>corr</sub>	7.94E-01	fraction
Rate of contaminant flow due to retardation	u	7.94E+00	m/d
Attenuation factor	AF <sub>s</sub>	1.46E+00	fraction

#### Attenuation and Dilution factors and discharge consent limit

Dilution Factor	DF	1.05E+00	
Unsaturated zone attenuation factor	AF <sub>u</sub>	1.77E+00	
Saturated zone attenuation factor	AF <sub>s</sub>	1.46E+00	
Concentration in groundwater at compliance point	C <sub>dis</sub>	0.481474429	mg/l
		or	
Environmental Permit limit value	EPL <sub>3</sub>	2.45E+00	mg/l
Distance to compliance point		100	m

Concentration at compliance point below target concentration

This sheet calculates attenuation factor for the saturated zone; substance concentration at downgradient compliance point and discharge consent limit



#### Enter method of defining partition co-efficient (using pull down list)

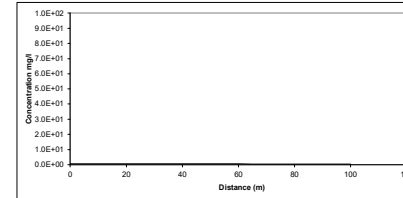
User specified value for partition coefficient		
Entry if specify partition coefficient (option)		
Soil water partition coefficient	K <sub>d</sub>	l/kg
Entry for organic chemicals (option)		
Fraction of organic carbon in aquifer	f <sub>oc</sub>	fraction
Organic carbon partition coefficient	K <sub>oc</sub>	l/kg
Soil water partition coefficient	K <sub>d</sub>	0.00E+00 l/kg

#### Define dispersivity (click brown cell and use pull down list)

Dispersivity based on Xu & Eckstein (1995)		
Longitudinal dispersivity (m)	ax	4.42E+00
Transverse dispersivity (m)	az	4.42E-01
Vertical dispersivity (m)	ay	4.42E-02

Note values of dispersivity must be > 0

Xu & Eckstein (1995) report  $ax = 0.83(\log_{10}x)^{0.414}$ ;  $az = ax/10$ ,  $ay = ax/100$  are assumed  
For calculated value, assumes  $ax = 0.1 \cdot x$ ,  $az = 0.01 \cdot x$ ,  $ay = 0.001 \cdot x$



Calculated concentrations for distance-concentration graph

From calculation sheet	Distance m	Concentration mg/l
	0	6.8E-01
	5.0	6.83E-01
	10.0	6.82E-01
	15.0	6.77E-01
	20.0	6.68E-01
	25.0	6.55E-01
	30.0	6.41E-01
	35.0	6.27E-01
	40.0	6.12E-01
	45.0	5.98E-01
	50.0	5.84E-01
	55.0	5.72E-01
	60.0	5.59E-01
	65.0	5.48E-01
	70.0	5.37E-01
	75.0	5.26E-01
	80.0	5.16E-01
	85.0	5.07E-01
	90.0	4.98E-01
	95.0	4.90E-01
	100.0	4.81E-01

Site being assessed:	Llyn Gwynant Campsite
Completed by:	0
Date:	0-Jan-00
Version:	0

## Infiltration Worksheet

### Summary of calculations for concentration of substance in groundwater

No input required, values taken from previous worksheets

#### Summary of compliance data, attenuation and dilution factors

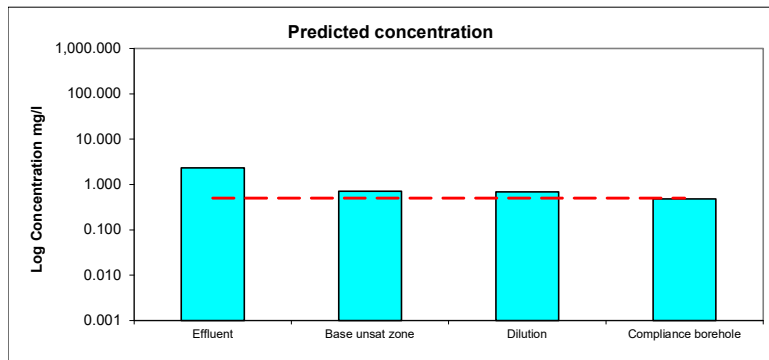
Substance	Ammonium		
Effluent concentration	$C_e$	2.30E+00	mg/l
Compliance value or environmental standard	$C_T$	0.50	mg/l
Distance to compliance point		100.00	m
Attenuation factor - unsat zone	$AF_u$	1.77E+00	
Dilution Factor	$DF$	1.05E+00	
Attenuation factor- sat zone	$AF_s$	1.46E+00	

#### Predicted concentrations at compliance point based on proposed effluent concentration

Concentration at base of unsaturated zone	$C_{wt}$	7.15E-01	mg/l	Attenuation in unsaturated zone only
Concentration in groundwater below drainage field	$C_{gw}$	6.83E-01	mg/l	Dilution taken into account
Concentration in groundwater at compliance point	$C_{dcp}$	4.81E-01	mg/l	Attenuation in saturated zone taken into account

#### Provisional Environmental Permit limit values

Based on attenuation in unsaturated zone	$EPL_1$	1.61E+00	mg/l	
Based on attenuation in unsaturated zone and dilution	$EPL_2$	1.68E+00	mg/l	
Based on dilution and attenuation in unsaturated and saturated zone	$EPL_3$	2.45E+00	mg/l	Discharge limit for discussion with Environment Agency



## Simple hydrogeological calculations

(These calculations are provided to allow additional hydrogeological calculations to be undertaken if required)

Parameter	symbol	unit	justification
Hydraulic conductivity	K	1.00E+00 m/d	Literature value
Hydraulic gradient	i	3.70E-02 unitless	May 2023 piezometric survey
Effective porosity of aquifer	n	1.00E-02 fraction	Estimate
Thickness of saturated aquifer	b	2.00E+00 m	from test pits
Width of aquifer perpendicular to flow	w	1.00E+02 m	survey
Distance to receptor	x	1.00E+02 m	Distance to drain
Bulk density of aquifer materials	$\rho$	1.80E+03 g/cm <sup>3</sup>	
Soil-water partition co-efficient	Kd	0.00E+00 l/kg	
Retardation factor of pollutant	R	1	

Groundwater flow velocity	v(GW)	4.29E-05 m/s	3.70E+00 m/day	1.35E+03 m/year
Time for groundwater to reach receptor	t(GW)	2.33E+06 seconds	2.70E+01 days	7.40E-02 years
Rate of groundwater flow through aquifer	Q	8.57E-05 m <sup>3</sup> /s	7.41E+00 m <sup>3</sup> /day	2.70E+03 m <sup>3</sup> /year

Contaminant flow velocity	v(contam)	4.29E-05 m/s	3.70E+00 m/day	1.35E+03 m/year
Time for contaminant to reach receptor	t(contam)	2.33E+06 seconds	2.70E+01 days	7.40E-02 years

**Attachment 2:**      Monitoring Borehole Layout Plan





Afon Glaslyn

Camping Fields

Llyn Gwynant

MW6

MW5

MW4

MW3

MW2

MW1

## Legend



Disposal Area



Small Streams



Drains



Calculated Groundwater  
Flow Direction (May 2023)



Predicted Groundwater Flow

Monitoring Wells



Existing



Proposed

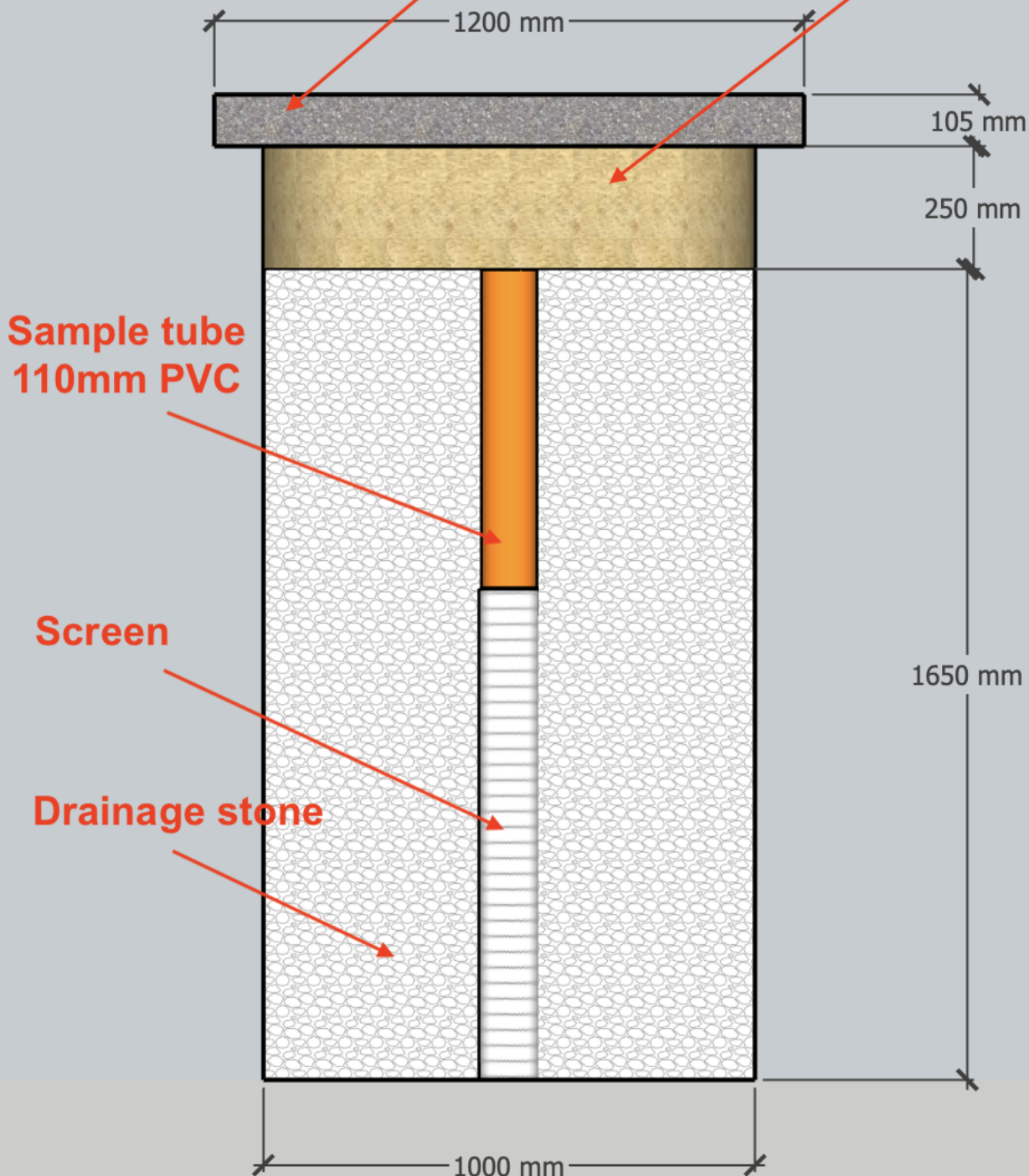
0 50 100 m



**Attachment 3:** Existing Borehole Details

**Protective concrete slab**

**Bentonite seal**





**Stuart Wells CMW8  
190mm BS124 cover**

**Sample tube extends  
up through bentonite  
and slab and is  
sealed to metal cover**

**Concrete slab**

**Drainage stone**

**Slab falls to all  
sides at 3% to  
prevent surface  
water ingress**

